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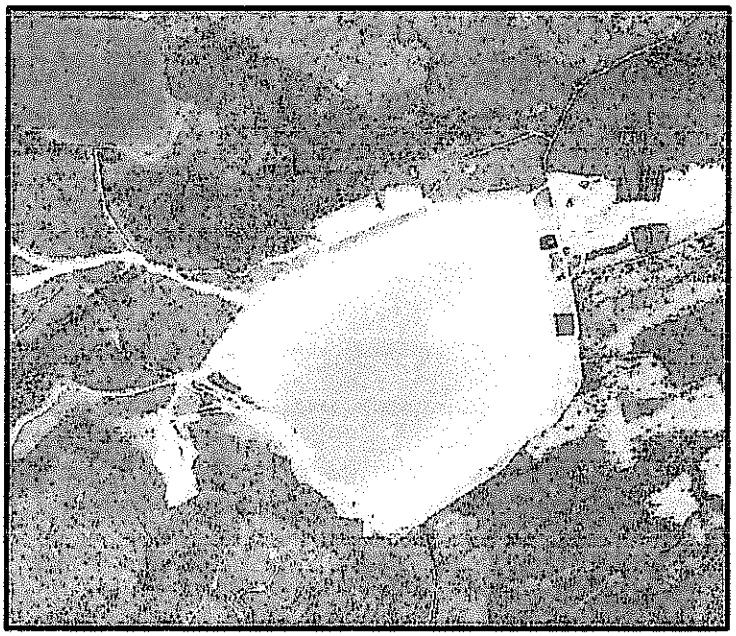
MOUNT POLLEY MINE
Tailings Storage Facility Stage 8/8A
2012 As-Built Report



Submitted to:

Mount Polley Mining Corporation,
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SUMMARY

This report presents the as-built report documenting the 2012 construction of the Mount Polley Mining Corporation (MPMC) tailings storage facility (TSF). The following gives a general summary of the 2012 TSF activities and key developments.

The Stage 8 TSF raise targeted a minimum crest raise of El. 963.5 m via a modified centerline design. At the request of MPMC, an intermediate Stage 8A TSF raise was designed to El. 965 m which utilized a centerline raise design above El. 963.5 m (AMEC 2012a). The Stage 8A design was requested by MPMC to allow the option of raising the dam during more favourable weather conditions in 2012 (as opposed to spring 2013).

Construction of the Stage 8/8A raise began with the placement of Zone S (Till) in early May. Zone S placement was suspended on October 26. At the end of construction the Zone S was completed to a minimum crest elevation of 963.5 m with Zone F (Filter) and Zone T (Transition) completed to a minimum elevation of 962.7 m.

The 2012 embankment raise consisted of:

- Placement of zone materials:
  - Zone U – comprised of tailings sand cells and non acid-generating (NAG) rockfill (minor volumes);
  - Zone S – comprised of compacted glacial till;
  - Zone F – comprised of filter zone NAG rockfill;
  - Zone T – comprised of transition zone NAG rockfill; and
  - Zone C – comprised of run of mine NAG rockfill.
- Foundation preparation of abutment tie-in on the Perimeter and South Embankments.

An AMEC representative was on site to observe the start of the construction and to provide training for the MPMC personnel responsible for the construction monitoring. AMEC reviewed daily reports, performed laboratory tests on selected samples, reviewed instrumentation data, and conducted site visits during critical stages of construction to verify that the materials and construction methodology satisfied design specifications.

MPMC performed all related earthwork construction for Zone U (Upstream Fill), Zone T and Zone C (NAG Rock Shell). Material placement and related earthwork construction for Zone S and Zone F were completed by Peterson Contracting Ltd (Peterson). MPMC monitored daily construction, issued daily reports, completed material sampling, and conducted instrumentation data gathering internally.

1.0 INTRODUCTION

1.1 General

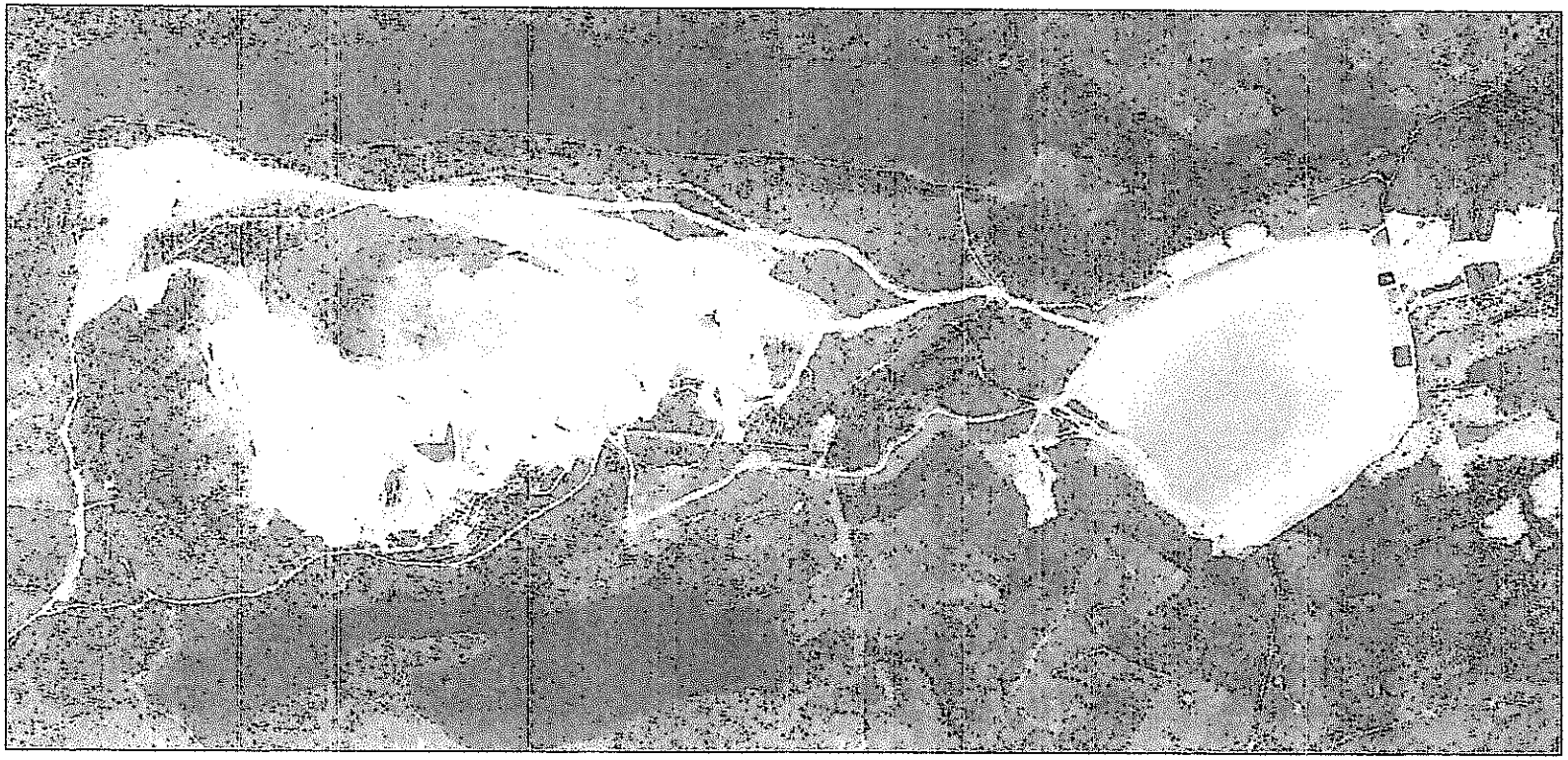
The Mount Polley Mine is located in central British Columbia, approximately 60 km northeast of Williams Lake. The Mount Polley copper and gold mine commenced production in 1997 and operated until October 2001 when operations were suspended for economic reasons. In March 2005 the mine restarted production and has been in continuous operation since. The mill throughput rate is approximately 20,000 tonnes per day (7.3 million tonnes per year). Mill tailings are discharged as slurry into the Tailings Storage Facility (TSF) located on the south area of the mine property. Figure 1.1 shows an aerial view of the site from 2012.

The starter dam for the TSF embankment was constructed in 1996 to a crest elevation of 927.0m. The starter dam was constructed out of a homogeneous compacted till fill. Beyond the starter dam the TSF embankment comprised compacted till as well as rockfill zones. The embankment was raised in subsequent years as follows:

- To elevation 934.0 m in 1997.
- To elevation 936.0 m in 1998.
- To elevation 937.0 m in 1999.
- To elevation 941.0 m in 2000.
- To elevation 942.5 m in 2001.
- To elevation 944.0 m in 2004.
- To elevation 946.0 m in 2005.
- To elevation 949.0 m in 2006.
- To elevation 950.9 m in 2007.
- To elevation 951.9 m in 2008.
- To elevation 953.9 m in 2009.
- To elevation 958.0 m in 2010.
- To elevation 960.1 m in 2011.

Construction of the Stage 8/8A dam raise began in May 2012 and was suspended in October 2012. The Stage 8/8A raise entailed a raise of approximately 3.4 m from approximately El. 960.1 m to El. 963.5 m. The raise, with a minimum crest of El. 963.5 m (Zone S) is projected to provide storage and freeboard through to summer 2013. The next dam raise is scheduled to be carried out in the spring/summer/fall of 2013.

Figure 1.1: Aerial View of Mount Polley Mine Site: 2012



1.2 Documentation Requirements

This report includes the relevant as-built information for the Stage 8/8A (2012) raise. The scope of this report includes the following:

- Description of the Stage 8/8A raise designs, and design modifications that were implemented during construction;
- Description of conditions encountered during construction;
- Inspection reports, field and laboratory test results including sample locations and test standards and/or methodologies;
- Description of the quality assurance and quality control (QA/QC) procedures and results;
- As-built drawings;
- Confirmation that the Stage 8/8A TSF construction was carried out in accordance with the design intent;
- Summary of instrumentation installed within the TSF; and
- Selection of construction photographs providing visual record of construction progress and condtions.

2.0 STAGE 8/8A DESIGN OVERVIEW

2.1 General

The Mount Polley TSF is comprised of one overall embankment that is approximately 4.5 km in length. The embankment is subdivided into three (3) sections; referred to as the Main Embankment, Perimeter Embankment and South Embankment. Heights vary along the embankment and are approximately 52 m, 34 m, and 25 m for the Main, Perimeter and South embankments, respectively.

2.2 2012 Dam Design

The 2012 construction schedule was initially planned to comprise the Stage 8 TSF embankment design raise target elevation of 963.5 m. At the request of MPMC during 2012 construction, the Stage 8A design was completed to allow for construction of the embankment to an elevation of 965 m. The decision by MPMC was made to continue raising the dam above El. 963.5 m during more favourable weather conditions in 2012 (as opposed to spring 2013). AMEC prepared a design package presenting the stability analyses and issued for construction drawings for the raise to El. 965 m which was submitted by MPMC to the British Columbia Ministry of Energy, Mines and Natural Gas (MEMNG) for approval.

The design of the Stage 8 raise has not changed from the previously approved and constructed Stage 7 raise design cross section, consisting of a downstream shell of NAG rockfill, a central, low permeability till core and a filter sequence downstream of the core. However, the design of the Stage 8A raise included the modification from the modified (upstream) centreline design to a centreline design above El. 963.5 m. Details of the Stage 8 and 8A designs are found in Drawings 2012AB.02 – 2012AB.06.

Both Stage 8 and 8A raises maintain a downstream slope of 1.3H:1V, which is temporary as the final dam downstream slope will be flattened as constructed. The NAG rockfill (Zone C) in the dam shell was placed and compacted by dozer and haul truck traffic. Transition material (Zone T) was obtained either on site crushing of run-of-mine waste rock or by selectively sorting run-of-mine waste rock. Sand and gravel filter material (Zone F) was processed by on site crushing of run-of-mine waste rock. Till core fill (Zone S) was obtained from a locally borrowed, low permeability glacial till. Total tailings (Zone U) are deposited into the impoundment and, in combination with run-of-mine waste rock placement, provide upstream support for the embankments, progressively raised in a modified centreline (up to El. 963.5 m) to centreline configuration (above El.963.5 m).

3.0 CONSTRUCTION MONITORING PROGRAM

3.1 Responsibilities for Construction Monitoring

Construction monitoring during the 2012 construction season was mainly carried out by MPMC personnel. AMEC's Support Engineer reviewed daily construction records and performed regular site visits to monitor the quality of construction and assess MPMC's monitoring of the construction.

3.1.1 AMEC Support Engineer

While on site the responsibilities of AMEC's Support Engineer were as follows:

- Monitor, train, and assist MPMC personnel with the requirements of construction monitoring;
- Monitor, sample, and requisition tests of the borrow areas, as required;
- Monitor and perform QA testing of compacted till core soils, as required;
- Review and approval of proposed borrow soils;
- Review and approval of transition and filter material, processing methodology and monitoring practices;
- Monitor and approve the drainage ditch excavation and preparation;
- Monitor and approve abutment preparation;
- Address any concerns or out-of-compliance situations observed and recorded during construction;
- Carry out the quality control field and laboratory testing;
- Direct the MPMC personnel to address the survey requirements, results, etc.; and
- Meet as required with MPMC to review the construction program.

AMEC's Support Engineer provided on-site supervision during the following periods:

- May Site Visit: May 14 to May 18, May 29 to June 1
- June Site Visit: June 25 to June 28
- July Site Visit: July 3 to July 6, July 9 to July 13, July 16 to July 18, July 25 to July 29
- August Site Visit: August 13 to August 15, August 28 to August 29
- September Site Visit: September 20 to September 21
- October Site Visit: October 25

While in the office the responsibilities of AMEC's Support Engineer were as follows:

- Review daily construction reports submitted by MPMC personnel;
- Review compaction results submitted by MPMC personnel;
- Plot and review instrumentation readings submitted by MPMC personnel;
- Address any concerns or out-of-compliance situations noted by MPMC personnel; and
- Coordinate with MPMC personnel and AMEC's Project Manager/Senior Engineer.

3.1.2 AMEC Senior Support

AMEC's Senior Support Engineer performed a site visit on August 13 to 14. In general, the purpose of the site visit was to view the construction activities, liaise with MPMC project personnel and discuss any issues with the TSF.

3.1.3 MPMC Field Inspector

MPMC Field Inspectors were responsible for the following:

- Monitor and maintain a photographic record of ongoing construction activities;
- Review borrow pit material to verify material consistency;
- Delineate embankment zones with stakes (every 25 m to 50 m);
- Perform QC compaction testing of placed Zone S material (as per material placement specifications);
- Collect material samples for QC laboratory testing;
- Perform on-site laboratory testing on Zone F and T materials;
- Conduct as-built surveys of various zones;
- Prepare and submit daily construction reports;
- Collect and submit instrumentation data; and
- Report out-of-compliance situations to AMEC's Support Engineer.

Examples of daily construction reports prepared during the construction season are presented in Appendix C.

3.2 QA/QC Testing

A summary of the testing requirements is given in Table 3.1.

Table 3.1: Embankment Material Types and QA/QC Testing Requirements

Material Type	On-Site Testing	Off-Site Testing	Sample Collection Schedule
Zone S Till Core	Source Classification: Visual inspection of borrow material. In-Place Testing: Visual inspection of zone dimension, and material. ND Density Testing (D6938-10) MDI Density Testing (D680-05) Moisture Content (D4318-10)	Source Classification and In-Place Testing : Proctor (D698-07 / D4718-07) Atterberg (D421-07 / D4318-10) Hydrometer Gradation (D421-07 and D422-07) Sieve Gradation (D6913-09)	Source Classification : One (1) per biweekly per source or One (1) per 10,000 m^3 per source In-Place Testing: One (1) per offset biweekly per source or one (1) per 6,500 linear meters per source Moisture Content: One (1) per 1000 linear meters per lift per day
Zone F Filter	During Production/Transportation: Wash Sieve Gradation (C117-04 and C136-06) During Placement: Visual inspection of material size, compaction, preparation, and zone dimension. Wash Sieve Gradation (C117-04 and C136-06)	During Production/Transportation: Wash Sieve Gradation (C117-04 and C136-06) In-Place Testing: Wash Sieve Gradation (C117-04 and C136-06)	During Production/Transportation: One (1) per 5,000 m^3 per stockpile A duplicate sample for off-site testing one (1) per stockpile In-Place Testing: One (1) per placement event or one (1) per 2,500 linear meters A duplicate sample for off-site testing one (1) per 4,500 linear meters
Zone T Transition	In-Place Testing: Wash Sieve Gradation (C117-04 and C136-06) Confirmation of waste rock inertness, as required. Visual inspection of material size, compaction, preparation, and zone dimension.	In-Place Testing: Wash Sieve Gradation (C117-04 and C136-06)	In-Place Testing: One (1) per 5,000 m^3 material placed. A duplicate sample for off-site testing one (1) per 10,000 m^3
Zone C Rockfill	Confirmation of waste rock inertness, as required. Visual in-place inspection of material size, preparation, and placement.	Not Applicable	Not Applicable

3.3 Instrumentation Monitoring

MPMC personnel are responsible for monitoring both vibrating wire piezometers and inclinometers located within the TSF. During the 2012 construction period, the instrumentation was generally read once every two weeks with inclinometers readings offset a week from the piezometer readings.

For the period prior to and after the 2012 construction period through the end of 2012, instrumentation monitoring was reduced to readings once a month.

4.0 TSF EMBANKMENT - STAGE 8/8A CONSTRUCTION OVERVIEW

4.1 General

Construction of the Stage 8/8A raise entailed a raise of approximately 3.4 m from approximate El. 960.1 m to a minimum crest El. 963.5 m. Till core (Zone S) placement took place between May 30 and October 26, 2012. The following subsections provide a brief summary of the 2012 construction activities for the TSF.

Drawing 2012AB.01 provides a general mine layout and the location of the borrow sources used in the Stage 8/8A construction. Drawing 2012AB.02 shows the as-built embankment in plan view while drawings 2012AB.03 through 2012AB.05 show the as-built sections of the embankment in relation to the design.

Throughout the report, references to specific photographs are listed to better illustrate given details about the embankment construction process. In each case, the photograph will be noted by a number; the photographs are presented in Appendix A.

4.2 Foundation Preparation

Foundation preparation of the abutments was carried out in accordance with the guidelines outlined in AMEC's 2012 Construction Monitoring Manual (AMEC 2012b). Preparation was conducted on the South and Perimeter abutments prior to fill placement and consisted of the following:

- **Removal of overburden** – Areas within the dam footprint and 2 m beyond, were stripped and cleared of organic material, loose or soft soils and deleterious material (including previously placed waste rockfill).

- **Test pitting** – Prior to cutoff trench construction, excavation of two test pits were performed (one at each the south and perimeter abutments) to confirm that a minimum of 2 m depth of native till was present beneath the embankment core limits. The test pits were completed downstream of the core limits such that the existing soils under the till core contact were not compromised. Bedrock was not encountered in either of the test pits. (see Photos 1 and 2)

- **Drainage ditch construction** – Foundation drains are installed within the downstream embankment foundation to improve foundation conditions and enhance surface dewatering. Construction of a drainage ditch to extend the foundation drains was performed along the Perimeter and South Embankments downstream of the abutment core extensions. As-built ditch dimensions were generally 0.6 to 1.0 m deep with a 2.0 m minimum base width. (see Photo 5) At the South Embankment the existing corrugated drainage pipe was extended, placing the pipe along the base of the ditch. In the area of abutment preparation at the Perimeter Embankment (approx. Stn. 4+800), only the drainage ditch was extended up the abutment, as there was no existing pipe to extend. Upon approval from the AMEC Support Engineer, the ditches were then backfilled with filter material (Zone F).

- **Drainage Blanket construction** – To promote drainage underneath the embankments, a drainage blanket is located along the base of the embankment, overlying the approved overburden. Prior to the extension of the drainage blanket along the South and Perimeter abutments, proof-rolling of the exposed native abutment material was completed using a 10 ton vibratory smooth drum compactor. The drainage blanket was constructed by placing a minimum lift thickness of approximately 0.6 m (Zone F material) in a single lift starting from the drainage ditch and extending to the embankment downstream shell limits. Thickness of the blanket lift was verified by hand digging a number of test pits in randomly selected locations. (see Photos 3 and 4)

4.3 Fill Placement

4.3.1 Zone U – Upstream Shell

Upstream support for the raising of the TSF embankment is provided by NAG tailings. The majority of the upstream shell comprised end of pipe spigotted tailings, utilizing cells, reworked with a dozer to achieve proper distribution, provide compaction and expedite excess water drainage. (see Photo 14) Further shaping of Zone U confining berms was done with the aid of an excavator. The majority of this work was carried out without AMEC supervision. Where the tailings could not be used for shell construction due to pipeline and pumping limitations, NAG run-of-mine waste rock was brought to the TSF by haul truck and placed/shaped by excavators and dozers. Specifically, NAG waste rock was substituted for use as Zone U along the Perimeter Embankment between Corner 1 and Corner 2 and along the central portion of the Main Embankment between Corner 2 and Corner 3. Waste rock used along the Perimeter Embankment was done by combining the placement of both tailings and NAG waste rock, and was completed proactively to prevent tailings beach erosion. Prior to Zone S placement downstream of Zone U, AMEC's Support Engineer inspected the NAG waste rock that had been used as Zone U to ensure that large boulders (diameter > 1 m) did not exist near the Zone U/Zone S interface.

4.3.2 Zone S – Till Core

All of the till fill core material used in the 2012 construction of the TSF embankment was obtained from the Perimeter Borrow. The borrow was located downstream of the Perimeter Embankment between Corner 1 and Corner 1.5. (see Photos 6, 21, and 23)

The placement of Zone S material was performed by Peterson and generally followed the methodology outlined below:

- Prior to placement of the first lift of till core during 2012, the existing till (Zone S and native till on the abutments) was prepared by proof-rolling with a 10 ton vibratory smooth drum roller. Areas that were noted to be soft or affected by the frost were removed and replaced with approved Zone S material.

- The top 0.1 m of the prepared surface was scarified with the aid of a dozer/grader, to promote bonding between successive lifts. (see Photo 7)

- The surface was moisture conditioned as required to further promote proper bonding of successive till lifts. (see Photo 11)

- The till fill was end dumped by articulated haul trucks and spread into 0.3 m thick lifts with a dozer. (see Photo 12)

- Compaction of the till was primarily achieved using a 10 ton smooth drum vibratory compactor, with additional compaction performed occasionally by articulated haul truck traffic.

- On average, for every two to three lifts placed, the downstream face of the till was trimmed and shaped by an excavator to maintain design lines. (see Photo 15)

4.3.3 Zone F – NAG Filter Rock

The material utilized for Zone F sand and gravel filter was crushed on site at the primary crusher. Haul trucks were used to transport and stockpile the material around the TSF embankment for use in construction. Drawing 2012AB.02 illustrates the stockpile locations used during the 2012 construction.

Prior to placement of Zone F material, the previously placed filter material was exposed to ensure vertical continuity of the filter. This was carried out by excavator in concert with the downstream limits trimming process of the till core. (see Photo 16) The filter material was then placed in 0.6 m lifts against the trimmed downstream limits of the till core. The material was transported by dump trucks and spread/shaped with the aid of an excavator, grader, or loader. (see Photo 17)

The placed Zone F material was lightly compacted in conjunction with Zone T material, by 10 ton smooth drum compactor and haul truck trafficking.

4.3.4 Zone T – Transition NAG Rock

The material utilized for Zone T was either crushed on site and transported to the embankment or selectively placed from suitable run-of-mine waste rock as required. Zone T material was hauled and placed by MPMC in 0.6 m to 1.2 m thick lifts with the aid of a loader and grader. Prior to placement of the Zone T material, the interface between the lifts was exposed and/or scarified to remove any smooth, pavement like surfaces.

The compaction of the transition material was achieved with a 10 ton smooth drum compactor and haul truck trafficking.

4.3.5 Zone C – Downstream Shell NAG Rock

The Zone C downstream rockfill shell was constructed with NAG rockfill obtained from the Springer pit. Prior to placement, the surface was scarified with the aid of a grader/dozer in areas where smooth, pavement like surfaces had developed. The scarification was performed to avoid continuous, low hydraulic conductivity zones within the rockfill shell, thus promoting downward drainage through the rockfill. The NAG rock was transported from active mining areas to the embankment via haul truck and placed and spread by dozers.

4.4 Survey Control

Survey control requirements for the 2012 construction of the TSF included the following:

- Establishing and maintaining upstream and downstream limits of Zone S (the stakes were generally placed every 25 to 50 m along the entire length of the embankment, as requested by Peterson);
- Maintaining the downstream crest chainage during construction;
- Verifying that a 5 m till core width was maintained during construction;
- Establishing and verifying the Zone F/T transition line for placement of Zone T material;
- Conducting spot checks to confirm that the minimum width of Zone F and Zone T were achieved;
- Surveying the location and elevation of in-situ density tests;
- Collecting and storing data as required for the as-built record; and
- Providing location and elevation data as required by the AMEC Support Engineer.

MPMC personnel performed the survey control described above for the 2012 construction season.

4.5 Quality Control and Quality Assurance Testing

QA/QC testing of the fills used in the construction of the embankment involved on-site and off-site tests. On-site testing included in-situ nuclear densometer tests (ASTM D6938-10) to confirm adequate compaction of the till fills placed. Sieve analyses of the Zone F filter material to assess particle size gradation (ASTM D-422-63) were also performed on-site to confirm adequate compliance to specifications.

Off-site testing of the fills included Standard Proctor Density (SPD) tests (ASTM D-698) that provided reference values used in the field to assess whether the compacted fill had achieved the 95% SPD in the design specifications. Tests of the fill material particle size gradation (ASTM D-422-63) were performed to assess whether the fill material satisfied the design specifications. Testing of the core materials Atterberg limits (ASTM D-4318-98) were also performed. The results of these tests are presented in Appendix B.

During the 2012 construction season, the testing frequencies as outlined in Section 3.2 were generally maintained. A summary of the as-built material quantities as well as all QA/QC testing performed on the fills is provided in Table 4.1.

Table 4.1: TSF Summary of As-built Material Quantities and Laboratory testing

Material Type	Source Of Material	Volume Placed (m^3)	QA/QC Tests Performed
Zone C – Downstream Shell NAG Rock	Springer Pit (ROM)*	297,995	Visual
Zone T – Transition NAG Rock	Springer Pit (Road Crush product)		2 Gradations (MPMC) 1 Gradations (AMEC)
Zone F – NAG Filter Rock	Springer Pit (Filter Crush)	28,165	11 Gradations (MPMC) 4 Gradations (AMEC)
Zone S - Till Core	Perimeter Borrow	109,095	15 Proctor 18 Gradation 18 Atterberg limits 20 QA ND field density (AMEC) 778 QC ND field density(MPMC) 36 Laboratory Moisture tests
	Total Fill Volume Placed	**435,255**	

*Run of mine material (no processing required)

4.5.1 Zone S – Till Core

In 2012, till placed on the embankment was obtained from the perimeter borrow pit, located downstream of the Perimeter Embankment between Corner 1 and Corner 1.5. Till material found in the borrow pit was generally within the specification and was classified as a low plasticity Sandy Silt, some clay with some to trace gravel.

A glaciolacustrine unit was encountered interbedded within the till in some areas of the borrow pit. The glaciolacustrine material typically met the core material specification, however due to its poor workability, this material was wasted or whenever possible, intermixed with approved till in a ratio of one part glaciolacustrine and two parts till.

The in-situ density and moisture content of the compacted till were determined using a nuclear densometer (ASTM D6938-10). (see Photo 18) Where field test results indicated that the specified 95% Standard Proctor Maximum Dry Density (SPMDD) was not achieved, the area was re-compacted and re-tested until satisfactory results were achieved. Samples of till were also collected and periodically sent to AMEC's Prince George lab facility for geotechnical index testing.

The SPMDD value used in the field was selected from the first SPMDD (2094 kg/m^3) lab result for the 2012 construction season and adjusted as necessary based on observations of the soil. The average of the SPMDD lab results over the 2012 construction season was 2055 kg/m^3.

In general, the fills achieved 95% SPMDD. Test results were recorded and entered into a spreadsheet. Plots of the test results were prepared and are presented in Appendix B.

4.5.2 Zone F – NAG Filter Rock

Filter Zone F was produced by running run-of-mine NAG waste rock through the mill crusher. The majority of the material placed in the embankment was fairly consistent, plotting within the accepted filter design criterion. Approximately half of the on-site tested samples plotted slightly to the coarse side of the specified envelope for the finer range of sizes (D_{15} to D_{30}), as indicated on the grain size analyses curves shown in Appendix B. This slight deviation from the gradation specification could be due to inexperienced MPMC lab testing personnel and/or segregation of the material during transportation and placement. Generally, based on the visual assessments as well as the laboratory testing results, the Zone F material was judged an acceptable filter for the Zone S material.

4.5.3 Zone T – Transition Zone

Transition Zone T was produced by running run-of-mine NAG waste rock through the mill crusher in addition to suitable run-of-mine material from the Springer Pit. Visual inspections of the Zones F and T interface indicated acceptable filter compatibility. Routine visual assessments were carried out during construction to determine qualitatively the conformance of Zone T transition to the gradation specifications and its acceptability as a filter for Zone F filter rock. Based on the visual assessments, the Zone T was judged an acceptable filter for the Zone F. Sieve analyses were also conducted on samples of the Zone T and results are presented in Appendix B.

4.5.4 Zone C – Downstream Shell NAG Rock

The Zone C downstream rockfill shell was constructed with NAG rockfill obtained from the Springer Pit. The Zone C gradation specifications call for a well-graded rockfill with a maximum diameter of 1 m. Routine visual assessments were carried out by MPMC during construction to determine qualitatively the conformance of Zone C transition to the gradation specifications and its acceptability as a filter for Zone T filter rock. Based on the visual assessments, the Zone C material was judged an acceptable filter for the Zone T material.

4.6 Conformance of 2012 Construction with Design Intent

In general, the 2012 Stage 8/8A raise of the embankment is judged to have been carried out in conformance with design intent. This conclusion is based on AMEC's periodic observations of the construction, review of reports prepared by MPMC when AMEC was not on site, and the review of QA/QC records.

However, there are two items which are currently out of compliance with original design intent but do not pose any immediate concerns to embankment stability or overall function. The items listed below are to be corrected prior to the 2013 construction season:

- **Zone F & Zone T elevation**: Zones F and T are at elevations lower than the Zone S elevation in each of the three embankments. As-built elevations recorded after the suspension of construction in 2012 were provided to AMEC by MPMC. The elevations indicated that the difference between the Zone S and Zone T/F lifts was approximately 1 m, 0.5 m and 0.9 m in the Perimeter, Main and South embankments, respectively. Maintenance of the Zones F and T above the tailings/pond level is part of the TSF

design requirements. MPMC was made aware that the elevation of the tailings pond is to be closely monitored, raising the level of the filter and transition materials as necessary.

- **Zone S width**: In several areas (approximately 800 m in total length) of the Main and Perimeter embankments the till core width was found to be less than the minimum design width of 5.0 m based on inspection of the field surveys. The upstream limits of the till core were found to deviate inwards in some areas by about 0.5 m to 1.0 m. (see Photo 24) The downstream limits were placed within the specified construction tolerances in order to maintain continuity and integrity of the filter and transition zones.

  The design deviation was discussed with MPMC project personnel. Prior to commencement of the 2013 construction season, the existing core is to be surveyed and clearly marked in the locations that are less than required 5 m width. In these marked areas, the core will need to be widened in the upstream direction by completing the following:

  - *Step 1*: Clear the area extending from the existing upstream till core to approximately 1.5 m upstream of the surveyed core limits, making sure to remove all loose, dry material that is inconsistent with approved Zone S.

  - *Step 2:* In the prepared areas (Step 1), excavate a trench that extends approximately 0.6 m downstream of the existing upstream core limits, to a minimum of 2.5 m upstream of that point (i.e. within the Zone U). The depth of trench shall extend a minimum of 0.6 m or until survey confirms that the upstream till design limits are satisfied. The trench shall have a minimum width of 1 m at its base and side slopes of 1H:1V, which are recommended to ensure proper tie-in and compaction are achieved.

  - *Step 3:* Within the approved trench, approved till fill material shall be placed in loose lifts of 0.3 m and compacted to 95% SPD. If compaction cannot be achieved using normal compactive methods (i.e. smooth drum roller), then compaction of thin till lifts with a walk-behind or plate-tamping compactor, or tamping with a hoe bucket may be required.

In general, the repair of the Zone S core (i.e. trench excavation, till core placement and compaction) shall be completed at the direction of the AMEC Support Engineer.

5.0 INSTRUMENTATION MONITORING

5.1 General

Instrumentation in the TSF consists of slope inclinometers (SI) and vibrating wire piezometers (VW). The as-built locations of the inclinometers and piezometers (organised by planes) is shown in plan view on Drawing 2012AB.07.

5.2 Piezometers

A total of eighty (80) functioning vibrating wire piezometers have been installed along the embankments in ten planes, designated as planes A to K (excluding H). The planes are located in the embankments as follows:

- Perimeter Embankment: G, D, J;
- Main Embankment: K, B, A, C, E; and
- South embankment: I, F.

The vibrating wires were installed into various areas within the embankments including the dam foundation soils, tailings, upstream fills, Zone F, Zone S and in various embankment drains.

5.3 Slope Inclinometers

A total of eight (7) slope inclinometers have been installed and are functioning in the TSF, one (1) in the Perimeter embankment and seven (6) in the Main embankment. The inclinometers are generally located at the downstream toe of the embankments within the foundation soils and extend to depths of approximately 12 to 48 meters below original ground surface.

5.4 New Instrumentation

In late 2012, readings from an inclinometer located downstream of the Perimeter embankment (SI11-04) showed compression failure deformation consistent with settlement at depths from ground surface to 15 m below ground surface. AMEC recommended that additional instrumentation be installed, as the SI11-04 would likely cease functioning due to the deformation. Upon the approval of MPMC, a site investigation program was initiated (in conjunction with an AMEC water well drilling program) and consisted of the installation of two (2) slope inclinometers along the downstream toe of the Perimeter embankment. The first inclinometer (SI12-01) was installed using a larger diameter casing with compression fittings. It is located directly adjacent SI11-04. The second inclinometer (SI12-02) is installed adjacent the location of vibrating wire J1. Locations of the inclinometers are shown in plan on Drawing 2012AB.07. The new slope inclinometers have been initialised with their first reading taking place on March 6, 2013.

6.0 WORKS TO BE COMPLETED

There are a number of outstanding tasks pertaining to the ongoing development of the tailings storage facility. These tasks are important to the proper completion of the development of the tailings embankment and AMEC is to be updated on their progress. These tasks include, but are not limited to:

- *Placement of the downstream filter and transition materials (Zones F and T)*: Zone F and T placement on the Perimeter, Main and South embankments to the minimum crest elevation of 963.5 m needs to be completed prior to the pond elevation reaching 963.5 m and/or the commencement of the 2013 construction period.

- *Repair of the till core (Zone S)*: Construction of the till core needs to be completed in the areas where survey indicates the width to be less than the minimum design width of 5.0 m.

- *Instrumentation monitoring:* Monitoring of all TSF instrumentation needs to continue at the recommended intervals outlined in the 2012 Construction Monitoring Manual (AMEC 2012b). Specifically, the two newest inclinometer installations will need to be closely monitored to ensure that they are accurately functioning after initialization.

7.0 REPORT CLOSURE

This report has been prepared for the exclusive use of MPMC for specific application to the area within this report. Any use which a third party makes of this report, or any reliance on or decisions made based on it, are the responsibility of such third parties. AMEC accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report. It has been prepared in accordance with generally accepted geotechnical and tailings dam engineering practices. No other warranty, expressed or implied, is made.

Respectfully submitted,

AMEC Environment & Infrastructure,
a division of AMEC Americas Limited

Reviewed by:

Original paper copies signed by
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Steve Rice, P.Eng.
Principal Engineer

Original paper copies signed and
sealed by Laura Wiebe, P.Eng.

Laura Wiebe, P.Eng.
Project Engineer

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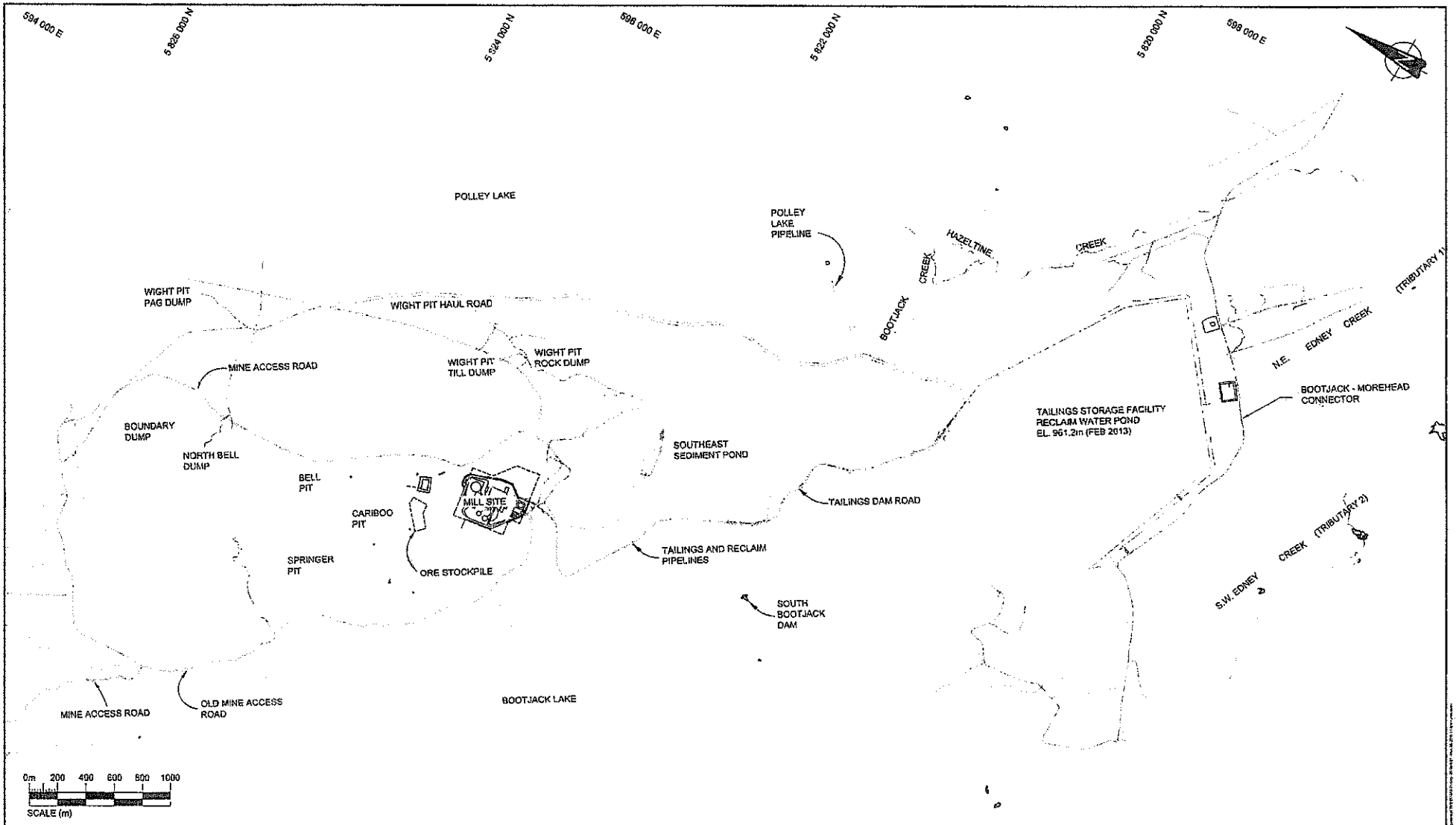
DRAWINGS



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Client Logo:

Client: MOUNT POLLEY MINING CORPORATION

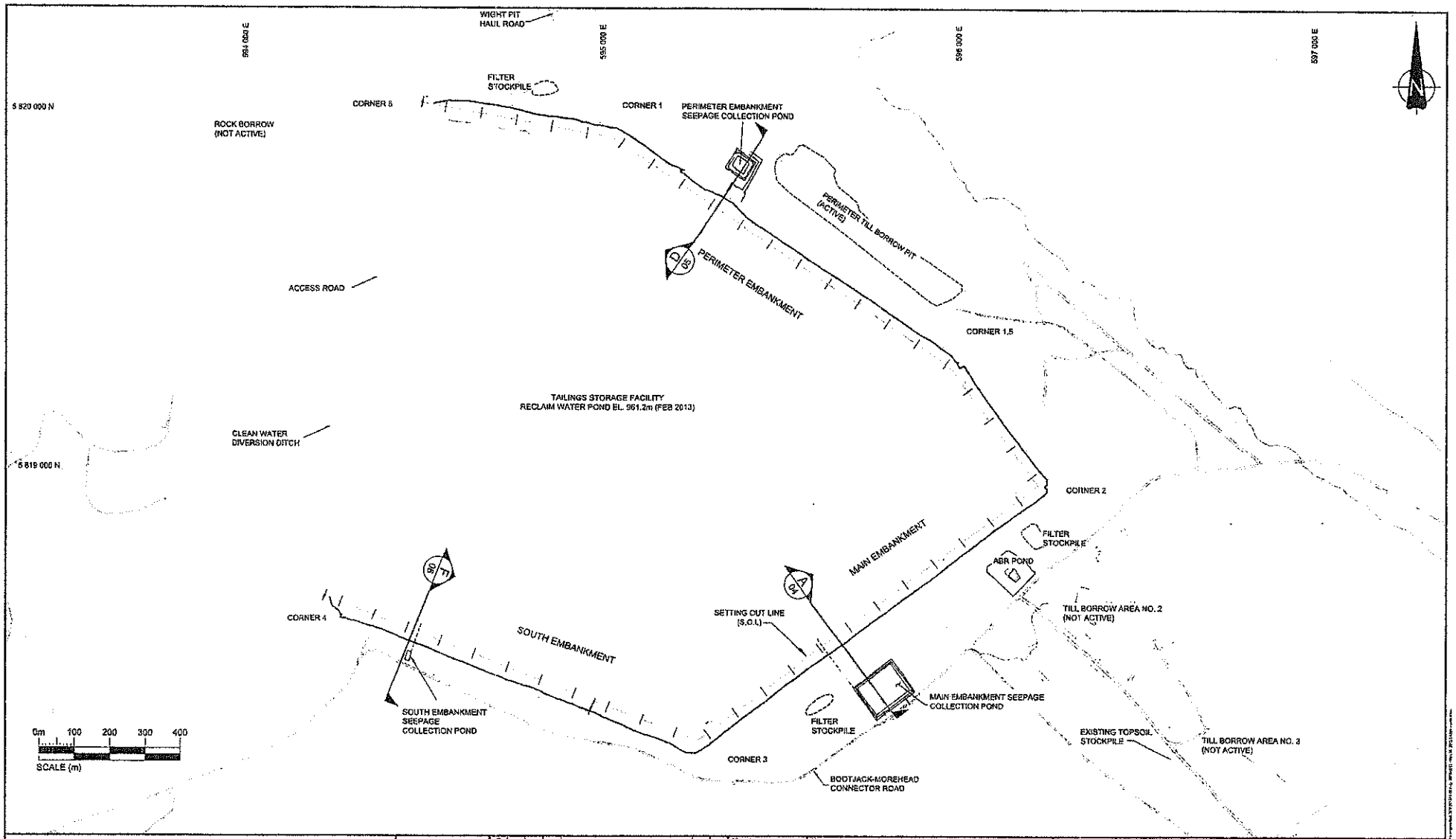
AMEC Environment & Infrastructure

DATUM: NAD 83
PROJECTION: UTM ZONE 10
DRAWN BY: VC
REVIEW BY: BR
ORIGINAL SCALE: AS SHOWN

PROJECT: MOUNT POLLEY MINE TAILINGS STORAGE FACILITY 2012 AS-BUILT REPORT

TITLE: GENERAL SITE PLAN

PROJECT NO: VM00580A
REVISION NO: 0
DATE: MARCH 2013
DRAWING NO: 2012AB.01
SHEET NO: 1 of 1



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Client: MOUNT POLLEY MINING CORPORATION

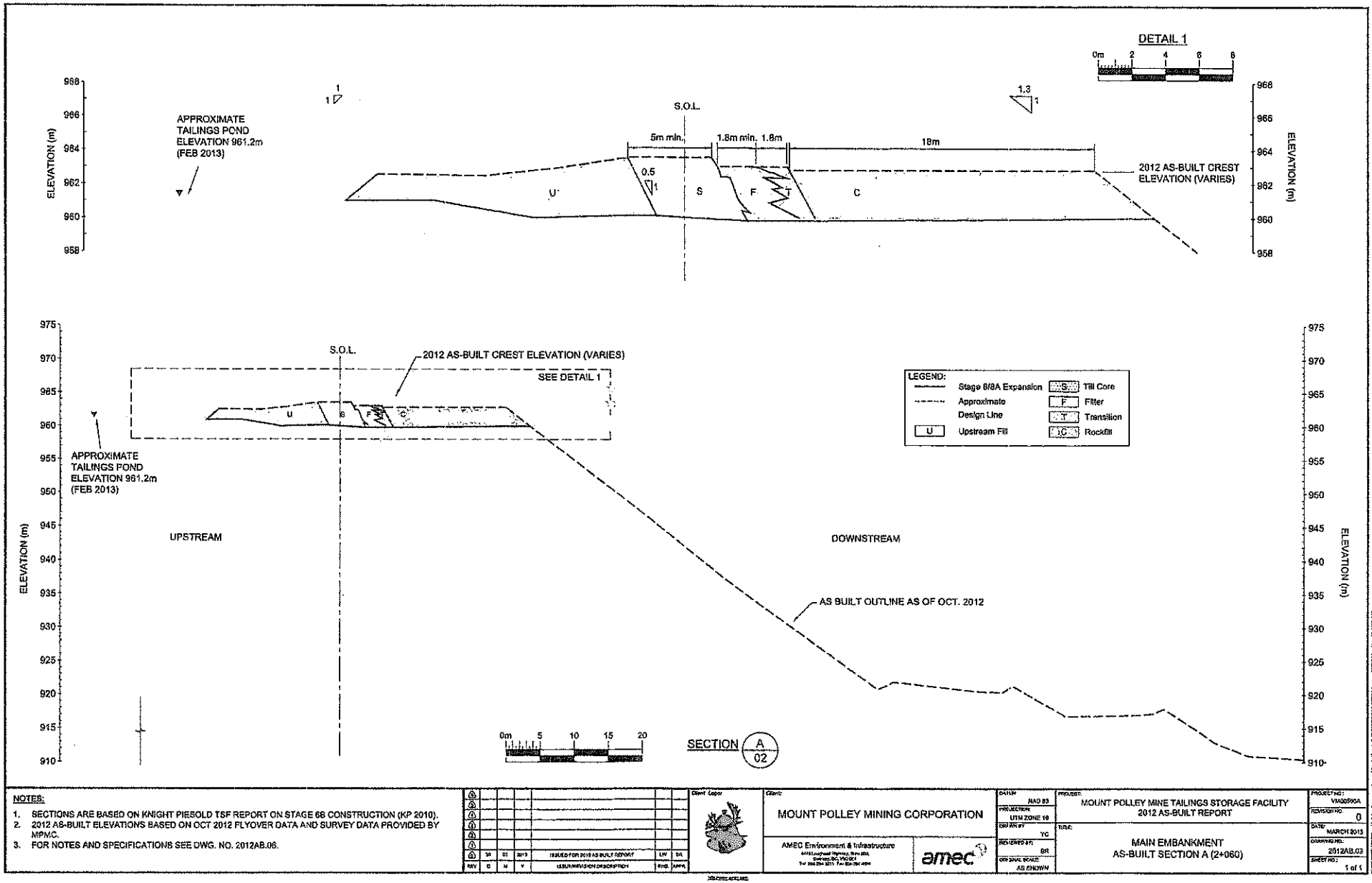
AMEC Environment & Infrastructure

DATUM: NAD 83
PROJECTION: UTM ZONE 10
DRAWN BY: YC
REVIEWED BY: SR
ORIGINAL SCALE: AS SHOWN

PROJECT: MOUNT POLLEY MINE TAILINGS STORAGE FACILITY 2012 AS-BUILT REPORT

TITLE: AS-BUILT PLAN VIEW

PROJECT NO.: VM00560A
REVISION NO.: 0
DATE: MARCH 2013
DRAWING NO.: 2012AB.02
SHEET NO.: 1 of 1



NOTES:

1. SECTIONS ARE BASED ON KNIGHT PIESOLD TSF REPORT ON STAGE 6B CONSTRUCTION (KP 2010).
2. 2012 AS-BUILT ELEVATIONS BASED ON OCT 2012 FLYOVER DATA AND SURVEY DATA PROVIDED BY MPMC.
3. FOR NOTES AND SPECIFICATIONS SEE DWG. NO. 2012AB.06.

REV	YR	MO	DY	ISSUE/REVISION DESCRIPTION	BY	APP'D
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Client Logo

Client: MOUNT POLLEY MINING CORPORATION

AMEC Environment & Infrastructure

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DATUM: NAD 83
PROJECTION: UTM ZONE 10
DRAWN BY: YC
REVIEWED BY: BR
ORIGINAL SCALE: AS SHOWN

PROJECT: MOUNT POLLEY MINE TAILINGS STORAGE FACILITY 2012 AS-BUILT REPORT

TITLE: MAIN EMBANKMENT AS-BUILT SECTION A (2+060)

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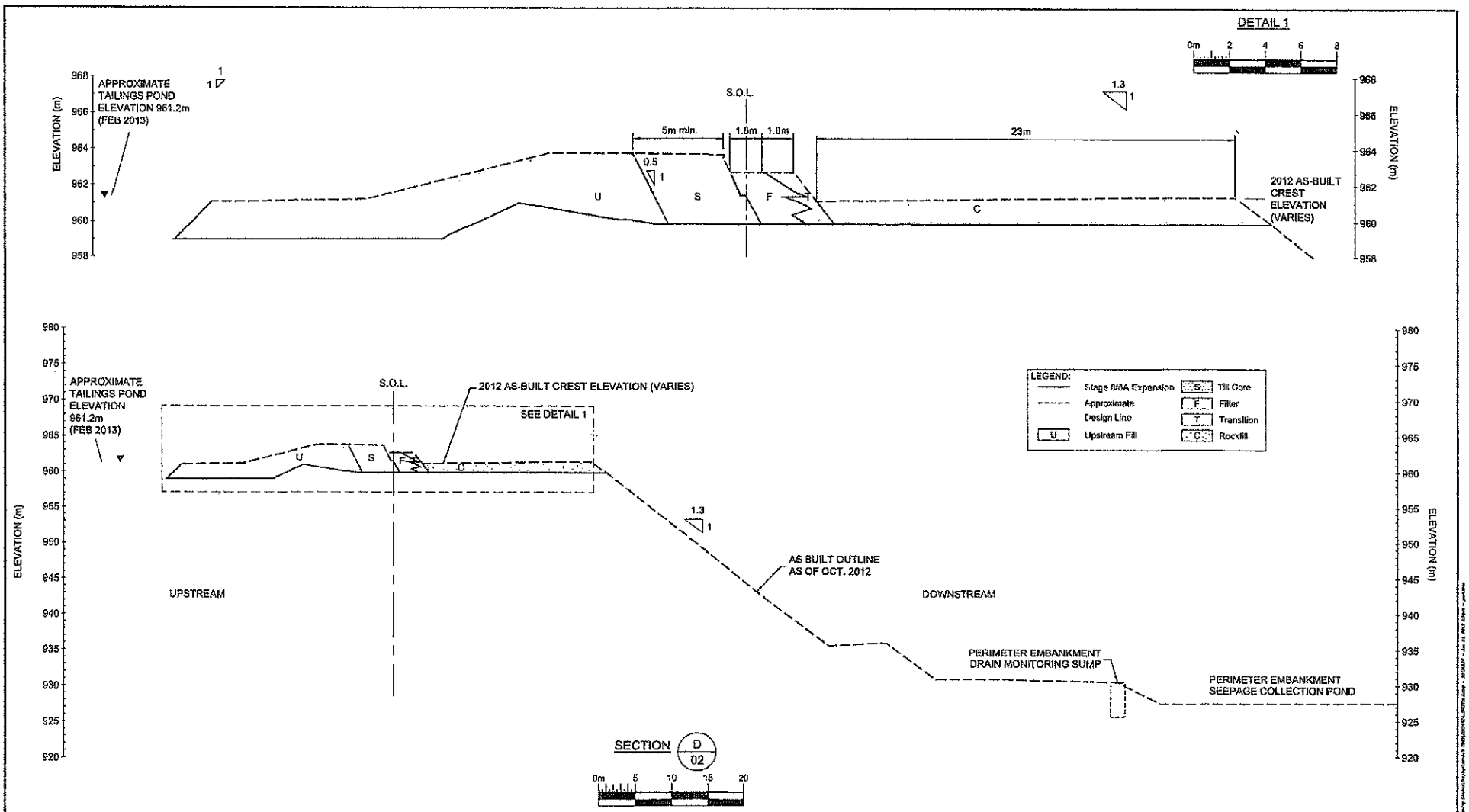
REVISION NO.: 0
DATE: MARCH 2013
DRAWING NO.: 2012AB.03
SHEET NO.: 1 of 1



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2. 2012 AS-BUILT ELEVATIONS BASED ON OCT 2012 FLYOVER DATA AND SURVEY DATA PROVIDED BY MPMC.
3. FOR NOTES AND SPECIFICATIONS SEE DWG. NO. 2012AB.06.

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Client: MOUNT POLLEY MINING CORPORATION

AMEC Environment & Infrastructure

DATUM: NAD 83
PROJECTION: UTM ZONE 10
DRAWN BY: YG
REVIEWED BY: SR
ORIGINAL SCALE: AS SHOWN

PROJECT: MOUNT POLLEY MINE TAILINGS STORAGE FACILITY 2012 AS-BUILT REPORT

TITLE: PERIMETER EMBANKMENT SECTION D (3+990)

PROJECT NO.: VM00560A
DESIGN NO.: 0
DATE: MARCH 2013
DRAWING NO.: 2012AB.04
SHEET NO.: 1 of 1

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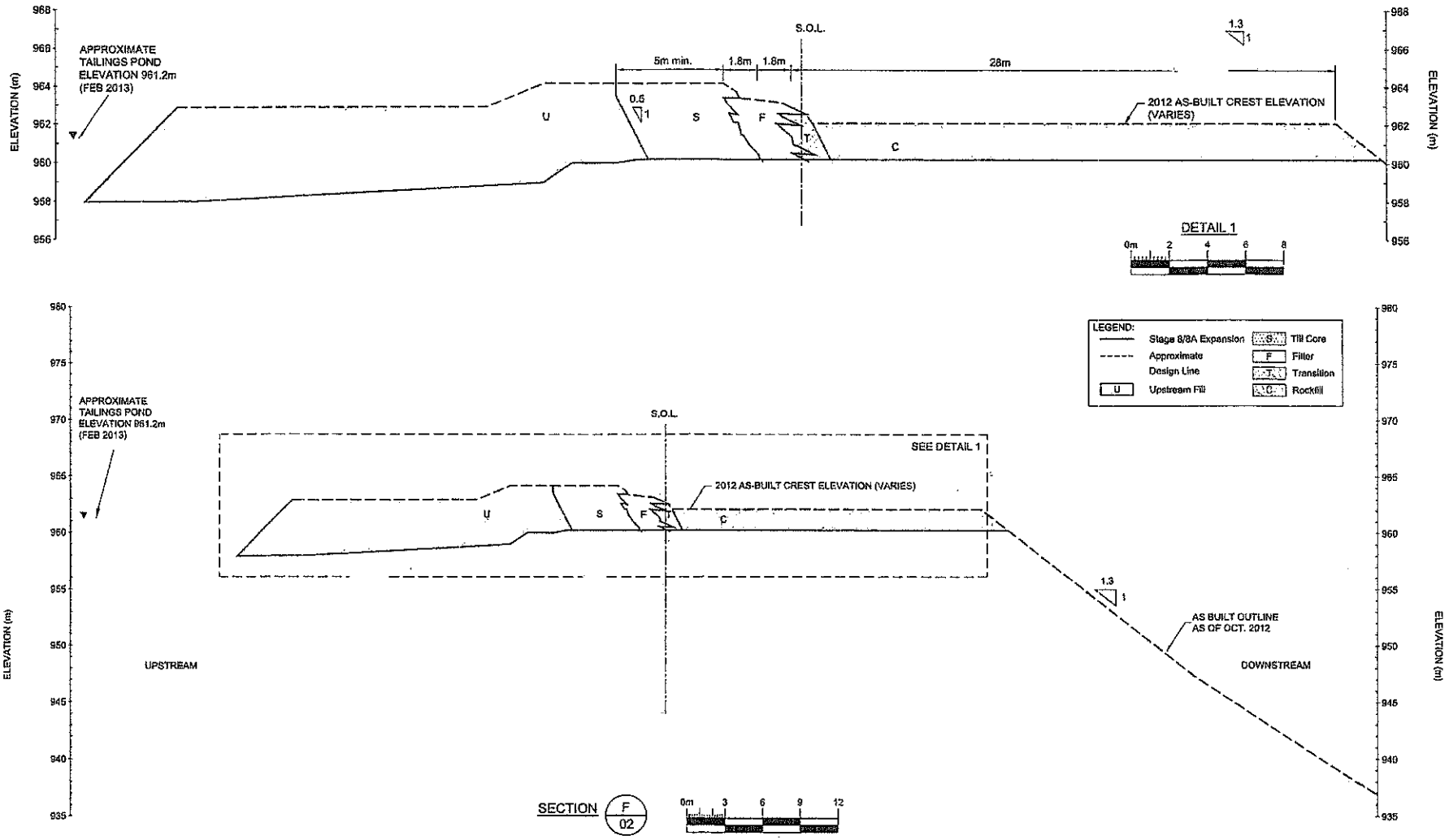

NOTES:

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2. 2012 AS-BUILT ELEVATIONS BASED ON OCT 2012 FLYOVER DATA AND SURVEY DATA PROVIDED BY MPMC.
3. FOR NOTES AND SPECIFICATIONS SEE DWG. NO. 2012AB.06.

REV	D	M	Y	ISSUE/REVISION DESCRIPTION	ENG.	APPR.
0	30	03	2013	ISSUED FOR 2012 AS BUILT REPORT	LW	GN

Client: MOUNT POLLEY MINING CORPORATION

AMEC Environment & Infrastructure

DATUM: NAD 83
PROJECTION: UTM ZONE 10
DRAWN BY: YC
REVIEWED BY: SR
ORIGINAL SCALE: AS SHOWN

PROJECT: MOUNT POLLEY MINE TAILINGS STORAGE FACILITY 2012 AS-BUILT REPORT

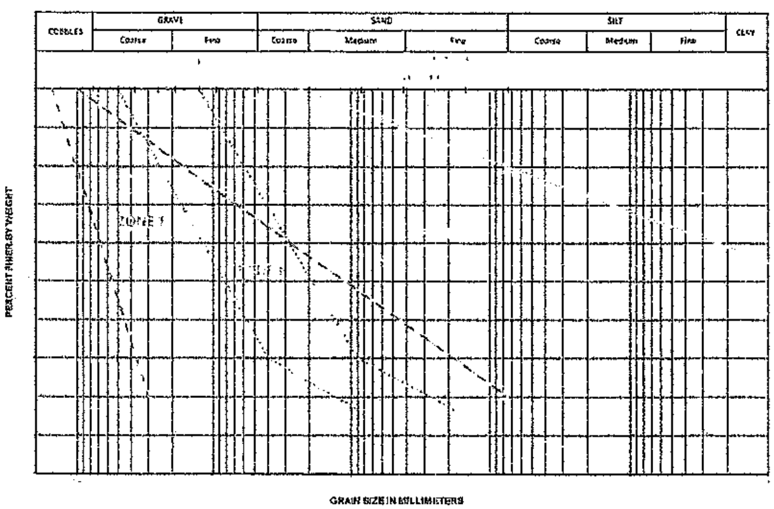
TITLE: SOUTH EMBANKMENT AS-BUILT SECTION F (0+720)

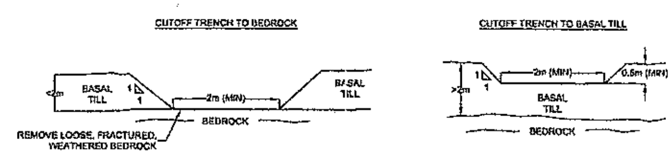
PROJECT NO.: VM00503A
REVISION NO.: 0
DATE: MARCH 2013
DRAWING NO.: 2012AB.05
SHEET NO.: 1 of 1

EMBANKMENT ZONE MATERIAL GRADATION AND PLACEMENT SPECIFICATIONS

EMBANKMENT ZONE	DESCRIPTION	MATERIAL TYPE	SPECIFICATIONS	SUBGRADE BASE PREPARATION	PLACEMENT AND COMPACTION	ON-SITE TESTING	OFF-SITE TESTING	SAMPLE COLLECTION SCHEDULE	SAMPLE SIZE
S	TILL CORE	GLACIAL TILL	Well graded to [illegible] (See Gradation Envelope below)	Strip all topsoil and organic material. Excavate cutoff trench as per detail (see Detail 1). Strip all frost softened and weakened soil, [illegible]	Place, moisture condition and spread in maximum 300mm loose lifts. [illegible] compaction to 95% of standard proctor maximum density. Density tested [illegible]	Source Classification: [illegible] In-Place Testing: [illegible] and material. ND Density Testing (D6938-10) Moisture Content (D4318-10)	Source Classification and In-Place Testing: Proctor (D698-07), (D4718-87); Atterberg (D4318-10); Hydrometer Gradation (D422-63 / D4221-11); Sieve Gradation (D6913-04)	Source Classification: One (1) per [illegible] per source or one (1) per 10,000 m³ per source. In-Place Testing: [illegible] Moisture Content: One (1) per [illegible] per day	Source Classification: Two (2) three-quarter (3/4) full five (5) gallon bucket, void of oversized rocks. In-Place Testing: Two (2) three-quarter (3/4) full five (5) gallon bucket, void of oversized rocks. Moisture Content: Minimum sample 700g
F	FILTER	SAND AND GRAVEL (NAG)	Sand and gravel sized material (See Gradation Envelope below)	Strip all frost softened and weakened soil. Expose previously placed material	Place and spread in maximum 500mm loose lifts. [illegible] compaction minimum of 4 passes [illegible] 10 ton smooth drum compactor	[illegible] Wash Sieve Gradation (C117-04 / C136-06). During Placement: [illegible] compaction, segregation and zone [illegible]. Wash Sieve Gradation (C117-04 / C136-06)	[illegible] Wash Sieve Gradation (C117-04 / C136-06). In-Place Testing: Wash Sieve Gradation (C117-04 / C136-06)	[illegible] A duplicate sample for off-site testing one (1) per stockpile. In-Place Testing: One (1) per [illegible] or one (1) per 2,400 linear meters. A duplicate sample for off-site testing one (1) per 4,800 linear meters	[illegible] One (1) three-quarter (3/4) full five (5) gallon bucket, void of oversized rocks. In-Place Testing: One (1) three-quarter (3/4) full five (5) gallon bucket, void of oversized rocks
T	TRANSITION	FINE ROCKFILL (NAG)	Cobble and gravel sized material (See Gradation Envelope below)	Strip all frost softened and weakened soil. Expose previously placed material	Place and spread in maximum 1,000mm loose lifts. Compacted by uniform routing of haul truck and spreading equipment	In-Place Testing: Wash Sieve Gradation (C117-04 / C136-06) 1 per 1,000 m³ material placed. Confirmation of waste rock chemistry as required. Visual inspection of material size, compaction, segregation and zone thickness	In-Place Testing: Wash Sieve Gradation (C117-04 / C136-06)	In-Place Testing: One (1) per [illegible] m³ of material placed. A duplicate sample for off-site testing one (1) per [illegible] m³	In-Place Testing: Three (3) three-quarter (3/4) full five (5) gallon bucket
	ROCKFILL	GENERAL ROCKFILL (NAG)	Specified as [illegible] maximum particle size	Strip all frost softened and weakened soil. Scarify previously placed material	Placed and spread in maximum 2,000mm loose lifts. Boulders [illegible] placed adjacent to the rock transition zone	Confirmation of waste rock chemistry as required. Visual in-place inspection of material size, compaction, and placement	Not Applicable	Not Applicable	Not Applicable
U	UPSTREAM FILL	SELECT FILL	[illegible] Constant monitoring of the [illegible] is needed to ensure [illegible] within the cell. If NAG waste rock is used, to be [illegible] maximum 0.5m diameter	Not Applicable	Placement and compaction requirements to be determined based on material [illegible]. If NAG waste rock is used, Place and spread in maximum 1,0[illegible]m loose lifts	Not Applicable	Not Applicable	Not Applicable	Not Applicable

EMBANKMENT ZONE MATERIAL GRADATION LIMITS





DETAIL 1 - CUTOFF TRENCH

NOTE:

1. THIS DRAWING TO BE READ IN CONJUNCTION WITH AMEC REPORT ENTITLED "TSF STAGE 6/6A 2012 AS-BUILT REPORT", DATED MARCH 2013.

REV	D	M	Y	ISSUE/REVISION DESCRIPTION	ENG	APPR
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Client Logo:

Client: MOUNT POLLEY MINING CORPORATION

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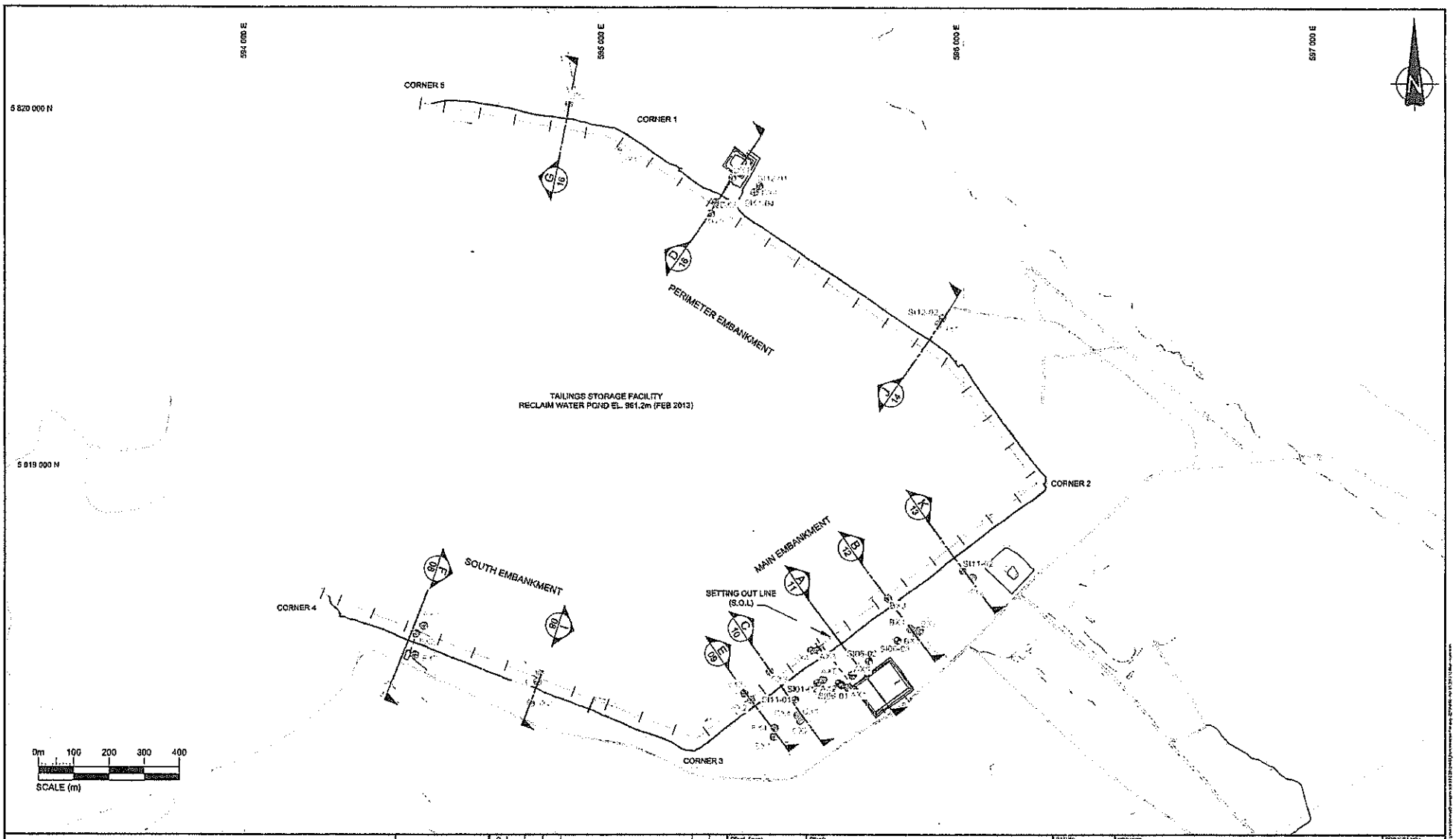
DATUM:	NAD 83
PROJECTION:	UTM ZONE 10
DRAWN BY:	YC
REVIEWED BY:	SR
ORIGINAL SCALE:	AS SHOWN

PROJECT: MOUNT POLLEY MINE TAILINGS STORAGE FACILITY 2012 AS-BUILT REPORT

TITLE: NOTES & SPECIFICATIONS

PROJECT NO.:	VM00560A
REVISION NO.:	0
DATE:	MARCH 2013
DRAWING NO.:	2012AB.05
SHEET NO.:	1 of 1



LEGEND:

- Vibrating Wire Location
- Slope Inclinometer Location
- 2012 Slope Inclinometer Location

REV	D	M	Y	ISSUE/REVISION DESCRIPTION	ENG.	APPR.
0	30	03	2013	ISSUED FOR 2012 AS-BUILT REPORT	LW	SR

Client: Teck

MOUNT POLLEY MINING CORPORATION

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DATUM: NAD 83
PROJECTION: UTM ZONE 10
DRAWN BY: YC
REVIEWED BY: SR
ORIGINAL SCALE: AS SHOWN

PROJECT: MOUNT POLLEY MINE TAILINGS STORAGE FACILITY 2012 AS-BUILT REPORT

TITLE: INSTRUMENTATION PLAN

PROJECT NO.: VM00560A
REVISION NO.: 0
DATE: MARCH 2013
DRAWING NO.: 2012AB.07
SHEET NO.: 1 of 1

APPENDIX A

2012 CONSTRUCTION SEASON PHOTOGRAPHS

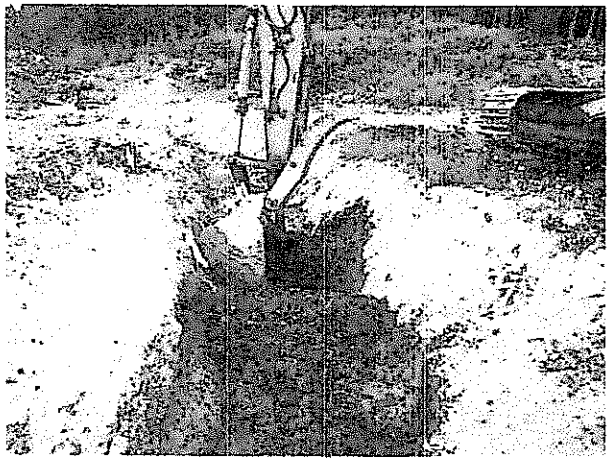


Photo 1: Test pit conducted in existing diversion trench near the south abutment.

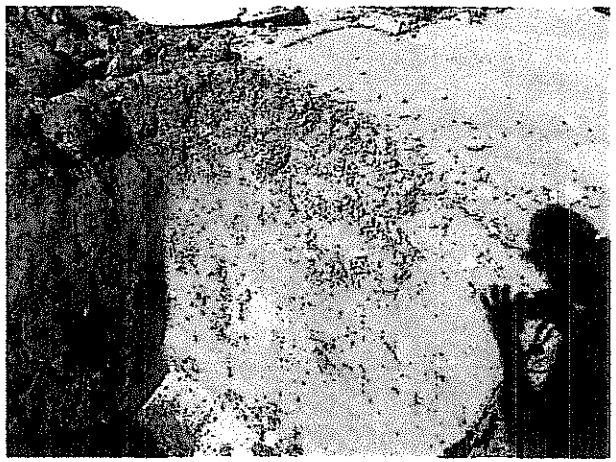


Photo 2: Test pit conducted at the Perimeter abutment.

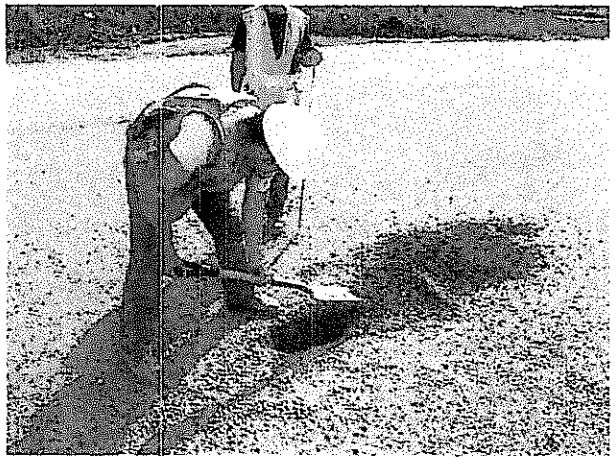


Photo 3: Test conducted at Perimeter abutment to verify filter blanket thickness.

Photo 4: Over view of the filter drainage blanket at the Perimeter abutment.

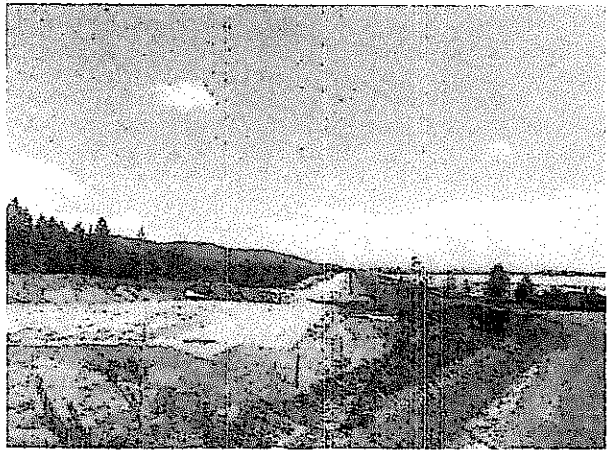


Photo 5: Drainage ditch excavated along the perimeter abutment.

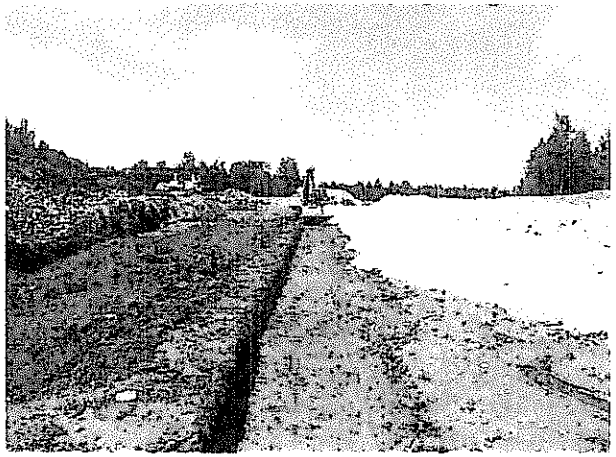
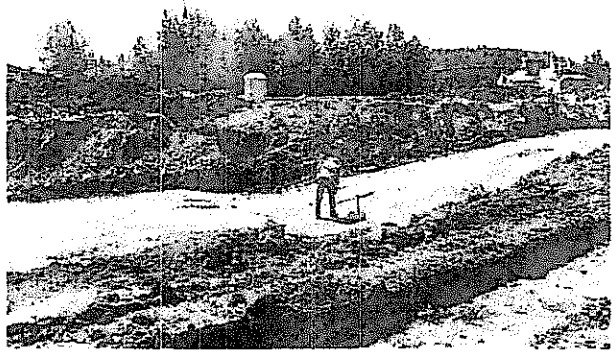


Photo 6: Native till density testing at Perimeter abutment.



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Mount Polley Mine

Tailings Storage Facility
2012 Construction Photos

DATE PREPARED: January 2013
SCALE: NTS
PREPARED BY: D. Ostritchenko
PROJECT No: VM00560A

Photos 1 to 6

Taken: July/ August 2012

Photo 7: Scarification of till core prior to placement of the successive lifts.

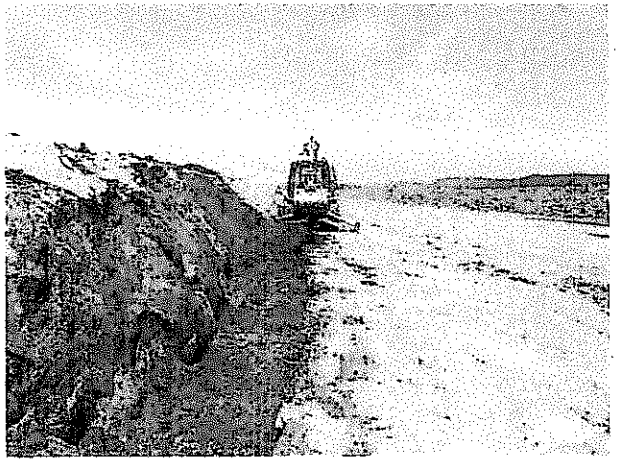

Photo 8: Trenching upstream of Zone S, to establish the required 5 m core till width and 5 m overlap with existing core.

Photo 9: Placement of till in the upstream excavated trench.

Photo 10: Compaction of the till core material focusing on the corrective trench core till material (Photos 8 and 9).

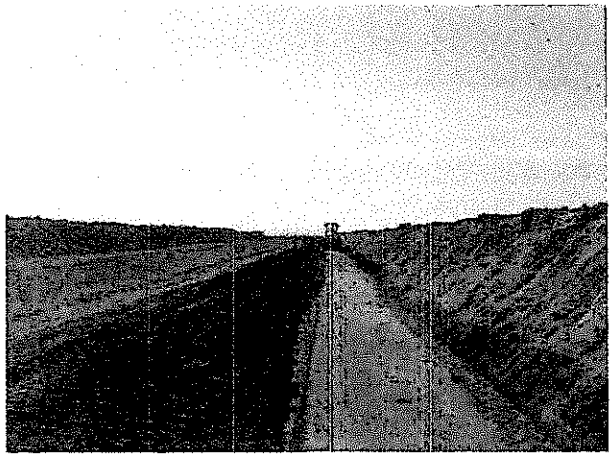

Photo 11: Moisture conditioning of the till core material prior to placement.

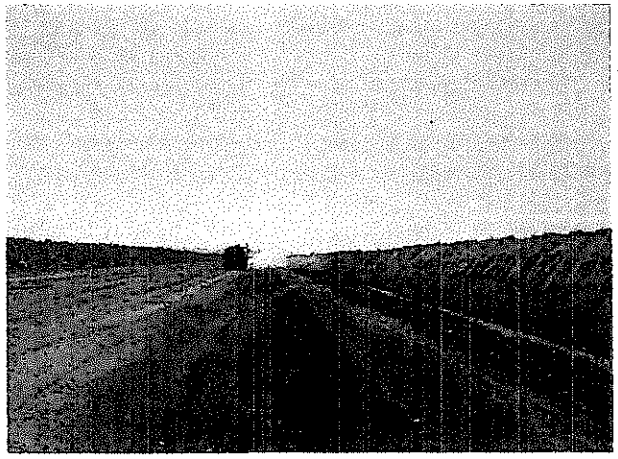

Photo 12: Placement and spreading of till core material.

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Mount Polley Mine

Tailings Storage Facility
2012 Construction Photos

DATE PREPARED: January 2013
SCALE: NTS
PREPARED BY: D. Ostritchenko
PROJECT No: VM00560A

Photos 7 to 12

Taken: June-August 2012

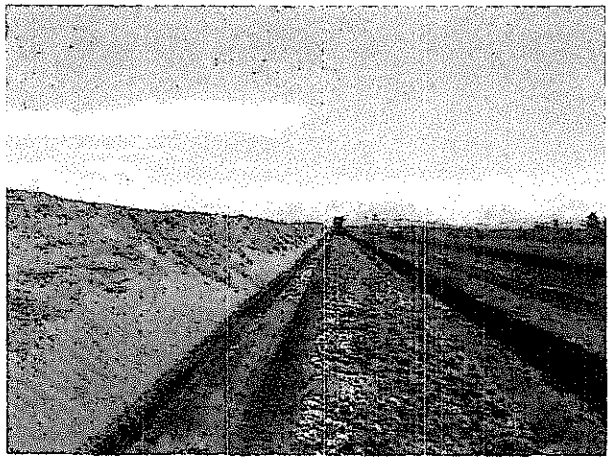


Photo 13: Looking southeast along South embankment, grading back Zone U material prior to placement of till core.

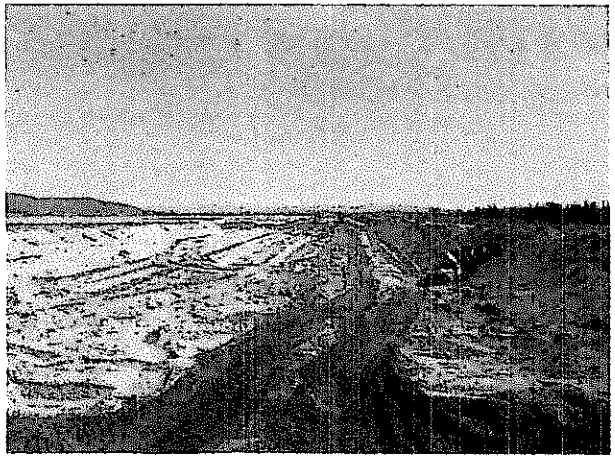


Photo 14: Looking southeast at the sand cell construction on the South embankment.

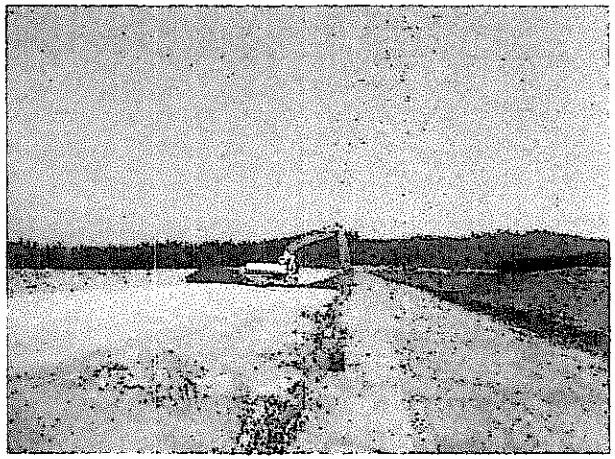


Photo 15: Looking northwest along South embankment, excavator trimming till core to design lines.

Photo 16: Looking along the South embankment at the prepared till/filter zone contact surface.

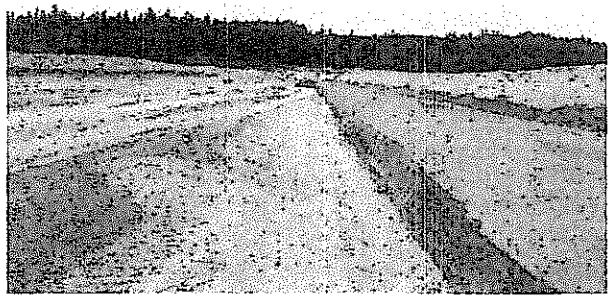


Photo 17: Placement of filter material along the south embankment.

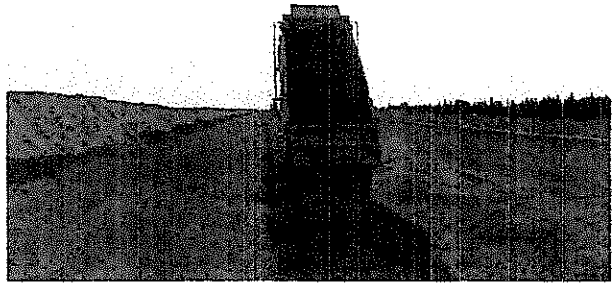
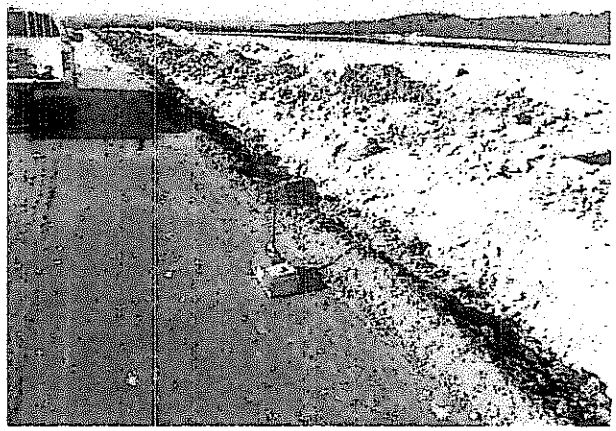


Photo 18: Quality control compaction testing along the Main embankment.



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Mount Polley Mine

Tailings Storage Facility
2012 Construction Photos

DATE PREPARED: January 2013

SCALE: NTS

PREPARED BY: D. Osiritchenko

PROJECT No: VM00560A

Photos 13 to 18

Taken: June to August 2012

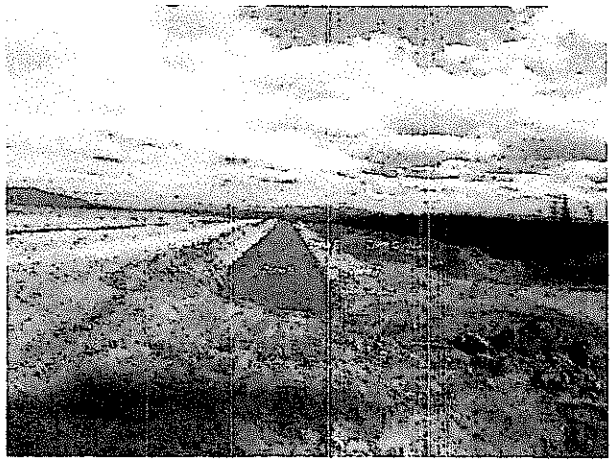


Photo 19: Looking east at the South embankment from South abutment.

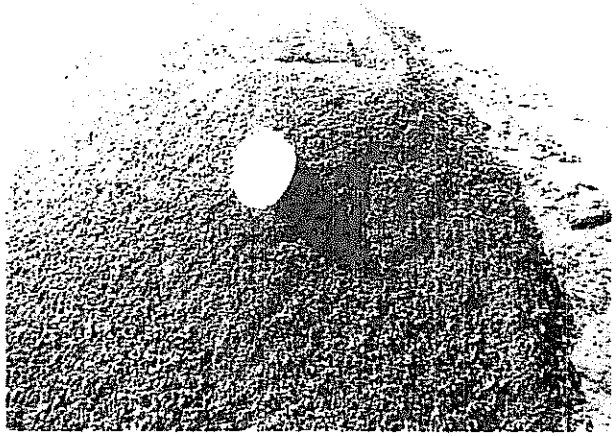


Photo 20: Visual confirmation of the placed Zone F material gradation.

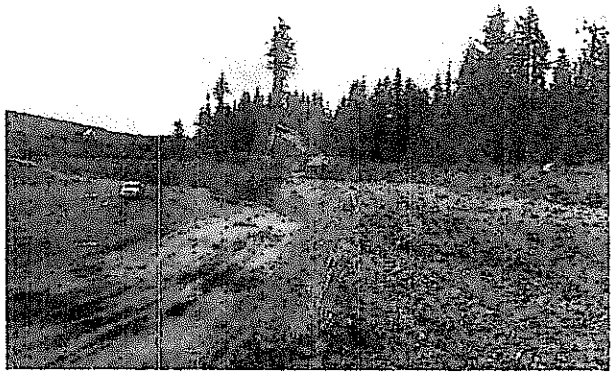


Photo 21: Borrow pit development along the north pit extents.

Photo 22: Ramping of transition material to allow for construction access.

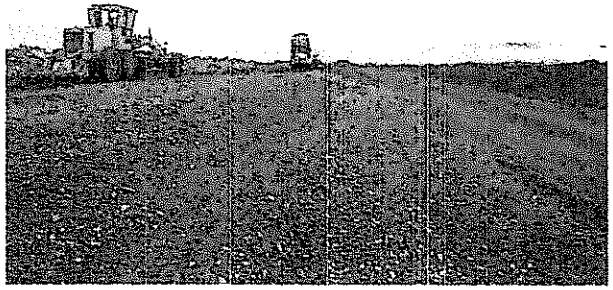
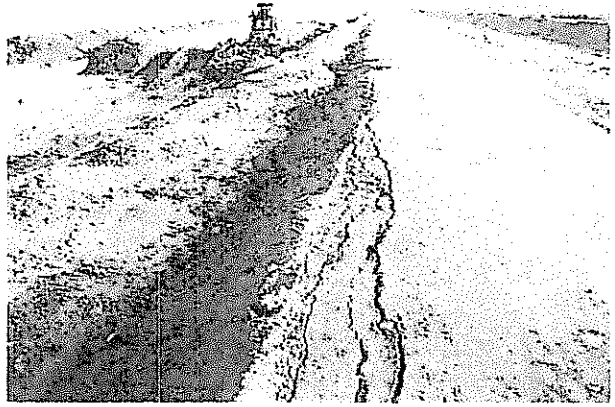


Photo 23: Overview of the borrow pit.

Photo 24: Tension cracks noted on the upstream side of the till core along the Perimeter embankment at the end of the 2012 construction.



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Mount Polley Mine

Tailings Storage Facility
2012 Construction Photos

DATE PREPARED: January 2013

SCALE: NTS

PREPARED BY: D. Ostritchenko

PROJECT No: VM00560A

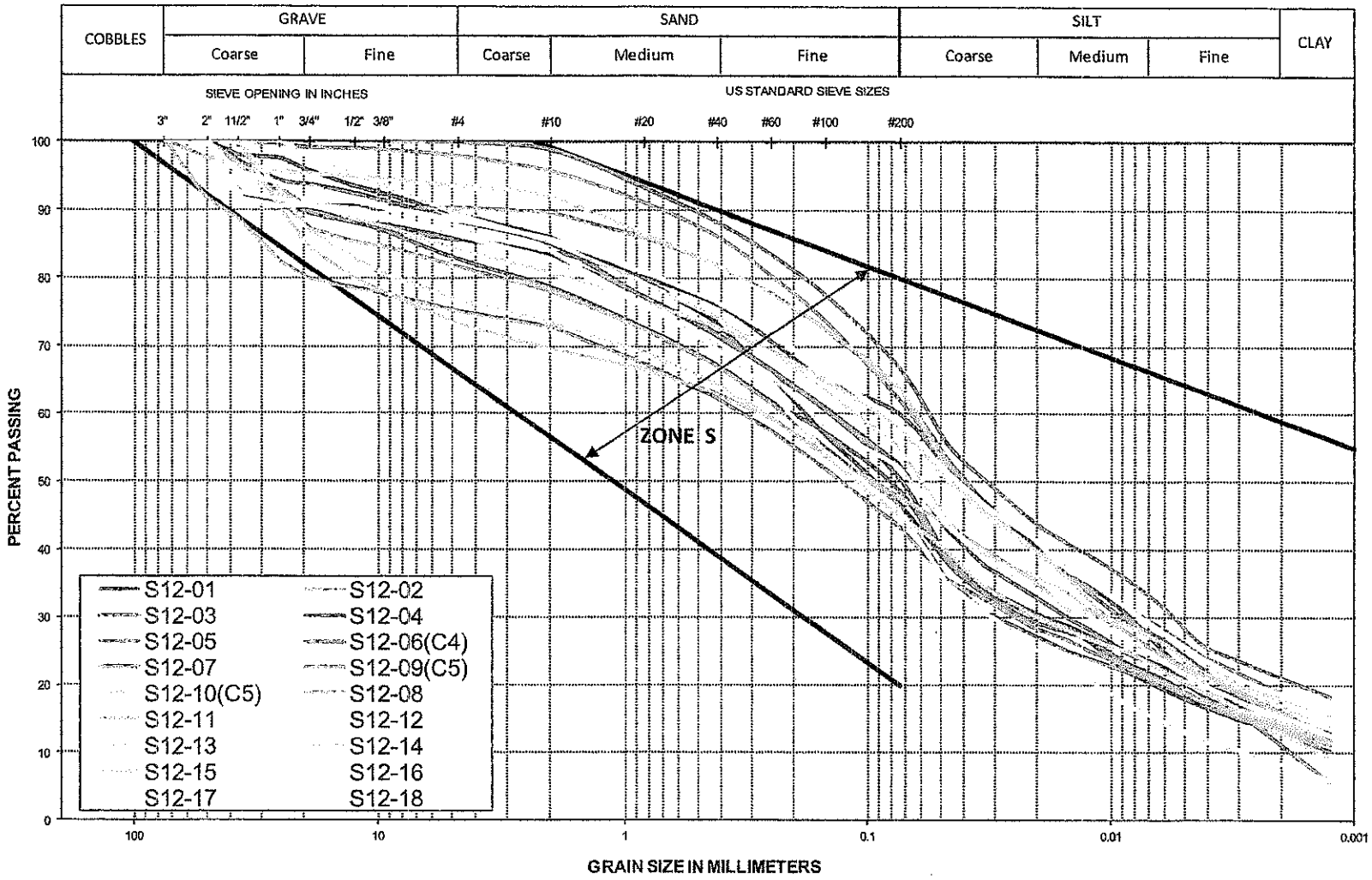
Photos 19 to 24

Taken: August to September 2012

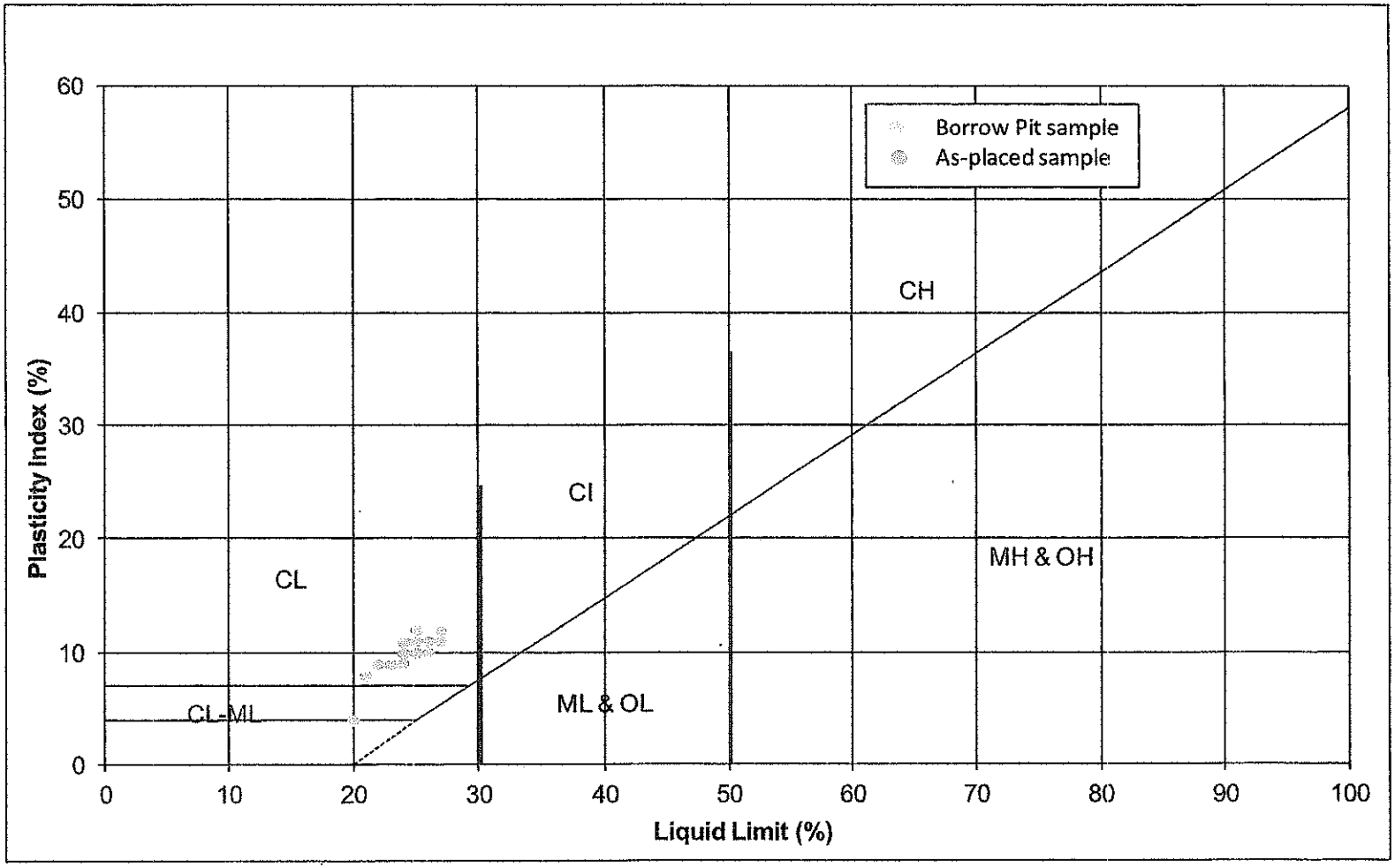
APPENDIX B

MATERIAL TESTING RESULTS

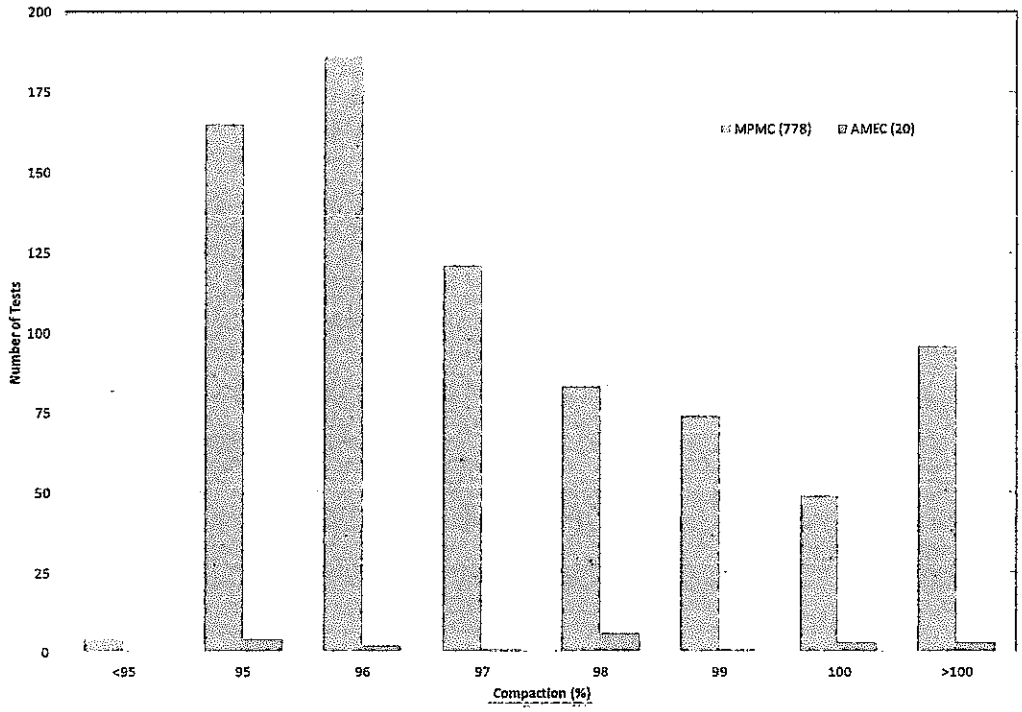
2012 ZONE S (TILL) GRADATIONS



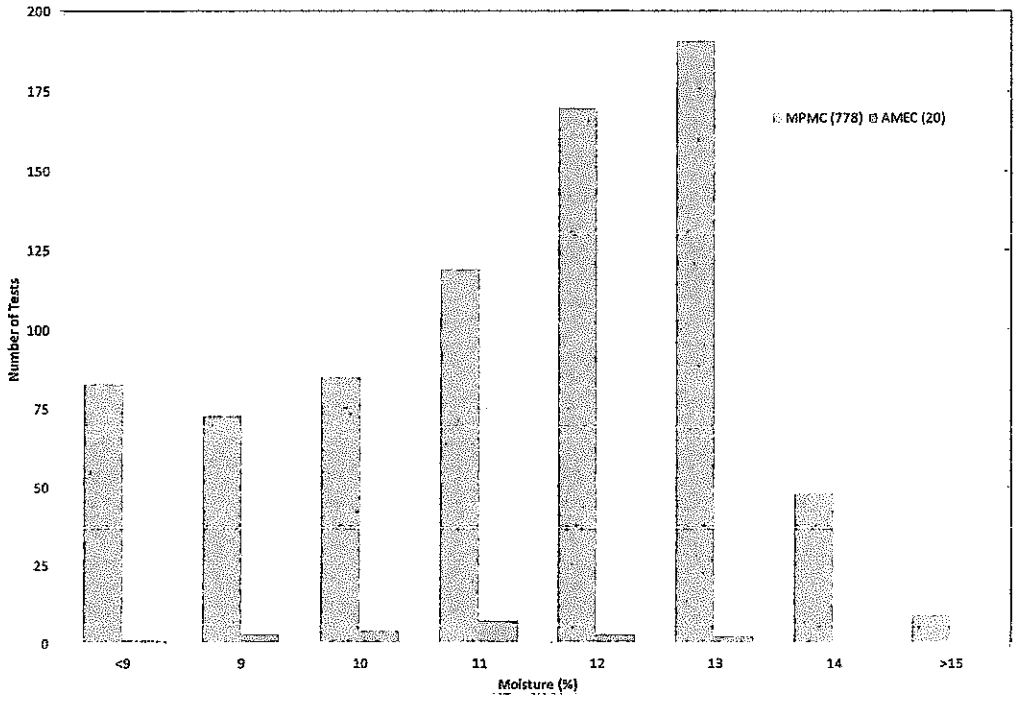
ZONE S (TILL) PLASTICITY CHART



Zone S % Compaction Distribution



Zone S Moisture Content Distribution



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Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
1	15-May-12	29.25			959.86	5819094	596114	2056		2300.0		2124.0	8.3	103%	YES		
2	15-May-12	28.25			959.83	5818984	596194	2056		2196.0		1981.0	10.8	96%	YES		
3	31-May-12	43.50	0.5		960.30			2094	145.4	2329.1	133.8	2143.3	8.6	102%	YES		
4	31-May-12	44.00	2.0		960.30			2094	146.2	2341.9	133.4	2136.9	9.6	102%	YES		
5	1-Jun-12	45.00	3.5		960.30			2094	137.9	2208.9	121.2	1941.4	13.8	93%	NO	#6, #49,#50	
6	1-Jun-12	46.00	3.5		960.30			2094	140.2	2245.8	125.3	2007.1	11.9	96%	YES		
7	1-Jun-12	46.00	0.5		960.30			2094	141.8	2271.4	126.1	2019.9	12.4	96%	YES		
8	1-Jun-12	47.00	2.0		960.30			2094	137.4	2200.9	120.4	1928.6	14.1	92%	NO	#20, #47	
9	2-Jun-12	47.50	2.0		960.30			2094	139.9	2241.0	125.1	2003.9	11.8	96%	YES		
10	2-Jun-12	47.00	1.0		960.30			2094	135.3	2167.3	120.8	1935.0	12.0	92%	NO	#20, #47	
11	2-Jun-12	46.25	4.0		960.30			2094	137.7	2205.7	124.8	1999.1	12.0	95%	YES		
12	2-Jun-12	45.25	2.0		960.30			2094	134.3	2151.3	120.8	1935.0	11.2	92%	NO	#16	
13	4-Jun-12	45.00	1.0		960.30			2094	135.1	2164.1	120.1	1923.8	12.5	92%	NO	#6, #49,#50	
14	4-Jun-12	46.00	2.0		960.30			2094	137.8	2207.3	123.8	1983.1	11.3	96%	YES		
15	4-Jun-12	46.00	3.5		960.30			2094	136.5	2186.5	121.0	1938.2	12.8	93%	NO	#6, #14, #49,#50	
16	4-Jun-12	45.25	2.0		960.30			2094	138.7	2221.8	124.5	1994.3		95%	YES		
17	4-Jun-12	45.25	0.5		960.30			2094	138.1	2212.1	123.3	1975.1	12.0	94%	NO	#16	
18	4-Jun-12	46.00	4.0		960.30			2094	140.4	2249.0	125.7	2013.5	11.7	96%	YES		
19	4-Jun-12	46.50	2.0		960.30			2094	138.2	2213.8	123.7	1981.5	11.7	96%	YES		
20	4-Jun-12	47.00	2.0		960.30			2094	140.2	2245.8	125.4	2008.7	11.8	96%	YES		
21	4-Jun-12	47.50	4.0		960.30			2094	137.6	2204.1	120.8	1935.0	13.9	92%	NO	#9, #46, #47	
22	11-Jun-12	32.25	2.7		960.23			2094	135.7	2173.7	118.3	1895.0	14.7	90%	NO	#60, #79	
23	11-Jun-12	33.00	4.2		960.31			2094	135.1	2164.1	117.0	1874.2	15.5	90%	NO	#78, #79	
24	11-Jun-12	33.00	0.6		960.24			2094	132.1	2116.0	113.3	1814.9	16.6	87%	NO	#78, #79	
25	11-Jun-12	33.75	4.4		960.15			2094	137.1	2196.1	120.3	1927.0	14.0	92%	NO	#77, #78	
26	11-Jun-12	33.75	2.6		960.19			2094	133.7	2141.7	116.3	1862.9	15.0	89%	NO	#77, #78	
27	11-Jun-12	34.75	0.8		960.35			2094	134.9	2160.9	118.5	1898.2	13.8	91%	NO	#76, #77	
28	11-Jun-12	34.75	3.8		960.31			2094	139.5	2234.6	122.2	1957.5	14.2	93%	NO	#76, #77	
29	11-Jun-12	35.75	3.5		960.25			2094	135.8	2175.3	116.5	1866.2	16.6	89%	NO	#30	
30	11-Jun-12	35.75	0.7		960.33			2094	139.8	2239.4	124.2	1989.5	12.6	95%	YES		
31	11-Jun-12	37.00	2.0		960.45			2094	141.0	2258.6	125.7	2013.5	12.2	96%	YES		
32	11-Jun-12	37.00	0.6		960.42			2094	137.7	2205.7	120.9	1936.6	13.9	92%	NO	#73	
33	11-Jun-12	38.00	3.7		960.33			2094	137.6	2204.1	122.5	1962.3	12.4	94%	NO	#34	
34	11-Jun-12	38.00	1.4		960.36			2094	141.1	2260.2	128.6	2060.0	9.7	98%	YES		
35	12-Jun-12	40.00	2.0					2094	139.9	2241.0	123.2	1973.5	13.6	94%	NO	#36	
36	12-Jun-12	40.00	3.7					2094	141.5	2266.6	124.5	1994.3	13.7	95%	YES		
37	12-Jun-12	39.50	2.4		960.43			2094	133.8	2143.3	113.3	1814.9	18.1	87%	NO	#65	
38	12-Jun-12	33.00	2.8		960.40			2094	137.5	2202.5	119.4	1912.6	15.1	91%	NO	#78, #79	
39	13-Jun-12	43.00	2.5		960.31			2094	138.0	2210.5	119.5	1914.2	15.5	91%	NO	#70	
40	13-Jun-12	43.00	4.0		960.32			2094	138.2	2213.8	121.1	1939.8	14.2	93%	NO	#70	
41	13-Jun-12	42.00	1.5		960.49			2094	137.6	2204.1	120.7	1933.4	14.0	92%	NO	#66, #69	
42	13-Jun-12	41.00	2.5		960.51			2094	141.1	2260.2	126.9	2032.7	11.1	97%	YES		
43	13-Jun-12	40.35	1.0		960.40			2094	142.8	2287.4	126.4	2024.7	13.0	97%	YES		
44	13-Jun-12	34.75	2.5		960.43			2094	137.8	2207.3	123.3	1975.1	11.8	94%	NO	#76, #77	
45	13-Jun-12	33.75	1.0		960.25			2094	136.9	2192.9	119.6	1915.8	14.4	91%	NO	#77, #78	
46	15-Jun-12	47.60	4.0		960.24			2094	138.3	2215.4	123.8	1983.1	11.4	95%	YES		
47	15-Jun-12	47.15	2.5		960.15			2094	138.1	2212.1	125.0	2002.3	10.5	96%	YES		
48	15-Jun-12	45.75	1.0		960.35			2094	145.7	2333.9	132.7	2125.7	9.8	102%	YES		
49	15-Jun-12	45.00	4.0		960.50			2094	149.1	2388.4	137.7	2205.7	8.3	105%	YES		
50	15-Jun-12	45.00	2.5		960.50			2094	135.2	2165.7	123.7	1981.5	10.0	95%	YES		
51	15-Jun-12	42.50	2.5		960.33			2094	135.0	2162.5	119.8	1919.0	12.7	92%	NO	#69, #70	
52	15-Jun-12	42.50	4.0		960.33			2094	132.1	2116.0	116.8	1871.0	13.1	89%	NO	#69, #70	
53	15-Jun-12	42.00	4.0		960.46			2094	132.4	2120.8	117.9	1888.6	12.3	90%	NO	#66, #69	
54	15-Jun-12	42.00	1.0		960.45			2094	132.1	2116.0	116.2	1861.3	13.6	89%	NO	#66, #69	
55	15-Jun-12	43.00	3.0		960.31			2094	137.9	2208.9	123.7	1981.5	11.6	95%	YES		
56	20-Jun-12	43.00	1.8					2094	134.5	2154.5	120.0	1922.2	12.1	92%	NO	#70	
57	20-Jun-12	42.25	0.3		960.45			2094	138.7	2221.8	123.7	1981.5	12.1	95%	YES	#66, #69	
58	20-Jun-12	41.75	3.2		960.68			2094	137.5	2202.5	122.4	1960.7	12.3	94%	NO	#66, #69	
59	20-Jun-12	35.75	1.8		960.36			2094	138.5	2218.6	123.3	1975.1	12.3	94%	NO	#30, #75	
60	21-Jun-12	32.14	3.4		960.30	5819311	595941	2094	140.9	2257.0	124.6	1995.9	13.0	95%	YES		
61	21-Jun-12	32.82	3.1		960.40	5819350	595884	2094	134.3	2151.3	118.1	1891.8	13.8	90%	NO	#78, #79	
62	21-Jun-12	33.58	3.7		960.47	5819392	595821	2094	130.5	2090.4	113.4	1816.5	15.0	87%	NO	#77, #78	
63	21-Jun-12	34.40	0.7		960.40	5819440	595754	2094	134.1	2148.1	117.4	1880.6	14.3	90%	NO	#76, #77	
64	21-Jun-12	34.99	1.9		960.44	5819472	595705	2094	134.5	2154.5	120.7	1933.4	11.4	92%	NO	#75, #76	
65	21-Jun-12	39.60	5.2		960.69	5819726	595320	2094	139.4	2233.0	126.1	2019.9	10.6	96%	YES		
66	21-Jun-12	41.60	0.6		960.47	5819842	595157	2094	141.7	2269.8	128.1	2052.0	10.6	98%	YES		
67	21-Jun-12	42.53	3.3		971.00	5819891	595078	2094	136.5	2186.5	122.3	1959.1	11.6	94%	NO	#69, #70	
68	22-Jun-12	41.50	2.4		960.60	5819834	595164	2094	136.7	2189.7	124.2	1989.5	10.1	95%	YES		
69	22-Jun-12	42.37	2.3		959.90	5819883	595092	2094	135.9	2176.9	123.1	1971.8	10.4	94%	NO		
70	22-Jun-12	43.03	3.8		960.40	5819919	595036	2094	129.6	2076.0	126.9	2032.7	10.0	97%	YES		
71	22-Jun-12	31.93	1.4		960.30	5819859	595129	2094	136.4	2184.9	124.2	1989.5	9.8	95%	YES		

27 March 2013

Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
72	22-Jun-12	38.49	4.0		960.40	5819665	595412	2094	138.1	2212.1	126.1	2019.9	9.5	96%	YES		
73	22-Jun-12	37.07	0.7		960.50	5819589	595533	2094	143.1	2292.2	131.8	2111.2	8.6	101%	YES		
74	22-Jun-12	36.22	2.9		960.30	5819540	595602	2094	142.6	2284.2	129.7	2077.6	9.9	99%	YES		
75	22-Jun-12	35.48	4.0		960.30	5819497	595662	2094	138.2	2213.8	126.1	2019.9	9.6	96%	YES		
76	22-Jun-12	34.80	0.9		960.30	5819462	595721	2094	139.4	2233.0	125.2	2005.5	11.4	96%	YES		
77	22-Jun-12	33.99	4.3		960.50	5819414	595787	2094	138.0	2210.5	125.2	2005.5	10.2	96%	YES		
78	22-Jun-12	33.13	2.1		960.40	5819368	595859	2094	137.8	2207.3	125.4	2008.7	9.9	96%	YES		
79	22-Jun-12	32.49	3.0		960.40	5819331	595912	2094	138.0	2210.5	124.6	1995.9	10.8	95%	YES		
80	26-Jun-12	14.98	2.5		960.25	5818267	595180	2094	135.5	2170.5	120.8	1935.0	12.2	92%	NO	#82	
81	26-Jun-12	12.98	1.0		960.63	5818338	594993	2094	141.7	2269.8	124.9	2000.7	13.4	96%	YES		
82	27-Jun-12	15.00	2.5		960.39			2094	138.2	2213.8	125.1	2003.9	10.5	96%	YES		
83	27-Jun-12	14.00	1.0		960.41			2094	141.1	2260.2	127.7	2045.6	10.5	98%	YES		
84	27-Jun-12	13.00	4.0		960.36			2094	134.5	2154.5	118.3	1895.0	14.0	90%	NO	#92	
85	27-Jun-12	13.00	4.0		960.36			2094	136.9	2192.9	119.9	1920.6	14.2	92%	NO	#92	
86	27-Jun-12	12.00	2.5		960.55	5818375	594902	2094	135.3	192.2	117.8	1887.0	14.8	90%	NO	#87	
87	27-Jun-12	12.00	3.0		960.56	5818376	594903	2094	140.1	192.2	123.7	1981.5	13.3	95%	YES		
88	27-Jun-12	11.00	1.0		960.52	5818411	594808	2094	131.1	2100.0	111.2	1781.3	18.0	85%	NO	#95	
89	27-Jun-12	11.05	4.0		960.50	5818414	594809	2094	133.2	2133.7	114.4	1832.5	16.5	88%	NO	#95	
90	27-Jun-12	10.02	2.5		960.48	5818448	594717	2094	131.1	2100.0	110.6	1771.6	18.6	85%	NO	#96	
92	27-Jun-12	12.95	1.5		960.47	581339	594992	2094	140.1	2244.2	123.7	1981.5	12.0	95%	YES		
93	27-Jun-12	11.95	2.5		960.56	5818378	594900	2094	137.4	2200.9	122.4	1960.7	10.9	94%	NO	#94	
94	27-Jun-12	11.95	2.5		960.56	5818378	594900	2094	140.3	2247.4	124.1	1987.9	13.0	95%	YES		
95	28-Jun-12	11.00	1.7		960.54	5818412	594806	2094	138.6	2220.2	124.0	1986.3	11.8	95%	YES		
96	28-Jun-12	10.03	2.5		960.59	5818477	594719	2094	139.9	2241.0	125.0	2002.3	11.9	96%	YES		
97	28-Jun-12	9.35	1.0		960.53	5818474	594655	2094	140.4	2249.0	124.8	1999.1	12.5	96%	YES		
98	28-Jun-12	8.95	4.0		960.60	5818487	594614	2094	140.9	2257.0	125.9	2016.7	11.9	96%	YES		
99	28-Jun-12	8.46	1.3		960.51	5818507	594569	2094	140.1	2244.2	124.8	2000.7	12.2	96%	YES		
100	28-Jun-12	7.67	3.0		960.57	5818533	594499	2094	139.2	2229.8	123.4	1976.7	12.8	94%	NO	#101	
101	28-Jun-12	7.67	3.0		960.57	5818533	594499	2094	140.4	2249.0	125.2	2005.5	12.1	96%	YES		
102	28-Jun-12	7.23	4.0		960.37	5818548	594458	2094	136.6	2188.1	122.6	1963.9	11.4	94%	NO	#128, #129	
103	28-Jun-12	17.50	4.0		959.92	5818348	595388	2094	138.9	2225.0	123.8	1983.1	15.1	95%	YES		
104	28-Jun-12	16.76	2.5		960.00	5818306	595331	2094	143.6	2300.3	129.3	2071.2	11.0	99%	YES		
105	28-Jun-12	16.03	1.2		959.90	5818262	595272	2094	141.1	2260.2	125.1	2003.9	11.5	96%	YES		
106	28-Jun-12	15.50	2.5		960.00	5818249	595230	2094	144.2	2309.9	129.6	2076.0	11.2	99%	YES		
107	28-Jun-12	7.40	2.5		960.23	5818544	594474	2094	138.7	2221.8	128.1	2052.0	8.3	98%	YES		
108	28-Jun-12	6.50	1.0		960.12	5818579	594387	2094	137.2	2197.7	123.8	1983.1	10.4	95%	YES		
109	28-Jun-12	5.47	3.7		960.36	5818613	594295	2094	138.2	2213.8	123.8	1983.1	10.4	95%	YES		
110	29-Jun-12	7.55	2.5		960.49	5818538	594487	2094	134.9	2160.9	117.2	1877.4	15.1	90%	NO	#112	
111	29-Jun-12	7.40	1.0		960.23	5818539	594480	2094	134.4	2152.9	117.4	1880.6	14.5	90%	NO	#107, #128, #129	
112	29-Jun-12	7.55	4.0		960.49	5818538	594487	2094	140.9	2257.0	124.3	1991.1	14.0	95%	YES		
113	29-Jun-12	19.23	2.5		959.91	5818451	595523	2094	139.1	2228.2	122.0	1954.3	14.4	93%	NO	#118,#117	
114	29-Jun-12	19.20	2.5		959.94	5818449	595523	2094	138.1	2212.1	120.7	1933.4	13.3	92%	NO	#118,#117	
115	29-Jun-12	18.50	4.0		959.69	5818408	595469	2094	144.3	2311.5	127.4	2040.8	13.3	97%	YES		
116	29-Jun-12	18.00	1.0		959.91			2094	141.4	2265.0	124.7	1997.5	13.4	95%	YES		
117	29-Jun-12	19.00	2.0		959.90			2094	143.5	2298.6	126.0	2018.3	13.8	96%	YES		
118	29-Jun-12	19.35	3.0		959.30			2094	143.9	2305.1	127.6	2044.0	12.7	98%	YES		
119	30-Jun-12	20.26	2.5		960.06	5818516	595611	2094	141.4	2265.0	129.9	2080.8	8.9	99%	YES		
120	30-Jun-12	21.11	1.5		959.84	5818585	595679	2094	137.7	2205.7	117.8	1887.0	16.9	90%	NO	#121	
121	30-Jun-12	21.10	2.0		959.99	5818564	595677	2094	140.9	2257.0	129.3	2071.2	9.0	99%	YES		
122	30-Jun-12	22.15	1.0		959.97	5818627	595760	2094	135.5	2170.5	124.7	1997.5	8.7	95%	YES		
123	1-Jul-12	27.29	2.5		960.01	5818939	596173	2094	131.1	2100.0	118.1	1891.8	9.9	90%	NO	#144, #145	
124	1-Jul-12	26.35	1.0		960.11	5818819	596019	2094	135.4	2168.9	121.1	1939.8	10.3	93%	NO	#156, #157	
125	1-Jul-12	24.25	4.2					2094	135.1	2180.1	121.8	1951.7	10.5	93%	NO	#158, #159	
126	1-Jul-12	23.42	1.7					2094	134.2	2149.7	118.9	1904.6	11.4	91%	NO	#158, #159	
127	30-Jun-12	5.45	3.0		960.73	5818617	594290	2094	140.3	2247.4	125.6	2011.9	11.7	96%	YES		
128	30-Jun-12	6.55	2.0		960.56	5818573	594395	2094	139.6	2236.2	126.5	2026.3	10.4	97%	YES		
129	30-Jun-12	7.53	3.7		960.65	5818535	594497	2094	139.8	2239.4	126.3	2023.1	10.6	97%	YES		
130	30-Jun-12	8.28	4.2		960.78	5818510	594558	2094	141.6	2268.2	129.1	2068.0	9.7	99%	YES		
131	30-Jun-12	9.26	1.0		960.70	5818474	594647	2094	140.1	2244.2	126.5	2026.3	10.7	97%	YES		
132	30-Jun-12	10.25	2.5		960.69	5818439	594741	2094	140.1	2244.2	128.2	2053.6	9.3	98%	YES		
133	30-Jun-12	11.25	3.7		960.73	5818402	594837	2094	141.2	2261.8	127.3	2039.2	10.9	97%	YES		
134	30-Jun-12	12.25	1.5		960.63	5818365	594928	2094	140.0	2242.6	127.3	2039.2	9.9	97%	YES		
135	30-Jun-12	13.28	3.8		960.67	5818330	595022	2094	141.3	2263.4	128.7	2061.6	9.8	98%	YES		
136	30-Jun-12	14.26	2.7		960.60	5818294	595113	2094	145.9	2337.1	134.8	2159.3	8.3	103%	YES		
137	30-Jun-12	15.12	1.4		959.97	5818261	595191	2094	141.1	2260.2	127.0	2034.3	11.1	97%	YES		
138	30-Jun-12	16.10	0.7		960.10	5818262	595277	2094	139.8	2239.4	125.9	2016.7	11.1	96%	YES		
139	30-Jun-12	17.05	2.5		960.23	5818324	595355	2094	138.3	2216.4	125.1	2003.9	10.5	96%	YES		
140	30-Jun-12	18.10	1.2		960.33	58183851	595439	2094	137.4	2200.9	124.1	1987.9	10.9	95%	YES		
141	30-Jun-12	19.05	4.1		960.21	5818444	595512	2094	141.4	2265.0	127.8	2047.2	10.6	98%	YES		
142	6-Jul-12	23.05	3.7		960.20	5818684	595833	2094	137.8	2207.3	126.2	2021.5	9.2	97%	YES	#142, #159	

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Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
143	6-Jul-12	23.77	0.7		960.30	5818725	595892	2094	130.0	2082.4	116.2	1861.3	11.8	89%	NO	#158, #159	
144	6-Jul-12	26.48	2.3		960.20	5818889	596108	2094	142.1	2276.2	129.8	2079.2	9.5	99%	YES		
145	6-Jul-12	27.44	0.7		960.30	5818945	596186	2094	135.9	2176.9	124.5	1994.3	9.1	95%	YES		
146	6-Jul-12	28.43	4.1		960.30	5819019	596166	2094	136.5	2186.5	122.0	1954.3	11.9	93%	NO	#185	
147	6-Jul-12	29.50	1.0		960.30	5819106	596104	2094	139.7	2237.8	126.8	2031.1	10.2	97%	YES		
148	6-Jul-12	30.55	3.6		960.30	5819188	596039	2094	135.2	2165.7	124.2	1989.5	10.3	95%	YES		
149	6-Jul-12	30.96	2.3		960.30	5819224	596014	2094	137.4	2200.9	124.8	1999.1	10.1	95%	YES		
150	6-Jul-12	25.58	1.1		960.30	5818834	596037	2094	135.6	2172.1	122.7	1965.5	10.5	94%	NO	#156, #157	
151	6-Jul-12	27.42	5.10		960.30	5818948	596182	2094	133.3	2135.3	119.2	1909.4	12.0	91%	NO	#151	
152	8-Jul-12	27.41	5.10		960.30	5818947	596181	2094	144.5	2314.7	129.8	2079.2	11.3	99%	YES		
153	8-Jul-12	26.99	5.00		960.10	5818922	596147	2094	137.4	2200.9	121.4	1944.6	13.1	93%	NO	#154	
154	8-Jul-12	28.97	4.90		960.10	5818920	596145	2094	137.3	2199.3	124.4	1992.7	11.2	95%	YES		
155	8-Jul-12	26.64	4.90		960.20	5818901	596119	2094	140.2	2245.8	127.2	2037.5	10.2	97%	YES		
156	8-Jul-12	26.01	5.10		960.40	5818863	596069	2094	137.7	2205.7	124.2	1989.5	10.9	95%	YES		
157	8-Jul-12	25.32	5.30		960.20	5818822	596014	2094	138.8	2223.4	124.2	1989.5	11.7	95%	YES		
158	8-Jul-12	24.50	5.10		960.20	5818772	595948	2094	139.9	2225.0	124.8	1999.1	11.3	95%	YES		
159	8-Jul-12	23.52	5.10		960.20	5818713	595870	2094	137.1	2196.1	121.9	1952.7	12.5	93%	NO	#168	No change with added compaction
160	8-Jul-12	22.65	5.10		960.20	5818660	595800	2094	137.2	2197.7	123.9	1984.7	10.7	95%	YES		
161	8-Jul-12	21.35	5.00		960.10	5818583	595697	2094	139.5	2234.6	125.3	2007.1	11.3	96%	YES		
162	9-Jul-12	19.69	5.00		960.20	5818484	595563	2094	141.1	2260.2	128.2	2053.6	10.1	98%	YES		
163	9-Jul-12	20.05	3.00		960.20	5818504	595594	2094	141.1	2260.2	124.5	1994.3	13.4	95%	YES		
164	9-Jul-12	19.61	2.90		960.40	5818477	595559	2094	138.4	2217.0	124.6	1995.9	11.2	95%	YES		
165	9-Jul-12	20.59	5.10		960.40	5818537	595635	2094	144.7	2317.9	131.3	2103.2	10.2	100%	YES		
166	9-Jul-12	21.68	1.20		960.30	5818599	595725	2094	139.9	2225.0	125.2	2005.5	10.9	96%	YES		
167	9-Jul-12	22.54	5.20		960.30	5818655	595792	2094	141.3	2263.4	127.6	2044.0	10.8	98%	YES		
168	9-Jul-12	23.61	3.90		960.40	5818718	595878	2094	142.3	2279.4	128.2	2053.6	11.1	98%	YES		
169	9-Jul-12	24.42	1.30		960.40	5818765	595943	2094	137.9	2208.9	125.1	2003.9	10.2	96%	YES	moisture test	
170	10-Jul-12	25.33	4.0		960.40	5818822	596015	2094	141.0	2256.6	128.2	2053.6	10.0	98%	YES		
171	10-Jul-12	26.33	4.8		960.30	5818882	596094	2094	138.4	2217.0	125.0	2002.3	10.7	96%	YES		
172	10-Jul-12	27.20	1.8		960.40	5818932	596166	2094	141.3	2263.4	126.0	2050.4	10.4	98%	YES		
173	12-Jul-12	31.25	4.2		960.27	5819245	595995	2094	141.8	2271.4	125.6	2011.9	12.1	96%	YES		
174	12-Jul-12	30.85	4.5		960.21	5819212	596020	2094	141.1	2260.2	124.0	1986.3	13.6	95%	YES		
175	12-Jul-12	30.35	4.7		960.23	5819176	596047	2094		2163.8		1926.0	12.3	92%	NO	#179	Test #175, to #224, performed with AMEC's Nuclear Densometer, to a depth of 300mm
176	12-Jul-12	30.35	4.8		960.22	5819176	596047	2094		2137.2		1910.7	11.8	91%	NO	#178	
177	12-Jul-12	30.35	4.7		960.22	5819176	596047	2094		2141.2		1918.8	11.6	92%	NO	#179	
178	12-Jul-12	30.35	4.8		960.22	5819176	596047	2094		2169.3		1957.9	11.8	94%	NO	#179	
179	12-Jul-12	30.05	4.8		960.26	5819151	596066	2094		2204.2		1979.0	11.4	95%	YES		
180	12-Jul-12	29.68	5.0		960.23	5819119	596090	2094		2308.4		2098.2	10.0	100%	YES		
181	12-Jul-12	29.25	4.3		960.22	5819087	596114	2094		2232.6		2012.4	10.9	96%	YES		
182	12-Jul-12	28.75	4.9		960.30	5819047	596144	2094		2232.1		2000.6	11.5	96%	YES		
183	12-Jul-12	28.37	5.0		960.20	5819020	596164	2094		2173.0		1948.0	11.5	93%	NO	#185	
184	12-Jul-12	28.37	4.7		960.20	5819020	596164	2094		2180.8		1961.8	11.1	94%	NO	#185	
185	12-Jul-12	28.37	4.7		960.20	5819020	596164	2094		2207.0		2004.0	10.1	96%	YES		
186	12-Jul-12	27.76	4.8		960.27	5818970	596199	2094		2203.7		1988.5	10.8	95%	YES		
187	12-Jul-12	33.85	5.1		960.22	5819407	595796	2094		2207.1		1995.6	10.5	95%	YES		
188	12-Jul-12	33.20	4.7		960.37	5819370	595850	2094		2157.5		1951.0	10.5	93%	NO	#190	
189	12-Jul-12	33.20	4.6		960.37	5819370	595850	2094		2289.6		2048.1	11.7	98%	YES		
190	12-Jul-12	32.60	4.6		960.31	5819336	595901	2094		2185.2		1979.5	10.7	95%	YES		
191	12-Jul-12	32.03	4.5		960.21	5819305	595947	2094		2257.5		2038.6	10.7	97%	YES		
192	12-Jul-12	31.70	5.0		960.31	5819278	595971	2094		2238.6		2048.4	9.2	98%	YES		
193	12-Jul-12	31.03	3.1		960.41	5819229	596009	2094		2285.8		2066.9	10.6	99%	YES		
194	12-Jul-12	30.30	4.3		960.44	5819173	596049	2094		2253.1		2037.9	10.5	97%	YES		
195	12-Jul-12	29.71	0.9		960.44	5819124	596090	2094		2246.8		2019.1	11.2	96%	YES		
196	12-Jul-12	28.90	4.5		960.38	5819061	596135	2094		2227.9		2000.1	11.3	96%	YES		
197	12-Jul-12	26.25	4.1		960.42	5819006	596175	2094		2240.6		2001.6	11.9	96%	YES		
198	12-Jul-12	27.40	1.1		960.46	5818947	59619	2094		2226.0		2002.0	10.9	96%	YES		
199	13-Jul-12	34.05	2.5		959.56	5819421	595778	2094		2294.0		2068.8	10.8	99%	YES		
200	13-Jul-12	34.05	2.0		959.70	5819423	595777	2094		2241.9		2006.7	11.7	96%	YES		
201	13-Jul-12	34.05	3.7		960.01	5819423	595775	2094		2242.8		1993.8	12.7	95%	YES		
202	13-Jul-12	35.60	2.9		959.96	5819507	581960	2094		2300.0		2052.5	12.0	98%	YES		
203	13-Jul-12	35.60	2.1		960.00	5819510	595650	2094		2310.9		2075.6	11.3	99%	YES		
204	13-Jul-12	36.45	3.2		960.09	5819562	595569	2094		2327.5		2118.5	9.8	101%	YES		
205	13-Jul-12	36.45	2.5		960.12	5819562	595569	2094		2210.7		1965.5	12.4	94%	NO	#217	
206	13-Jul-12	34.10	1.4		960.34	5819423	595778	2094		2293.2		2075.6	10.4	99%	YES		
207	13-Jul-12	34.03	4.0		960.23	5819415	595784	2094		2130.4		1900.2	12.2	91%	NO	#211, #212	
208	13-Jul-12	37.03	3.7		960.42	5819455	595926	2094		2151.3		1918.5	12.1	92%	NO	#211, #212	
209	13-Jul-12	34.06	2.4		960.20	5819414	595492	2094		2320.1		2091.1	10.9	100%	YES		
210	13-Jul-12	33.95	2.5		960.26	5819413	595393	2094		2252.3		2097.0	12.7	143%	YES		
211	13-Jul-12	33.95	4.6		960.20	5819413	595787	2094		2162.9		1996.5	11.0	95%	YES		
212	13-Jul-12	33.95	4.6		960.20	5819413	595787	2094		2236.2		2019.7	10.9	98%	YES		

27 March 2013

Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
213	13-Jul-12	34.50	5.0		960.40	5819442	595743	2094		2280.6		2052.9	11.0	98%	YES		
214	13-Jul-12	35.27	4.7		960.40	5819489	595676	2094		2289.1		2062.6	10.9	99%	YES		
215	13-Jul-12	35.65	2.9		960.35	5819508	595649	2094		2223.3		1991.8	11.6	95%	YES		
216	13-Jul-12	36.00	4.1		960.30	5819527	595615	2094		2305.1		2079.9	10.8	99%	YES		
217	13-Jul-12	36.60	2.8		960.32	5819562	595569	2094		2239.2		2010.2	11.6	96%	YES		
218	13-Jul-12	37.00	4.7		960.34	5819583	595535	2094		2242.6		2019.8	11.0	96%	YES		
219	13-Jul-12	37.53	3.2		960.42	5819613	595494	2094		2251.5		2003.8	12.3	96%	YES		
220	13-Jul-12	37.90	4.0		960.33	5819635	595458	2094		2134.6		1920.2	12.1	92%	NO	#222	
221	13-Jul-12	37.90	4.0		960.33	5819635	595458	2094		2052.9		1820.2	12.7	87%	NO	#222	
222	13-Jul-12	37.90	4.0		960.34	5819634	595457	2094		2230.7		1992.9	11.9	95%	YES		
223	13-Jul-12	38.75	2.0		960.50	5819680	595394	2094		2219.3		1995.3	11.2	95%	YES		
224	13-Jul-12	39.90	5.0		960.50	5819808	595377	2094		2222.5		2018.5	10.1	96%	YES		
225	16-Jul-12	40.25	3.7		960.07	5819765	595264	2094		2282.7		2109.9	8.1	101%	YES		
226	16-Jul-12	40.57	4.1		960.47	5819781	595239	2094		2215.8		1985.3	11.6	95%	YES		
227	16-Jul-12	41.27	5.0		960.51	5819821	595180	2094		2278.5		2020.4	12.9	96%	YES		
228	16-Jul-12	41.97	4.7		960.48	5819859	595123	2094		2230.5		1980.9	12.5	95%	YES		
229	16-Jul-12	42.60	4.5		960.38	5819895	595071	2094		2208.8		1945.6	13.5	93%	NO	#230	
230	16-Jul-12	42.60	4.5		960.38	5819895	595071	2094		22.12.3		1979.9	11.9	95%	YES		
231	16-Jul-12	47.90	4.9		960.39	5819915	595040	2094		2182.6		1943.3	9.2	93%	NO	#261	
232	16-Jul-12	40.25	1.2		960.21	5819767	595266	2094		2302.5		2056.9	11.9	98%	YES		
233	16-Jul-12	39.60	4.7		959.97	5819728	595317	2094		2317.5		2093.2	10.7	100%	YES		
234	16-Jul-12	39.57	5.2		960.26	5819727	595320	2094		2271.2		2034.4	11.6	97%	YES		
235	16-Jul-12	39.48	5.4		960.08	5819720	595329	2094		2239.4		2015.1	11.1	96%	YES		
236	16-Jul-12	40.11	4.9		960.21	5819752	595283	2094		2267.4		2026.8	11.8	97%	YES		
237	16-Jul-12	39.65	5.0		960.34	5819731	595314	2094		2163.3		1924.0	12.4	92%	NO	#266, #267	
238	16-Jul-12	39.48	5.1		960.28	5819721	595329	2094		2250.2		2036.5	10.3	97%	YES		
239	16-Jul-12	39.45	5.2		960.36	5819716	595333	2094		2250.1		2012.0	11.8	96%	YES		
240	16-Jul-12	39.13	4.7		960.39	5819700	595360	2094		2231.1		1999.3	11.5	95%	YES		
241	16-Jul-12	39.72	5.1		960.26	5819733	595310	2094		2294.0		2053.4	11.7	98%	YES		
242	16-Jul-12	42.97	4.7		960.37	5819916	595039	2094		2308.0		2122.5	8.7	101%	YES		
243	16-Jul-12	38.34	3.1		960.77	5819677	595397	2094		2269.9		2079.5	9.1	99%	YES		
244	16-Jul-12	37.66	4.9		960.53	5819636	595455	2094		2319.0		2124.6	9.1	101%	YES		
245	16-Jul-12	37.00	1.2		960.58	5819600	595516	2094		2313.4		2135.5	8.3	102%	YES		
246	16-Jul-12	36.31	3.2		960.65	5819559	595573	2094		2201.4		2024.7	8.7	97%	YES		
247	16-Jul-12	35.63	5.0		960.46	5819513	595637	2094		2247.0		2061.6	8.9	98%	YES		
248	16-Jul-12	38.50	1.1		960.62	5819475	595700	2094		2193.5		2006.8	9.3	96%	YES		
249	16-Jul-12	34.17	3.2		960.48	5819433	595759	2094		2288.0		2078.8	9.0	99%	YES		
250	16-Jul-12	33.46	4.5		960.44	5819389	595822	2094		2295.4		2135.2	9.4	102%	YES		
251	16-Jul-12	32.20	1.4		960.48	5819316	595938	2094		2000.1		2000.1	8.5	96%	YES		
252	16-Jul-12	32.08	3.1		960.48	5819311	595942	2094		2103.5		2103.5	8.3	100%	YES		
253	17-Jul-12	43.36	4.9		960.47	5819949	594942	2094		1985.0		1985.0	11.9	95%	YES		
254	17-Jul-12	44.03	4.7		960.28	5819936	595009	2094		1987.9		1987.9	11.8	95%	YES		
255	17-Jul-12	44.70	4.8		960.53	5819960	594878	2094		2305.3		2066.0	11.5	99%	YES		
256	17-Jul-12	45.47	4.5		960.42	5819974	594803	2094		2300.8		2071.5	11.0	99%	YES		
257	17-Jul-12	46.21	5.1		960.39	5819987	594730	2094		2254.3		2008.7	12.2	96%	YES		
258	17-Jul-12	46.80	4.5		960.46	5819999	594668	2094		2264.6		2019.2	12.1	96%	YES		
259	17-Jul-12	48.86	N/A		963.82	5820062	594476	2094		2206.6		1922.2	14.7	92%	NO		tie-in
260	17-Jul-12	48.82	N/A		964.89	5820048	594452	2094		2217.2		1927.8	15.0	92%	NO		tie-in
261	17-Jul-12	48.20	N/A		960.05	5820036	594531	2094		2300.5		2091.3	10.0	100%	YES		tie-in
262	18-Jul-12	27.90	4.6		960.40	5818972	596196	2094	136.4	2184.9	124.2	1989.5	9.9	95%	YES		
263	18-Jul-12	29.09	1.4		960.40	5819073	596129	2094	138.9	2225.0	128.1	2052.0	8.4	98%	YES		
264	18-Jul-12	30.02	3.2		960.50	5819147	596071	2094	140.8	2255.4	129.2	2069.6	9.0	99%	YES		
265	18-Jul-12	31.09	4.5		960.40	5819232	596005	2094	140.2	2245.8	129.8	2063.2	8.9	99%	YES		
266	18-Jul-12	39.18	4.0		960.50	5819728	595316	2094	138.0	2210.5	125.4	2008.7	10.0	96%	YES		
267	18-Jul-12	40.17	4.6		960.50	5819759	595272	2094	137.2	2197.7	125.4	2008.7	9.4	96%	YES		
268	18-Jul-12	41.04	1.3		960.70	5819810	595203	2094	139.7	2237.8	127.3	2039.2	9.8	97%	YES		
269	18-Jul-12	42.06	2.4		960.70	5819866	595117	2094	136.6	2188.1	125.2	2005.6	9.2	96%	YES		
270	20-Jul-12	42.95	3.3		960.48	5819915	595043	2094	124.5	1994.3	130.8	2095.2	9.0	100%	YES		
271	20-Jul-12	44.05	0.8		960.60	5819952	594943	2094	138.8	2223.4	126.6	2027.9	9.7	97%	YES		
272	20-Jul-12	45.00	5.1		960.78	5819965	594849	2094	139.6	2236.2	127.8	2047.2	9.2	98%	YES		
273	20-Jul-12	46.07	2.9		960.95	5819987	594745	2094	141.5	2266.6	129.8	2079.2	9.0	99%	YES		
274	20-Jul-12	47.03	4.7		960.70	5920002	594649	2094	136.3	2183.3	121.5	1946.2	12.2	93%	NO		
275	26-Jul-12	14.27	2.7		960.96	5818292	595115	2094	143.3	2295.4	126.9	2032.7	12.9	97%	YES		
276	26-Jul-12	14.96	4.0		960.67	5818259	595177	2094	141.1	2260.2	124.9	2000.7	13.0	96%	YES		
277	26-Jul-12	13.63	1.1		961.02	5818315	595053	2094	140.8	2255.4	124.9	2000.7	12.7	96%	YES		
278	26-Jul-12	12.75	2.8		961.00	5818349	594970	2094	142.1	2276.2	125.5	2010.3	13.3	96%	YES		
279	26-Jul-12	11.95	5.0		960.99	5818380	594897	2094	143.0	2290.6	126.4	2024.7	13.2	97%	YES		
280	26-Jul-12	11.36	0.7		960.96	5818397	594843	2094	144.8	2319.5	129.1	2068.0	12.1	99%	YES		
281	26-Jul-12	11.07	1.5		961.02	5818480	594634	2094	141.8	2271.4	126.7	2029.5	12.0	97%	YES		
282	26-Jul-12	10.15	4.7		960.99	5818447	594726	2094	142.4	2281.0	126.4	2008.7	13.5	96%	YES		

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Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
283	26-Jul-12	9.17	2.6		961.07	5818407	594819	2094	140.9	2257.0	124.9	2000.7	12.8	96%	YES		
284	26-Jul-12	8.22	0.9		961.02	5818513	594547	2094	143.6	2300.3	126.5	2058.4	11.8	98%	YES		
285	26-Jul-12	7.28	4.9		960.84	5818549	594464	2094	142.1	2276.2	125.4	2008.7	13.3	96%	YES		
286	27-Jul-12	6.59	3.0		960.91	588564	59420	2094	145.5	2330.7	130.1	2084.0	11.8	100%	YES		
287	27-Jul-12	14.50	4.6		961.11	5818290	595127	2094	143.3	2295.4	126.0	2018.3	13.7	96%	YES		
288	27-Jul-12	13.55	1.0		961.33	5818317	595049	2094	142.1	2276.2	125.7	2013.5	13.1	96%	YES		
289	27-Jul-12	12.73	3.4		961.28	5818349	594970	2094	141.8	2271.4	125.8	2015.1	12.7	96%	YES		
290	27-Jul-12	11.75	4.3		961.17	5818387	594878	2094	141.9	2273.0	125.6	2011.9	12.9	96%	YES		
291	27-Jul-12	10.86	0.4		961.22	5818415	594798	2094	143.2	2293.8	125.6	2011.9	14.1	96%	YES		
292	27-Jul-12	10.35	2.6		961.22	5818435	594750	2094	124.1	1987.9	124.1	1987.9	11.0	95%	YES		
293	28-Jul-12	9.38	4.9		961.20	5818472	594661	1963	143.0	2290.6	126.8	2031.1	12.7	103%	YES		SE Tie-in
294	28-Jul-12	4.58			962.77	5818545	594220	1963	136.0	2178.5	117.8	1887.0	15.4	96%	YES		PE Tie-in
295	29-Jul-12	48.45			961.36	5820029	594512	1963	138.4	2217.0	118.4	1896.6	16.9	97%	YES		PE Tie-in
296	29-Jul-12	48.39			961.97	5820030	594494	1963	136.9	2192.9	119.9	1920.6	14.2	98%	YES		PE Tie-in
297	29-Jul-12	48.58			962.34	5820030	594494	1963	134.1	2148.1	114.1	1827.7	17.5	93%	NO		PE Tie-in
298	29-Jul-12	48.20			962.29	5820030	594495	1963	134.5	2154.5	114.6	1835.7	17.4	94%	NO		PE Tie-in
299	29-Jul-12	48.40			964.80	5820040	594451	1963	137.0	2194.5	116.1	1891.8	16.0	96%	YES		PE Tie-in
300	31-Jul-12	8.63	3.0		961.32	5818498	594589	2094	141.1	2260.2	126.7	2029.5	11.4	97%	YES		
301	31-Jul-12	8.10	1.9		961.22	5818517	594538	2094	142.6	2284.2	128.5	2058.4	11.0	98%	YES		
302	31-Jul-12	7.21	4.3		961.07	5818552	594456	2094	141.7	2269.8	126.5	2026.3	12.1	97%	YES		
303	31-Jul-12	6.66	2.7		961.11	5818571	594404	2094	138.8	2223.4	122.0	1953.9	14.0	93%	NO	#304	
304	31-Jul-12	6.64	2.5		961.15	5818572	594400	2094	142.3	2279.4	125.3	2007.1	13.6	95%	YES		
305	31-Jul-12	27.10	3.2		960.61	5818927	596157	2094	139.7	2237.8	124.7	1997.5	12.1	95%	YES		
306	31-Jul-12	26.21	5.3		960.70	5818873	596082	2094	144.3	2311.5	129.6	2076.0	11.3	99%	YES		
307	31-Jul-12	25.19	1.1		960.70	5818804	595996	2094	142.7	2285.8	127.6	2044.0	11.9	98%	YES		
308	31-Jul-12	24.32	3.0		960.75	5818761	595937	2094	143.7	2301.9	129.0	2066.4	11.4	99%	YES		
309	31-Jul-12	23.74	3.8		960.79	5818726	595888	2094	145.5	2330.7	129.5	2074.4	12.3	99%	YES		
310	31-Jul-12	21.75	4.9		960.68	5818711	595867	2094	143.1	2292.2	128.9	2064.8	11.0	99%	YES		
311	31-Jul-12	23.50	1.9		960.62	5818657	595800	2094	141.8	2271.4	126.6	2027.9	12.0	97%	YES		
312	31-Jul-12	20.97	0.7		960.53	5818555	595667	2094	141.8	2271.4	126.2	2021.5	12.3	97%	YES		
313	31-Jul-12	21.75	6.0		960.56	5818807	595727	2094	142.6	2284.2	127.4	2040.9	11.9	97%	YES		
314	1-Aug-12	19.84	4.1		960.49	5818491	595576	2094	142.4	2281.0	127.6	2044.0	11.6	98%	YES		
315	1-Aug-12	18.96	0.7		960.45	5818435	595507	2094	140.1	2244.2	124.5	1994.3	12.6	95%	YES		
316	1-Aug-12	17.98	4.6		960.64	5818379	595428	2094	149.1	2388.4	133.9	2144.8	11.4	102%	YES		
317	1-Aug-12	16.93	2.6		960.63	5818315	595345	2094	143.3	2295.4	129.2	2069.6	10.9	99%	YES		
318	1-Aug-12	16.01	4.8		960.39	5818262	595270	2094	141.5	2266.6	124.5	1994.3	13.6	95%	YES		
319	1-Aug-12	15.39	2.6		960.69	5818252	595218	2094	142.0	2274.6	126.5	2026.3	12.2	97%	YES		
320	3-Aug-12	27.35	1.0		960.94	5818941	596178	2094	141.8	2271.4	127.2	2037.5	11.4	97%	YES		
321	3-Aug-12	26.36	4.3		960.93	5818885	596099	2094	137.3	2199.3	121.7	1949.4	12.8	93%	NO		
322	3-Aug-12	25.41	5.6		960.92	5818827	596020	2094	140.3	2247.4	125.0	2002.3	12.3	96%	YES		
323	3-Aug-12	24.37	2.5		960.98	5818763	595934	2094	143.3	2295.4	128.5	2058.4	11.5	98%	YES		
324	3-Aug-12	23.41	5.2		960.87	5818707	595861	2094	141.4	2265.0	125.6	2011.9	12.6	96%	YES		
325	3-Aug-12	20.10	3.2		960.66	5818506	595597	2094	148.7	2381.9	134.2	2149.7	10.9	103%	YES		
326	3-Aug-12	22.30	2.6		960.86	5818638	595773	2094	140.1	2244.2	122.4	1960.7	14.5	94%	NO	#335	
327	3-Aug-12	21.41	4.0		960.88	5818586	595702	2094	137.3	2199.3	120.4	1928.6	14.1	92%	NO	#334, #335	
328	3-Aug-12	20.04	3.1		960.89	5818502	595592	2094	141.1	2260.2	124.2	1989.5	13.7	95%	YES		
329	3-Aug-12	19.05	1.3		960.82	5818442	595515	2094	141.5	2266.6	128.0	2050.4	10.5	98%	YES		
330	3-Aug-12	18.01	4.0		960.91	5818381	595430	2094	145.1	2324.3	129.9	2080.8	11.8	99%	YES		
331	3-Aug-12	17.01	2.0		960.86	5818320	595351	2094	142.3	2279.4	128.5	2058.4	10.8	98%	YES		
332	3-Aug-12	16.02	0.2		960.62	5818259	595273	2094	140.0	2242.6	126.1	2019.9	11.0	96%	YES		
333	3-Aug-12	15.13	3.8		960.92	5818262	595195	2094	142.9	2289.0	127.0	2034.3	12.5	97%	YES		
334	3-Aug-12	20.88	2.8		960.90	5818559	595668	2094	139.7	2237.8	125.0	2002.3	11.8	96%	YES		
335	3-Aug-12	22.24	5.5		960.85	5818637	595767	2094	139.4	2233.0	124.3	1991.1	12.2	95%	YES		
336	7-Aug-12	21.52	3.2	3	960.72	5819267	595981	2094	141.0	2258.6	124.2	1989.5	13.7	95%	YES		
337	7-Aug-12	30.60	4.5	3	960.67	5819192	596035	2094	141.5	2266.6	126.3	2007.1	12.9	96%	YES		
338	7-Aug-12	29.58	0.9	3	960.66	5819113	596094	2094	143.5	2298.6	127.3	2039.2	12.8	97%	YES		
339	7-Aug-12	28.63	3.0	3	960.64	5819035	596155	2094	140.4	2249.0	124.8	1999.1	12.5	95%	YES		
340	7-Aug-12	27.59	4.1	3	960.79	5818958	596194	2094	139.0	2226.6	124.8	1999.1	11.4	95%	YES		
341	7-Aug-12	26.39	1.6	4	960.89	5818884	596101	2094	137.6	2204.1	127.4	2040.8	8.0	97%	YES		
342	7-Aug-12	31.09	2.9	4	960.93	5819228	596010	2094	141.2	2261.8	125.8	2015.1	12.2	96%	YES		
343	7-Aug-12	30.04	1.4	4	961.00	5819149	596071	2094	143.2	2293.8	127.6	2044.0	12.2	98%	YES		
344	7-Aug-12	29.03	5.2	4	960.94	5819066	596129	2094	141.7	2269.8	127.9	2048.8	10.8	98%	YES		
345	7-Aug-12	28.05	3.1	4	960.98	5818989	596189	2094	141.1	2260.2	125.6	2011.9	12.3	96%	YES		
346	7-Aug-12	27.45	5.0	4	960.87	5818950	596184	2094	140.6	2252.2	126.2	2021.5	11.4	97%	YES		
347	8-Aug-12	32.26	3.1	3	960.70	5819319	596928	2094	145.7	2333.9	130.5	2090.4	11.6	100%	YES		
348	8-Aug-12	33.27	1.6	3	960.84	5819377	595845	2094	143.2	2293.8	127.2	2037.5	12.6	97%	YES		
349	8-Aug-12	34.05	5.2	3	960.72	5819412	595786	2094	141.3	2263.4	124.6	1995.9	12.3	95%	YES		
350	8-Aug-12	35.03	2.7	3	960.86	5819470	595704	2094	139.3	2231.4	122.8	1967.1	13.5	94%	NO	#352	
351	8-Aug-12	35.73	1.3	3	960.83	5819514	595643	2094	140.6	2252.2	124.2	1989.5	13.2	95%	YES		
352	8-Aug-12	35.04	2.4	3	960.88	5819472	595703	2094	145.4	2329.1	129.3	2071.2	12.4	99%	YES		

27 March 2013

Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
353	8-Aug-12	36.74	4.5	3	960.91	5819569	595558	2094	140.2	2245.8	124.6	1995.9	12.5	95%	YES		
354	8-Aug-12	37.76	1.1	3	960.80	5819626	595473	2094	141.2	2261.8	125.9	2016.7	12.2	96%	YES		
355	8-Aug-12	31.88	2.0	4	960.96	5819297	595959	2094	141.2	2261.8	124.9	2000.7	13.1	95%	YES		
356	8-Aug-12	32.86	5.2	4	961.03	5819352	595877	2094	141.2	2261.8	124.7	1997.5	14.0	95%	YES		
357	8-Aug-12	33.88	1.2	4	960.90	5819410	595797	2094	142.4	2281.0	126.4	2024.7	12.7	97%	YES		
358	8-Aug-12	34.75	3.0	4	961.15	5819465	595712	2094	143.2	2293.8	126.9	2032.7	12.9	97%	YES		
359	9-Aug-12	35.79	5.0	4	961.05	5819515	595634	2094	141.7	2269.8	126.7	2029.5	11.8	97%	YES		
360	9-Aug-12	36.59	2.0	4	961.20	5819560	595572	2094	143.5	2298.6	126.4	2024.7	13.6	97%	YES		
361	9-Aug-12	37.20	3.4	4	961.16	5819593	595521	2094	141.9	2273.0	126.6	2027.9	12.1	97%	YES		
362	9-Aug-12	37.68	1.4	4	961.11	5819621	595483	2094	142.5	2282.6	125.9	2016.7	13.2	96%	YES		
363	9-Aug-12	14.68	3.1	5	961.34	5818279	595150	2094	139.2	2229.8	124.4	1992.7	11.9	95%	YES		
364	9-Aug-12	13.70	4.3	5	961.48	5818316	595060	2094	143.9	2305.1	128.0	2050.4	12.4	98%	YES		
365	9-Aug-12	12.70	1.0	5	961.49	5818349	594967	2094	145.0	2322.7	131.7	2109.6	10.1	101%	YES		
366	9-Aug-12	11.69	2.3	5	961.40	5818387	594872	2094	142.7	2285.8	127.0	2034.3	12.3	97%	YES		
367	9-Aug-12	10.70	3.1	5	961.42	5818425	594779	2094	147.1	2356.3	132.2	2117.6	11.3	101%	YES		
368	9-Aug-12	9.72	4.2	5	961.47	5818461	594688	2094	142.2	2277.8	123.8	1983.1	14.7	95%	YES		
369	9-Aug-12	8.70	0.9	5	961.45	5818495	594593	2094	141.4	2265.0	124.6	1995.9	13.5	95%	YES		
370	9-Aug-12	7.73	3.1	5	961.52	5818529	594513	2094	140.9	2257.0	125.7	2013.5	12.1	96%	YES		
371	10-Aug-12	7.14	0.6	5	961.34	5818552	594447	2094	140.0	2242.6	123.9	1984.7	13.0	95%	YES		
372	10-Aug-12	6.62	4.9	5	961.37	5818575	594393	2094	141.2	2261.8	124.8	1999.1	14.2	95%	YES		
373	10-Aug-12	14.40	4.0	6	961.57	5818290	595126	2094	147.3	2359.5	132.5	2122.4	10.4	101%	YES		
374	10-Aug-12	13.55	5.0	6	961.79	5818325	595040	2094	143.6	2300.3	127.7	2045.6	12.8	98%	YES		
375	10-Aug-12	12.66	3.4	6	961.73	5818363	594962	2094	142.7	2285.8	124.1	1987.9	15.0	95%	YES		
376	10-Aug-12	11.72	4.3	6	961.66	5818388	594877	2094	141.8	2271.4	125.2	2005.5	13.2	96%	YES		
377	10-Aug-12	7.63	2.4	5	961.50	5818536	594494	2094	138.0	2210.5	123.0	1970.3	12.2	94%	NO	#378	
378	10-Aug-12	7.64	2.4	5	961.49	5818536	594494	2094	146.2	2341.9	130.3	2087.2	12.2	100%	YES		
379	10-Aug-12	4.96	1.4	1	960.55	5818633	594243	2094	142.1	2276.2	123.6	1979.9	14.9	95%	YES		
380	11-Aug-12	10.85	1.0	6	961.64	5818416	594795	2094	142.1	2276.2	129.5	2074.4	9.7	99%	YES		
381	11-Aug-12	9.84	3.0	6	961.76	5818454	594703	2094	142.3	2279.4	128.7	2061.6	10.6	98%	YES		
382	11-Aug-12	8.91	4.2	6	961.76	5818490	594616	2094	140.5	2250.6	127.6	2044.0	10.1	98%	YES		
383	11-Aug-12	8.02	1.1	6	961.78	5818516	594541	2094	143.4	2297.0	129.8	2079.2	10.5	99%	YES		
384	11-Aug-12	7.22	2.4	6	961.67	5818551	594456	2094	141.4	2265.0	126.7	2029.5	12.7	97%	YES		
385	11-Aug-12	6.71	4.9	6	961.65	5818569	594413	2094	140.0	2242.6	126.3	2023.1	10.9	97%	YES		
386	13-Aug-12	5.01	2.3	2	960.83	5818625	594266	2094	136.1	2180.1	120.6	1931.8	12.9	92%	NO	#387	
387	13-Aug-12	5.02	2.4	2	960.83	5818624	594265	2094	142.4	2281.0	127.9	2048.8	11.4	98%	YES		
388	13-Aug-12	47.04	4.0	2	960.65	5820004	594648	2094	140.5	2250.6	129.8	2079.2	8.3	99%	YES		
389	13-Aug-12	46.23	3.0	1	960.55	5820025	594532	1963	134.8	2159.3	122.4	1960.7	10.1	100%	YES		PE tie-in
390	13-Aug-12	40.31	3.1	3	960.92	5819789	595260	2094	141.2	2261.8	124.9	2000.7	13.1	96%	YES		
391	13-Aug-12	41.30	1.4	3	960.99	5819825	595178	2094	143.5	2298.6	126.3	2023.1	12.6	97%	YES		
392	13-Aug-12	42.28	3.4	3	960.95	5819877	595098	2094	142.0	2274.6	124.8	1999.1	13.8	96%	YES		
393	13-Aug-12	42.85	1.2	3	960.68	5819913	595049	2094	141.5	2266.6	124.7	1997.5	13.5	95%	YES		
394	13-Aug-12	42.70	5.1	3	960.85	5819941	594979	2094	141.7	2269.8	126.9	2032.7	11.7	97%	YES		
395	13-Aug-12	44.76	3.1	3	961.07	5819963	594870	2094	137.0	2194.5	116.5	1866.2	17.6	89%	NO		
396	13-Aug-12	45.17	1.5	3	961.07	5819972	594833	2094	138.2	2213.8	119.7	1917.4	15.5	92%	NO		
397	13-Aug-12	44.47	6.0	3	960.91	5819955	594900	2094	138.8	2223.4	120.5	1930.2	15.2	92%	NO		
398	13-Aug-12	44.54	2.1	3	960.94	5819957	594902	2094	142.0	2274.6	126.6	2027.9	12.2	97%	YES		
399	13-Aug-12	44.85	3.4	3	961.05	5819963	594865	2094	134.7	2157.7	110.0	1762.0	22.4	84%	NO		
400	13-Aug-12	47.13	3.2	3	960.91	5820005	594641	2094	130.0	2082.4	106.2	1701.2	22.5	81%	NO		
401	13-Aug-12	47.90	3.0	1	960.36	5820020	594563	2094	143.0	2290.6	125.0	2002.3	14.4	96%	YES		
402	14-Aug-12	15.21	3.9	5	961.23	5818261	595199	2094	140.6	2252.2	123.7	1981.5	13.9	95%	YES		
403	14-Aug-12	15.56	1.5	5	961.06	5818248	595229	2094	142.1	2276.2	127.2	2037.5	11.7	97%	YES		
404	14-Aug-12	16.51	4.2	5	961.25	5818292	595311	2094	144.6	2316.3	129.8	2079.2	11.4	99%	YES		
405	14-Aug-12	17.51	4.0	5	961.16	5818351	595391	2094	140.4	2249.0	125.6	2011.9	11.7	96%	YES		
406	14-Aug-12	18.48	2.0	5	960.89	5818408	595469	2094	141.6	2268.2	125.5	2010.3	12.8	96%	YES		
407	14-Aug-12	19.45	2.0	5	961.06	5818466	595545	2094	141.4	2265.0	124.6	1995.9	13.4	95%	YES		
408	14-Aug-12	40.51	2.0	4	961.28	5819789	595230	2094	141.4	2265.0	125.7	2013.5	12.4	96%	YES		
409	14-Aug-12	41.45	3.2	4	961.23	5819826	595178	2094	141.8	2271.4	125.6	2011.9	12.9	96%	YES		
410	14-Aug-12	42.10	4.6	4	961.23	5819870	595110	2094	135.7	2173.7	118.1	1891.8	15.0	90%	NO	#421, #424	
411	15-Aug-12	19.40	3.1	6	961.39	5818462	595541	2094	142.7	2285.8	126.3	2023.1	13.0	97%	YES		
412	15-Aug-12	18.52	1.1	6	961.20	5818410	595472	2094	144.3	2311.5	129.0	2066.4	11.8	99%	YES		
413	15-Aug-12	17.49	5.1	6	961.42	5818351	595387	2094	144.4	2313.1	128.9	2064.8	12.0	99%	YES		
414	15-Aug-12	14.77	2.5	6	961.55	5818275	595162	2094	140.6	2252.2	125.4	2008.7	12.2	96%	YES		
415	15-Aug-12	16.59	3.2	6	961.47	5818296	595317	2094	144.0	2306.7	128.3	2055.2	12.3	98%	YES		
416	15-Aug-12	15.60	5.0	6	961.42	5818250	595240	2094	139.2	2229.8	124.2	1989.5	12.3	96%	YES		
417	15-Aug-12	18.00	2.2	6	961.51	5818381	595432	2094	140.1	2244.2	125.4	2008.7	11.7	96%	YES		
418	15-Aug-12	48.10	3.1	3	961.60	5820023	594544	2094	144.6	2316.3	129.6	2076.0	11.6	99%	YES		
419	15-Aug-12	47.59	5.1	3	960.70	5819013	594594	2094	140.6	2252.2	124.2	1989.5	13.4	95%	YES		
420	15-Aug-12	44.35	2.6	4	961.20	5819955	594913	2094	139.3	2231.4	123.4	1976.7	12.9	94%	NO	#422	
421	17-Aug-12	42.02	2.4	4	961.25	5819863	595121	2094	129.6	2076.0	126.1	2019.9	10.7	96%	YES		
422	17-Aug-12	44.35	1.8	4	961.17	5819956	594914	2094	139.3	2231.4	124.9	2000.7	11.5	96%	YES		

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Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
423	17-Aug-12	43.46	5.1	4	961.20	5819937	594999	2094	142.8	2287.4	126.7	2029.5	12.6	97%	YES		
424	17-Aug-12	42.77	2.9	4	961.06	5819904	595059	2094	140.6	2252.2	125.4	2008.7	12.1	96%	YES		
425	17-Aug-12	42.07	4.6	4	961.24	5819864	595116	2094	143.1	2292.2	126.1	2052.0	11.7	98%	YES		
426	17-Aug-12	27.39	0.80	5	961.04	5818942	596181	2094	143.7	2301.9	127.9	2048.8	12.3	98%	YES		
427	17-Aug-12	26.47	3.00	5	961.23	5818889	596106	2094	140.8	2256.4	124.2	1989.5	13.4	95%	YES		
428	17-Aug-12	25.65	4.70	5	961.29	5818842	596040	2094	142.8	2287.4	126.4	2024.7	13.0	97%	YES		
429	17-Aug-12	24.76	3.20	5	961.22	5818787	595970	2094	143.1	2292.2	126.2	2053.6	11.6	98%	YES		
430	17-Aug-12	27.28	2.00	5-10cm	960.96	5818938	596172	2094	137.7	2205.7	124.2	1989.5	13.8	95%	YES		The test was performed after an excavator removed the top 10cm.
431	17-Aug-12	23.80	1.20	5	961.22	5818727	595894	2094	141.3	2263.4	125.5	2010.3	12.6	96%	YES		
432	17-Aug-12	22.81	3.50	5	961.24	5818670	595814	2094	142.7	2285.8	126.1	2019.9	13.1	96%	YES		
433	17-Aug-12	21.89	5.20	5	960.98	5818616	595740	2094	142.1	2276.2	124.8	1999.1	13.9	95%	YES		
434	17-Aug-12	21.12	0.70	5	961.09	5818566	595680	2094	140.2	2245.8	124.6	1995.9	12.5	95%	YES		
435	17-Aug-12	20.32	3.40	5	961.15	5818520	595615	2094	143.0	2290.6	126.6	2027.9	13.0	97%	YES		
436	17-Aug-12	27.15	2.30	6	961.36	5818930	596162	2094	140.7	2253.8	124.2	1989.5	13.3	95%	YES		
437	17-Aug-12	26.16	5.10	6	961.36	5818873	596081	2094	137.3	2199.3	120.6	1931.8	13.8	92%	NO	#438	
438	20-Aug-12	26.25	3.4	6	961.37	5818876	596088	2094	142.5	2282.6	130.1	2084.0	9.6	100%	YES		
439	20-Aug-12	25.32	0.6	6	961.46	5818818	596016	2094	143.2	2293.8	130.8	2095.2	9.5	100%	YES		
440	20-Aug-12	24.35	5.3	6	961.48	5818764	595936	2094	141.0	2258.6	128.0	2050.4	10.1	98%	YES		
441	20-Aug-12	23.46	3.6	6	961.52	5818709	595866	2094	141.8	2271.4	125.0	2002.3	13.5	96%	YES		
442	20-Aug-12	24.35	3.1	6-10cm	961.29	5818762	595937	2094	142.0	2274.6	125.7	2013.5	13.0	96%	YES		
443	20-Aug-12	22.37	5.4	6	961.36	5818645	595777	2094	146.0	2338.7	132.0	2114.4	10.6	101%	YES		
444	20-Aug-12	21.59	0.9	6	961.36	5818594	595718	2094	140.8	2255.4	125.0	2002.3	12.7	96%	YES		
445	20-Aug-12	20.15	5.0	5	961.14	5818510	595600	2094	140.6	2252.2	124.9	2000.7	12.6	96%	YES		
446	20-Aug-12	19.71	5.2	5	961.07	5818485	595560	2094	139.9	2241.0	124.2	1989.5	12.8	95%	YES		
447	20-Aug-12	20.03	1.0	6	961.43	5818633		2094	142.2	2277.8	126.8	2031.1	12.1	97%	YES		
448	20-Aug-12	20.24	4.3	6	961.38	5818516	595607	2094	144.9	2321.1	129.6	2076.0	11.8	99%	YES		
449	20-Aug-12	19.69	2.8	6	961.35	5818481	595565	2094	140.3	2247.4	124.2	1989.5	13.2	95%	YES		
450	20-Aug-12	31.45	4.5	5	961.39	5819259	595984	2094	144.1	2308.3	129.4	2072.8	11.4	99%	YES		
451	20-Aug-12	30.52	4.0	5	961.21	5819186	596040	2094	143.7	2301.9	127.9	2048.8	12.4	98%	YES		
452	20-Aug-12	29.53	0.5	5	961.16	5819109	596102	2094	142.4	2281.0	127.0	2034.3	12.2	97%	YES		
453	20-Aug-12	28.59	2.2	5	961.11	5819033	596157	2094	143.9	2305.1	127.9	2048.8	12.5	98%	YES		
454	20-Aug-12	27.52	4.7	5	961.12	5818954	596190	2094	142.8	2287.4	127.7	2045.6	11.8	98%	YES		
455	20-Aug-12	31.34	2.1	6	961.56	5819253	595992	2094	143.8	2303.5	129.1	2068.0	11.4	99%	YES		
456	20-Aug-12	30.47	4.5	6	961.50	5819182	596043	2094	142.3	2279.4	128.7	2061.6	10.6	98%	YES		
457	21-Aug-12	29.56	4.7	6	961.50	5819109	596097	2094	142.2	2277.8	126.6	2027.9	12.3	97%	YES		
458	21-Aug-12	28.61	3.1	6	961.44	5819033	596155	2094	146.3	2343.5	130.5	2090.4	12.1	100%	YES		
459	21-Aug-12	31.61	3.0	5	961.32	5819274	595975	2094	142.4	2281.0	126.1	2019.9	13.0	96%	YES		
460	21-Aug-12	32.51	5.7	5	961.20	5819330	595908	2094	142.0	2274.6	126.9	2032.7	11.9	97%	YES		
461	21-Aug-12	33.25	5.3	5	961.31	5819371	595846	2094	140.7	2253.8	124.4	1992.7	13.2	95%	YES		
462	21-Aug-12	33.93	0.8	5	961.16	5819413	595793	2094	143.1	2292.2	126.0	2018.3	13.6	96%	YES		
463	21-Aug-12	27.43	4.9	6	961.42	5818943	596175	2094	141.2	2261.8	126.0	2018.3	12.1	96%	YES		
464	21-Aug-12	31.60	2.7	6	961.53	5819273	595976	2094	142.2	2277.8	127.1	2036.9	11.9	97%	YES		
465	21-Aug-12	32.49	1.0	6	961.46	5819332	595912	2094	140.9	2257.0	125.2	2005.5	12.6	96%	YES		
466	21-Aug-12	33.45	3.9	6	961.57	5819384	595831	2094	140.8	2255.4	126.0	2018.3	11.8	96%	YES		
467	21-Aug-12	34.43	1.1	5	961.20	5819440	595752	2094	140.0	2242.6	122.3	1959.1	14.5	94%	NO	#486	
468	21-Aug-12	44.60	2.6	3	961.01	5819960	594889	2094	142.5	2282.6	125.0	2002.3	14.0	96%	YES		
469	21-Aug-12	45.45	5.1	3	960.89	5819973	594807	2094	142.5	2282.6	125.0	2002.3	14.0	96%	YES		
470	21-Aug-12	46.23	0.5	3	960.87	5819992	594729	2094	142.1	2276.2	125.3	2007.1	13.4	96%	YES		
471	21-Aug-12	47.28	3.1	3	960.76	5820008	595625	2094	141.9	2273.0	125.0	2002.3	13.4	96%	YES		
472	22-Aug-12	44.66	2.7	4	961.28	5819961	594881	2094	143.0	2290.6	127.0	2034.3	12.6	97%	YES		
473	22-Aug-12	45.64	1.3	4	961.16	5819981	594784	2094	141.3	2263.4	124.3	1991.1	13.7	95%	YES		
474	22-Aug-12	46.56	6.0	4	961.28	5819993	594693	2094	140.1	2244.2	123.6	1979.9	13.5	95%	YES		
475	22-Aug-12	47.51	3.1	4	961.03	5820012	594608	2094	142.2	2277.8	126.6	2027.9	12.4	97%	YES		
476	22-Aug-12	48.08	3.3	4	960.99	5820022	594549	2094	141.7	2269.8	125.9	2016.7	12.5	96%	YES		
477	22-Aug-12	4.93	4.2	3	961.24	5818635	594244	2094	141.4	2265.0	124.4	1992.7	13.7	95%	YES		
478	22-Aug-12	5.81	4.0	3	961.24	5818640	594230	2094	142.6	2284.2	125.1	2003.9	13.9	96%	YES		
479	22-Aug-12	5.19	4.0	4	961.32	5818607	594318	2094	143.6	2300.3	128.5	2058.4	11.7	98%	YES		
480	22-Aug-12	5.72	5.0	4	961.37	5819440	595752	2094	141.9	2273.0	125.5	2010.3	13.0	96%	YES		
481	22-Aug-12	6.46	3.1	4	961.39	5819960	594889	2094	140.0	2242.6	127.4	2040.8	9.9	97%	YES		
482	23-Aug-12	6.20	3.4	5	961.73	5818621	594279	2094	141.7	2269.8	125.9	2016.7	12.6	96%	YES		
483	23-Aug-12	6.03	0.7	5	961.59	5818592	594346	2094	141.2	2261.8	126.8	2015.1	12.9	96%	YES		
484	23-Aug-12	6.16	3.4	6	961.57	5818590	594356	2094	140.2	2245.8	124.1	1987.9	13.5	95%	YES		
485	23-Aug-12	34.61	4.2	5	961.39	5819449	595735	2094	141.0	2258.6	123.6	1979.9	14.1	95%	YES		
486	23-Aug-12	35.54	2.3	5	961.27	5819503	595657	2094	141.6	2268.2	125.0	2002.3	13.1	96%	YES		
487	23-Aug-12	36.31	0.9	5	961.39	5819599	595510	2094	145.7	2333.9	131.1	2100.0	11.2	100%	YES		
488	23-Aug-12	37.31	4.4	5	960.94	5819656	595428	2094	141.1	2260.2	124.6	1995.9	13.2	95%	YES		
489	23-Aug-12	38.32	3.6	6	961.58	5819384	595831	2094	140.9	2257.0	125.4	2008.7	12.4	96%	YES		
490	23-Aug-12	34.30	4.3	6	961.24	5819672	595400	2094	142.9	2289.0	125.9	2016.7	13.5	96%	YES		
491	23-Aug-12	37.00	3.4	6	961.60	5819583	595540	2094	141.8	2271.4	124.9	2000.7	13.5	96%	YES		
492	23-Aug-12	36.00	5.5	6	961.49	5819529	595618	2094	140.5	2250.6	124.8	1999.1	12.6	95%	YES		

27 March 2013

Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
493	23-Aug-12	35.04	2.3	6	961.59	5819471	595704	2094	141.7	2269.8	124.9	2000.7	13.5	96%	YES		
494	23-Aug-12	34.15	5.0	6	961.55	5819434	595759	2094	142.3	2279.4	125.8	2015.1	13.1	96%	YES		
495	23-Aug-12	40.64	4.0	5	961.54	5819786	595233	2094	141.2	2261.8	124.8	1999.1	13.2	95%	YES		
496	24-Aug-12	41.41	1.0	5	961.04	5819842	596181	2094	143.2	2293.8	126.8	2031.1	12.9	97%	YES		
497	24-Aug-12	42.41	4.3	5	961.43	5819883	595086	2094	142.1	2276.2	126.3	2023.1	12.5	97%	YES		
498	24-Aug-12	43.40	4.4	5	961.39	5819937	595006	2094	141.0	2258.6	125.0	2002.3	12.8	96%	YES		
499	24-Aug-12	44.10	3.2	5	961.49	5819950	594938	2094	141.5	2265.6	125.6	2011.9	12.6	96%	YES		
500	24-Aug-12	40.62	1.9	6	961.72	5819784	595238	2094	140.3	2247.4	124.5	1994.3	12.7	95%	YES		
501	24-Aug-12	41.59	4.3	6	961.92	5819833	595162	2094	141.0	2258.6	124.1	1987.9	13.7	95%	YES		
502	24-Aug-12	42.58	5.1	6	961.81	5819883	595086	2094	141.3	2263.4	125.5	2010.3	12.6	96%	YES		
503	24-Aug-12	43.55	1.4	6	961.63	5819942	594991	2094	139.9	2241.0	124.0	1986.3	12.8	95%	YES		
504	24-Aug-12	14.96	4.7	7	961.86	5818270	595177	2094	141.4	2265.0	127.1	2035.9	11.2	97%	YES		
505	24-Aug-12	13.97	1.6	7	961.94	5818303	595086	2094	138.5	2218.6	124.1	1987.9	11.6	95%	YES		
506	24-Aug-12	13.09	2.6	7	961.98	5818409	594824	2094	144.0	2306.7	129.7	2077.6	11.1	99%	YES		
507	24-Aug-12	13.09	2.6	7	962.01	5818333	595014	2094	141.1	2260.2	128.3	2055.2	10.0	98%	YES		
508	24-Aug-12	12.06	3.8	7	961.89	5818333	595014	2094	144.1	2308.3	130.4	2088.8	10.5	100%	YES		
509	24-Aug-12	11.12	4.9	7	962.01	5818376	594905	2094	141.6	2268.2	127.8	2047.2	10.8	98%	YES		
510	24-Aug-12	10.09	3.0	7	961.99	5818445	594722	2094	141.4	2265.0	125.4	2008.7	12.7	96%	YES		
511	27-Aug-12	14.57	2.7	8	962.12	5818281	595141	2094	140.8	2255.4	124.4	1992.7	13.2	95%	YES		
512	27-Aug-12	13.74	4.1	8	962.24	5818314	595068	2094	143.4	2297.0	125.3	2007.1	14.4	96%	YES		
513	27-Aug-12	13.03	0.7	8	962.19	5818339	595003	2094	142.1	2276.2	126.5	2026.3	12.4	97%	YES		
514	27-Aug-12	12.05	5.1	8	962.35	5818372	594908	2094	142.1	2276.2	125.8	2015.1	12.9	96%	YES		
515	27-Aug-12	11.13	2.0	8	962.24	5818404	594837	2094	140.5	2250.6	126.8	2031.1	10.8	97%	YES		
516	27-Aug-12	10.11	3.7	8	962.03	5818462	594636	2094	139.6	2236.2	126.3	2023.1	10.5	97%	YES		
517	27-Aug-12	9.12	1.3	7	962.03			2094	143.0	2290.6	128.5	2058.4	11.3	98%	YES		
518	27-Aug-12	8.11	4.3	7	961.95	5818524	594524	2094	142.6	2284.2	126.7	2029.5	12.6	97%	YES		
519	27-Aug-12	7.10	2.5	7	961.93	5818556	594444	2094	140.7	2253.8	124.3	1991.1	13.2	95%	YES		
520	27-Aug-12	6.14	2.0	7	961.83	5818589	594352	2094	141.3	2263.4	124.9	2000.7	13.1	96%	YES		
521	28-Aug-12	5.79	3.7	7	961.80	5818603	594326	2094	141.1	2260.2	125.0	2002.3	12.9	96%	YES		
522	28-Aug-12	4.99	2.1	7	961.92	5818629	594254	2094	141.1	2260.2	125.8	2015.1	12.1	96%	YES		
523	28-Aug-12	8.29	4.0	8	962.29	5818512	594556	2094	144.5	2314.7	129.9	2080.8	11.3	99%	YES		
524	28-Aug-12	9.29	0.9	8	962.15	5818466	594669	2094	141.2	2261.8	126.5	2026.3	11.6	97%	YES		
525	28-Aug-12	6.50	4.1	8	962.23	5818541	594484	2094	145.0	2322.7	129.7	2077.6	11.8	99%	YES		
526	28-Aug-12	5.64	2.3	8	962.21	5818574	594394	2094	140.4	2249.0	124.7	1997.5	12.6	95%	YES		
527	28-Aug-12	4.96	2.9	8	962.16	5818608	594310	2094	141.1	2260.2	125.1	2003.9	12.8	96%	YES		
528	28-Aug-12	4.96	3.5	8	962.16	5818635	594245	2094	139.0	2226.6	123.4	1976.7	12.7	94%	NO	#529	
529	28-Aug-12	5.06	3.5	8	962.18	5818627	594256	2094	141.0	2258.6	123.8	1983.1	13.9	95%	YES		
530	28-Aug-12	5.11	0.5	8	962.18	5818627	594257	2094	137.4	2200.9	119.8	1919.0	14.7	92%	NO	#531	
531	28-Aug-12	5.11	0.5	8	962.18	5818626	594261	2094	142.9	2289.0	127.0	2034.3	12.5	97%	YES		
532	29-Aug-12	27.15	3.5	7	961.56	5818831	596161	2094	142.0	2274.6	124.2	1989.5	14.4	95%	YES		
533	29-Aug-12	26.17	5.1	7	961.63	5818874	596082	2094	142.6	2284.2	127.1	2035.9	12.1	97%	YES		
534	29-Aug-12	24.25	5.4	7	961.58	5818758	595927	2094	141.6	2268.2	124.9	2000.7	13.3	96%	YES		
535	29-Aug-12	23.25	0.6	7	961.60	5818694	595850	2094	141.2	2261.8	124.7	1997.5	13.2	95%	YES		
536	29-Aug-12	22.34	3.9	7	961.63	5818642	595776	2094	142.7	2285.8	125.2	2005.5	14.0	96%	YES		
537	29-Aug-12	21.47	4.6	7	961.55	5818590	595706	2094	141.5	2268.6	125.2	2005.5	13.0	96%	YES		
538	29-Aug-12	20.47	1.4	7	961.74	5818526	595628	2094	142.7	2285.8	126.9	2032.7	12.5	97%	YES		
539	29-Aug-12	19.50	5.7	7	961.46	5818473	595547	2094	140.1	2244.2	124.4	1992.7	12.7	95%	YES		
540	29-Aug-12	18.62	3.7	7	961.45	5818418	595479	2094	144.0	2306.7	127.4	2040.8	13.0	97%	YES		
541	29-Aug-12	17.67	4.2	7	961.71	5818362	595403	2094	141.7	2269.8	126.6	2027.9	12.0	97%	YES		
542	29-Aug-12	16.79	2.8	7	961.65	5818308	595333	2094	144.3	2311.5	127.4	2040.8	13.3	97%	YES		
543	29-Aug-12	15.95	5.7	7	961.42	5818259	595264	2094	142.5	2282.6	126.4	2024.7	12.7	97%	YES		
544	29-Aug-12	15.10	2.6	7	961.63	5818260	595194	2094	142.4	2281.0	126.5	2026.3	12.6	97%	YES		
545	29-Aug-12	26.25	3.2	7	961.65	5818816	596008	2094	142.9	2289.0	126.0	2018.3	13.4	96%	YES		
546	4-Sep-12	27.26	5.1	8	961.83	5818940	596169	2094	142.2	2277.8	127.4	2040.8	11.6	97%	YES		
547	4-Sep-12	26.28	0.8	8	961.84	5818877	596093	2094	139.5	2234.6	125.4	2008.7	11.2	96%	YES		
548	4-Sep-12	24.50	1.2	8	961.86	5818770	595950	2094	142.1	2276.2	127.4	2040.8	11.5	97%	YES		
549	4-Sep-12	23.65	3.7	8	962.04	5818721	595881	2094	141.3	2263.4	126.8	2031.1	11.4	97%	YES		
550	4-Sep-12	26.04	5.2	8	961.89	5818886	596071	2094	142.4	2281.0	126.8	2031.1	12.3	97%	YES		
551	4-Sep-12	25.49	2.6	8	962.07	5818830	596028	2094	142.4	2281.0	128.2	2053.6	11.1	98%	YES		
552	4-Sep-12	22.79	4.3	8	961.89	5818669	595811	2094	140.0	2242.6	125.0	2002.3	12.0	96%	YES		
553	4-Sep-12	20.07	2.7	7	961.60	5818504	595595	2094	143.9	2305.1	124.9	2000.7	14.6	96%	YES		
554	4-Sep-12	21.81	1.4	8	961.79	5818608	595735	2094	141.9	2273.0	124.5	1994.3	13.9	95%	YES		
555	4-Sep-12	21.02	5.3	8	961.82	5818585	595669	2094	146.3	2343.5	131.4	2104.8	11.4	101%	YES		
556	4-Sep-12	20.06	5.2	8	961.77	5818506	595593	2094	139.1	2228.2	125.0	2002.3	11.3	96%	YES		
557	4-Sep-12	19.02	2.2	8	961.82	5818442	595512	2094	142.2	2277.8	126.4	2024.7	12.5	97%	YES		
558	4-Sep-12	18.21	0.7	8	961.79	5818391	595448	2094	140.7	2253.8	124.2	1989.5	13.4	95%	YES		
559	5-Sep-12	17.13	2.3	8	961.86			2094	141.7	2269.8	124.7	1997.5	13.7	95%	YES		
560	5-Sep-12	16.40	3.5	8	961.91	5818317	595344	2094	143.3	2295.4	127.6	2044.0	12.4	98%	YES		
561	5-Sep-12	15.74	5.8	8	961.69	5818251	595250	2094	143.3	2295.4	126.4	2024.7	13.4	97%	YES		
562	5-Sep-12	44.30	5.8	6	961.60	5819951	594918	2094	144.5	2314.7	130.3	2087.2	10.9	100%	YES		

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Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
563	5-Sep-12	45.26	1.6	5	961.44	5819973	594823	2094	145.3	2327.5	128.6	2060.0	13.0	98%	YES		
564	5-Sep-12	46.12	3.0	5	961.35	5819991	594716	2094	143.1	2292.2	127.1	2035.9	12.5	97%	YES		
565	5-Sep-12	47.34	5.8	5	961.33	5820007	594616	2094	143.9	2305.1	126.8	2031.1	13.5	97%	YES		
566	6-Sep-12	44.18	4.0	6	961.80	5819951	594929	2094	142.5	2282.6	125.6	2011.9	13.5	96%	YES		
567	6-Sep-12	45.03	1.2	6	961.75	5819988	594850	2094	142.3	2279.4	127.7	2045.6	11.4	98%	YES		
568	6-Sep-12	45.96	5.6	6	961.66	5819981	594755	2094	142.8	2287.4	126.3	2023.1	13.1	97%	YES		
569	6-Sep-12	47.05	4.9	6	961.71	5820002	594647	2094	140.7	2253.8	125.2	2005.5	12.4	96%	YES		
570	6-Sep-12	48.01	5.7	6	961.33	5820019	594554	2094	141.4	2265.0	125.6	2011.9	12.6	96%	YES		
571	6-Sep-12	31.56	4.3	7	961.66	5819269	595977	2094	144.3	2311.5	128.0	2050.4	12.8	98%	YES		
572	6-Sep-12	30.56	4.9	7	961.67	5819189	596036	2094	143.5	2298.6	127.1	2035.9	12.9	97%	YES		
573	6-Sep-12	29.67	0.3	7	961.61	5819120	596094	2094	139.0	2226.6	124.2	1989.5	12.0	95%	YES		
574	6-Sep-12	28.79	2.1	7	961.60	5819049	596145	2094	141.9	2273.0	124.8	1999.1	13.7	95%	YES		
575	6-Sep-12	28.03	4.0	7	961.68	5818986	596189	2094	142.0	2274.6	125.6	2011.9	13.1	96%	YES		
576	6-Sep-12	27.59	5.4	7	961.65	5818957	596191	2094	148.6	2380.3	132.4	2120.8	12.3	101%	YES		
577	7-Sep-12	27.39	5.1	8	961.82	5818941	596179	2094	143.0	2290.6	143.0	2290.6	11.3	109%	YES		
578	7-Sep-12	28.82	3.4	8	961.90	5819049	596144	2094	142.6	2284.2	142.6	2284.2	12.5	109%	YES		
579	7-Sep-12	29.91	0.7	8	962.01	5819138	596079	2094	148.0	2370.7	148.0	2370.7	10.3	113%	YES		
580	7-Sep-12	31.61	24.0	7	961.71	5819271	595979	2094	141.1	2260.2	141.1	2260.2	13.3	108%	YES		Daily sample
581	7-Sep-12	30.90	4.8	8	961.97	5819216	596016	2094	144.8	2319.5	144.8	2319.5	12.2	111%	YES		
582	7-Sep-12	32.60	4.9	7	961.70	5819335	595901	2094	143.0	2290.6	143.0	2290.6	12.7	109%	YES		
583	7-Sep-12	33.85	1.2	7	961.73	5819397	595816	2094	141.7	2269.8	141.7	2269.8	13.0	108%	YES		
584	7-Sep-12	34.87	3.8	7	961.84	5819462	595715	2094	142.1	2276.2	142.1	2276.2	12.4	109%	YES		
585	7-Sep-12	35.82	6.3	7	961.70	5819514	595633	2094	147.7	2365.9	147.7	2365.9	11.4	113%	YES		
586	7-Sep-12	36.59	1.9	7	961.90	5819561	595572	2094	141.9	2273.0	141.9	2273.0	1.7	109%	YES		
587	7-Sep-12	37.85	0.7	7	961.70	5819632	595468	2094	139.7	2237.8	124.1	1987.9	12.6	95%	YES		
588	7-Sep-12	31.90	0.5	8	961.96	5819298	595959	2094	143.2	2293.8	128.2	2053.6	11.7	98%	YES		
589	7-Sep-12	32.62	3.4	8	962.02	5819349	595862	2094	144.0	2306.7	129.3	2071.2	11.4	99%	YES		
590	7-Sep-12	37.53	4.7	8	962.07	5819610	595492	2094	146.1	2340.3	129.6	2076.0	12.7	99%	YES		
591	7-Sep-12	36.35	3.7	8	962.13	5819556	595574	2094	148.5	2378.7	133.9	2144.9	10.9	102%	YES		
592	7-Sep-12	35.62	0.5	6	961.94	5819508	595652	2094	145.2	2325.9	129.3	2071.2	12.3	99%	YES		
593	7-Sep-12	34.39	1.3	8	961.99	5819428	595754	2094	140.8	2255.4	125.2	2005.5	12.5	96%	YES		
594	7-Sep-12	33.67	4.4	8	961.97	5819399	595806	2094	139.9	2241.0	125.1	2003.9	11.9	96%	YES		
595	9-Sep-12	39.15	3.8	5	960.73	5819702	595358	2094	144.6	2316.3	132.7	2125.7	9.0	102%	YES		
596	9-Sep-12	40.01	6.0	5	960.60	5819749	595286	2094	138.6	2218.6	124.3	1991.1	11.4	95%	YES		
597	9-Sep-12	40.50	1.4	7	961.72	5819779	595248	2094	147.5	2362.7	128.5	2058.4	9.3	98%	YES		
598	9-Sep-12	41.34	2.9	7	962.00	5819824	595177	2094	146.7	2349.9	134.2	2149.7	9.3	103%	YES		
599	9-Sep-12	12.33	2.3	7	962.00	5819879	595095	2094	145.0	2322.7	131.1	2100.0	10.6	100%	YES		
600	9-Sep-12	43.06	5.1	7	961.76	5819919	595033	2094	142.8	2287.4	129.6	2076.0	10.1	99%	YES		
601	10-Sep-12	38.88	2.2	6	961.00	58195881	595382	2094	143.7	2301.9	128.0	2050.4	12.2	98%	YES		Daily sample
602	10-Sep-12	40.03	2.5	6	960.91	5819752	595286	2094	143.7	2301.9	126.9	2032.7	13.2	97%	YES		
603	10-Sep-12	40.58	6.1	6	962.21	5819779	595237	2094	142.4	2281.0	126.9	2032.7	12.2	97%	YES		
604	10-Sep-12	41.57	4.3	6	962.40	5819833	595160	2094	141.1	2260.2	125.1	2003.9	12.8	96%	YES		
605	10-Sep-12	42.22	1.5	6	962.30	5819875	595105	2094	139.2	2229.8	124.2	1989.5	12.1	95%	YES		
606	10-Sep-12	43.11	3.2	8	962.14	5819923	595030	2094	140.8	2257.0	124.5	1994.3	13.1	95%	YES		
607	10-Sep-12	14.57	2.2	9	962.30	5818282	595143	2094	141.0	2258.6	124.6	1995.9	13.2	95%	YES		
608	10-Sep-12	13.62	4.2	9	962.32	5818318	595655	2094	141.6	2268.2	126.1	2019.9	12.3	96%	YES		
609	10-Sep-12	12.66	0.9	9	962.43	5818350	594965	2094	140.8	2255.4	124.4	1992.7	12.9	95%	YES		
610	10-Sep-12	39.58	4.2	7	961.15	5819725	595322	2094	141.2	2261.8	124.2	1989.5	13.3	95%	YES		
611	11-Sep-12	12.14	2.7	9	962.52	5818371	594917	2094	145.0	2322.7	129.1	2068.0	12.3	99%	YES		
612	11-Sep-12	38.46	2.4	7	961.31	5819665	595413	2094	143.1	2292.2	125.6	2011.9	13.9	96%	YES		
613	11-Sep-12	39.77	4.5	7	961.18	5819736	595305	2094	142.5	2282.6	126.8	2031.1	12.4	97%	YES		
614	11-Sep-12	48.39	1.5	7	961.64	5820029	594516	2094	140.1	2244.2	124.5	1994.3	12.6	95%	YES		
615	11-Sep-12	47.31	0.6	7	961.78	5820009	594621	2094	144.4	2313.1	128.2	2053.6	12.6	98%	YES		
616	11-Sep-12	45.59	0.7	7	961.81	5819980	594791	2094	141.4	2265.0	124.8	1999.1	13.4	95%	YES		
617	11-Sep-12	44.94	4.7	7	961.94	5819986	594854	2094	144.2	2309.9	128.1	2052.0	12.5	98%	YES		
618	11-Sep-12	43.92	5.6	7	961.91	5819944	594952	2094	140.8	2255.4	124.5	1994.3	12.9	95%	YES		
619	11-Sep-12	45.66	3.5	7	961.84	5819978	594785	2094	141.7	2269.8	126.2	2021.5	12.4	97%	YES		
620	11-Sep-12	11.33	2.0	9	961.84			2094	141.8	2271.4	125.4	2008.7	13.0	96%	YES		
621	12-Sep-12	38.47	3.2	8	961.67	5819664	595415	2094	144.9	2321.1	128.4	2056.8	12.9	98%	YES		
622	12-Sep-12	39.47	2.9	8	961.84	5819720	595332	2094	140.4	2249.0	125.0	2002.3	12.3	96%	YES		
623	12-Sep-12	44.07	6.1	8	962.17	5819947	594939	2094	144.3	2311.5	129.4	2072.8	11.5	99%	YES		
624	12-Sep-12	45.96	5.7	8	962.32	5819981	594754	2094	140.2	2245.8	124.2	1989.5	13.2	95%	YES		
625	12-Sep-12	9.86	3.5	9	962.46	5818455	594705	2094	142.1	2276.2	125.9	2016.7	12.9	96%	YES		
626	12-Sep-12	18.31	4.1	9	962.45	5818432	594765	2094	140.1	2244.2	124.5	1994.3	12.6	95%	YES		
627	12-Sep-12	45.00	6.2	8	962.17	5819963	594850	2094	142.0	2274.6	126.8	2031.1	12.0	97%	YES		
628	12-Sep-12	46.98	3.2	8	962.24	5820002	594653	2094	141.0	2258.6	125.0	2002.3	12.8	96%	YES		
629	12-Sep-12	47.96	0.8	8	962.01	5820022	594558	2094	143.1	2292.2	128.7	2061.6	11.2	98%	YES		
630	12-Sep-12	12.71	1.1	10	962.77	5818349	594969	2094	142.3	2279.4	127.0	2034.3	12.1	97%	YES		
631	12-Sep-12	7.87	3.0	9	962.47	5818527	594517	2094	141.4	2265.0	125.8	2015.1	12.5	96%	YES		
632	12-Sep-12	8.89	0.4	9	962.44	5818487	594614	2094	145.0	2322.7	130.5	2090.4	11.8	100%	YES		

27 March 2013

Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
633	12-Sep-12	9.80	0.7	9	962.45	5818455	594697	2094	141.5	2266.6	125.4	2008.7	12.9	96%	YES		
634	12-Sep-12	11.75	2.0	10	962.70	5818385	594880	2094	141.6	2268.2	125.0	2002.3	13.3	96%	YES		
635	12-Sep-12	10.76	4.4	10	962.62	5818423	594790	2094	139.1	2228.2	124.2	1989.5	12.7	95%	YES		
636	13-Sep-12	9.73	4.2	10	962.72	5818461	594693	2094	142.1	2276.2	137.3	2199.3	11.7	105%	YES		
637	13-Sep-12	8.74	0.8	10	962.73	5818493	594560	2094	142.3	2279.4	125.6	2011.9	13.3	96%	YES		
638	13-Sep-12	8.03	4.7	10	962.51	5818523	594535	2094	141.2	2261.8	125.2	2005.5	12.8	96%	YES		
639	13-Sep-12	13.55	2.7	10	962.79	5818320	595046	2094	143.5	2298.6	127.8	2047.2	12.3	98%	YES		
640	13-Sep-12	14.37	1.7	10	962.56	5818289	595124	2094	141.5	2266.6	126.3	2023.1	12.1	97%	YES		
641	13-Sep-12	19.74	3.2	9	962.04	5818485	595568	2094	143.9	2305.1	124.3	1991.1	12.0	95%	YES		
642	13-Sep-12	17.74	4.4	9	962.13	5818366	595408	2094	141.1	2260.2	127.1	2035.9	11.1	97%	YES		
643	13-Sep-12	16.71	2.3	9	962.15	5818302	595327	2094	143.0	2290.6	129.0	2066.4	10.9	99%	YES		
644	13-Sep-12	15.70	3.0	9	961.95	5818298	595242	2094	141.0	2258.6	125.0	2002.3	12.9	96%	YES		
645	13-Sep-12	14.77	0.5	9	962.30	5818273	595181	2094	141.0	2258.6	125.2	2005.5	12.6	96%	YES		
646	14-Sep-12	27.54	5.0	9	962.18	5818956	596191	2094	141.4	2265.0	127.6	2044.0	10.9	98%	YES		
647	14-Sep-12	26.54	2.6	9	962.07	5818894	596113	2094	141.4	2265.0	125.2	2005.5	13.0	96%	YES		
648	14-Sep-12	25.54	0.5	9	962.25	5818832	596033	2094	139.3	2231.4	124.9	2000.7	11.5	96%	YES		
649	14-Sep-12	24.55	2.3	9	962.11	5818774	595953	2094	142.2	2277.8	126.4	2024.7	12.5	97%	YES		
650	14-Sep-12	23.51	4.2	9	962.13	5818713	595869	2094	143.5	2298.6	129.3	2071.2	11.0	99%	YES		
651	14-Sep-12	22.54	5.0	9	962.00	5818655	595791	2094	139.7	2237.8	124.4	1992.7	12.3	95%	YES		
652	14-Sep-12	19.49	1.8	10	962.30	5818469	595549	2094	143.0	2290.6	127.4	2040.8	12.3	97%	YES		
653	14-Sep-12	18.49	2.3	10	962.22	5818410	595469	2094	145.3	2327.5	134.6	2156.1	8.0	103%	YES		
654	14-Sep-12	17.47	4.9	10	962.41	5818351	595386	2094	142.2	2277.9	126.4	2024.7	12.5	97%	YES		
655	14-Sep-12	15.52	5.1	10	962.30	5818251	595232	2094	141.1	2260.2	124.4	1992.7	13.4	95%	YES		
656	14-Sep-12	14.71	2.9	10	962.58	5818278	595156	2094	140.0	2242.6	124.2	1989.5	12.7	95%	YES		
657	14-Sep-12	16.49	0.5	10	962.41	5818289	595310	2094	140.7	2253.8	124.3	1991.1	13.8	95%	YES		
658	14-Sep-12	21.52	5.4	9	961.85	5818594	595709	2094	139.0	2226.6	124.2	1989.5	12.0	95%	YES		
659	14-Sep-12	20.58	2.3	9	962.16	5818535	595636	2094	141.7	2269.8	125.5	2010.3	12.9	96%	YES		
660	14-Sep-12	27.44	0.7	10	961.41	5818945	596185	2094	141.0	2258.6	126.1	2019.9	11.8	96%	YES		
661	14-Sep-12	26.51	3.9	10	962.37	5818893	596109	2094	140.2	2245.8	124.2	1989.5	12.9	95%	YES		
662	14-Sep-12	25.52	2.6	10	962.46	5818833	596031	2094	141.5	2266.6	125.7	2013.5	12.6	96%	YES		
663	14-Sep-12	24.49	1.8	10	962.31	5818771	595949	2094	139.9	2241.0	124.3	1991.1	12.7	95%	YES		
664	14-Sep-12	23.51	4.3	10	962.42	5818713	595869	2094	140.6	2252.2	124.6	1995.9	12.9	95%	YES		
665	17-Sep-12	21.75	2.9	10	962.28	5818606	595729	2094	141.7	2269.8	128.8	2063.2	9.6	99%	YES		
666	17-Sep-12	22.61	0.5	10	962.30	5818656	595800	2094	141.7	2269.8	128.2	2053.6	10.5	98%	YES		
667	17-Sep-12	7.26	2.2	9	962.49	5818549	594462	2094	142.4	2281.0	125.6	2011.9	13.4	96%	YES		
668	17-Sep-12	6.32	4.2	9	962.42	5818585	594375	2094	141.1	2260.2	124.3	1991.1	13.5	95%	YES		
669	17-Sep-12	7.42	1.0	9	962.44	5818541	594477	2094	141.9	2273.0	124.4	1992.7	14.0	95%	YES		
670	17-Sep-12	5.91	4.2	9	962.39	5818618	594291	2094	141.2	2261.8	125.4	2008.7	12.6	96%	YES		
671	17-Sep-12	4.80	1.3	9	962.45	5818638	594231	2094	141.3	2263.4	125.3	2007.1	12.7	96%	YES		
672	17-Sep-12	7.69	3.2	10	962.76	5818535	594499	2094	140.7	2253.8	124.7	1997.5	12.9	95%	YES		
673	17-Sep-12	6.69	4.6	10	962.71	5818571	594409	2094	140.9	2257.0	124.2	1989.5	13.5	95%	YES		
674	17-Sep-12	5.75	0.7	10	962.59	5818602	594321	2094	140.9	2257.0	124.3	1991.1	13.4	95%	YES		
675	17-Sep-12	4.60	3.9	10	962.61	5818645	594221	2094	140.5	2250.6	124.4	1992.7	12.9	95%	YES		
676	17-Sep-12	4.98	3.2	10	962.70	5818634	594247	2094	145.8	2335.5	131.9	2112.8	10.6	101%	YES		
677	17-Sep-12	19.97	3.6	9	962.07	5818499	595587	2094	140.6	2252.2	124.3	1991.1	13.1	95%	YES		
678	17-Sep-12	19.92	5.1	10	962.28	5818497	595582	2094	142.1	2276.2	126.2	2021.5	12.6	97%	YES		
679	18-Sep-12	21.62	4.0	10	962.24	5818599	595718	2094	141.4	2265.0	124.2	1989.5	13.8	95%	YES		
680	18-Sep-12	20.72	4.7	10	962.36	5818546	595646	2094	141.4	2265.0	129.2	2069.6	12.0	99%	YES		
681	18-Sep-12	19.79	2.6	10	962.34	5818485	595567	2094	140.4	2249.0	124.3	1991.1	12.9	95%	YES		
682	18-Sep-12	16.46	3.7	11	962.66	5818289	595306	2094	140.7	2253.8	124.2	1989.5	13.4	95%	YES		
683	18-Sep-12	16.70	3.1	11	962.47	5818248	595242	2094	140.2	2245.8	124.2	1989.5	13.1	95%	YES		
684	18-Sep-12	14.72	4.1	11	962.75	5818276	595162	2094	144.2	2309.9	127.1	2035.9	14.0	97%	YES		
685	18-Sep-12	13.76	2.6	11	962.98	5818312	595067	2094	142.9	2289.0	126.6	2027.9	12.8	97%	YES		
686	18-Sep-12	12.79	2.3	11	962.97	5818347	594978	2094	141.6	2268.2	124.4	1992.7	13.9	95%	YES		
687	18-Sep-12	11.77	4.3	11	963.00	5818386	594882	2094	140.0	2242.6	123.7	1981.5	13.3	95%	YES		
688	19-Sep-12	16.29	4.2	12	962.87	5818279	595292	2094	142.2	2277.8	125.9	2016.7	13.0	96%	YES		
689	19-Sep-12	15.32	0.1	12	962.92	5818253	595212	2094	140.2	2245.8	124.3	1991.1	12.9	95%	YES		
690	19-Sep-12	14.30	1.2	12	963.20	5818291	595118	2094	140.8	2255.4	124.4	1992.7	13.2	95%	YES		
691	19-Sep-12	13.23	3.7	12	963.33	5818333	595018	2094	141.7	2269.8	124.9	2000.7	13.5	96%	YES		
692	19-Sep-12	12.21	3.3	12	963.29	5818370	594923	2094	139.8	2239.4	124.2	1989.5	12.6	95%	YES		
693	19-Sep-12	11.52	3.6	12	963.20	5818395	594860	2094	140.9	2257.0	125.1	2003.9	12.7	96%	YES		
694	19-Sep-12	10.82	0.5	11	963.05	5818417	594794	2094	140.2	2245.8	124.4	1992.7	12.7	95%	YES		
695	19-Sep-12	9.78	2.4	11	962.98	5818457	594698	2094	141.6	2268.2	124.7	1997.5	13.6	95%	YES		
696	19-Sep-12	9.04	0.6	11	963.02	5818482	594627	2094	142.8	2287.4	127.7	2046.6	11.9	98%	YES		
697	20-Sep-12	11.63	3.4	12	963.30	5818400	594846	2094	143.3	2295.4	125.7	2013.5	12.0	96%	YES		
698	20-Sep-12	10.37	1.3	12	963.36	5818435	594751	2094	145.4	2329.1	128.6	2060.0	13.1	98%	YES		
699	20-Sep-12	9.50	2.1	12	963.36	5818467	594671	2094	140.6	2252.2	124.2	1989.5	13.3	95%	YES		
700	20-Sep-12	8.49	3.7	12	963.47	5818506	594577	2094	141.2	2261.8	124.3	1991.1	13.5	95%	YES		
701	20-Sep-12	19.87	3.8	11	962.62	5818494	595576	2094	140.7	2253.8	124.4	1992.7	13.2	95%	YES		
702	20-Sep-12	18.96	3.7	11	962.48	5818439	595505	2094	140.6	2252.2	125.2	2005.5	12.3	96%	YES		

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Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
703	20-Sep-12	18.25	0.4	11	962.54	5818393	595450	2094	141.2	2261.8	125.1	2003.9	12.9	96%	YES		
704	20-Sep-12	17.22	1.5	11	962.67	5818333	595368	2094	141.4	2265.0	125.0	2002.3	12.9	96%	YES		
705	20-Sep-12	16.63	4.0	11	962.61	5818299	595320	2094	136.1	2180.1	120.4	1928.6	13.1	92%	NO		PASS - Added compaction had no effect.
707	24-Sep-12	21.67	3.5	11	962.50	5818502	595722	2094	142.0	2274.6	127.0	2034.3	11.8	97%	YES		
708	24-Sep-12	22.43	4.6	11	962.41	5818649	595782	2094	142.4	2281.0	129.2	2069.6	10.2	99%	YES		
709	24-Sep-12	27.53	0.3	11	962.66	5818941	596178	2094	142.1	2276.2	129.9	2080.8	9.4	99%	YES		
710	24-Sep-12	26.58	1.7	11	962.55	5818895	596115	2094	143.0	2290.6	128.7	2061.6	11.1	98%	YES		
711	24-Sep-12	25.69	2.2	11	962.62	5818841	595043	2094	149.9	2401.2	138.0	2210.5	8.6	106%	YES		
712	24-Sep-12	24.68	5.0	11	962.51	5818784	595582	2094	139.7	2237.8	126.7	2029.5	10.3	97%	YES		
713	24-Sep-12	24.29	3.8	11	962.72	5818760	595931	2094	147.2	2357.9	134.5	2154.5	9.5	103%	YES		
714	24-Sep-12	23.45	5.1	11	962.68	5818707	595886	2094	142.4	2281.0	129.8	2079.2	9.7	99%	YES		
715	24-Sep-12	21.09	0.8	11	962.73	5818564	595676	2094	145.8	2335.5	133.0	2130.5	9.6	102%	YES		
716	24-Sep-12	20.44	3.9	11	962.74	5818528	595624	2094	146.5	2346.7	134.5	2154.5	8.9	103%	YES		
717	25-Sep-12	20.09	1.1	11	962.56	5818505	595597	2094	142.3	2279.4	130.7	2093.6	8.9	100%	YES		
718	25-Sep-12	20.02	2.6	12	962.76	5818502	595591	2094	141.1	2260.2	130.6	2092.0	8.1	100%	YES		
719	25-Sep-12	19.09	0.7	12	962.82	5818444	595517	2094	149.4	2393.2	136.9	2192.9	9.2	105%	YES		
720	25-Sep-12	18.02	3.6	12	962.84	5818382	595430	2094	148.2	2373.9	137.6	2204.1	7.7	105%	YES		
721	25-Sep-12	17.07	2.3	12	962.95	5818324	595355	2094	139.0	2226.6	126.6	2027.9	9.7	97%	YES		
722	25-Sep-12	8.26	2.7	11	962.98	5818612	594535	2094	142.2	2277.8	131.5	2106.4	8.1	101%	YES		
723	25-Sep-12	7.56	4.7	11	963.05	5818540	594490	2094	141.7	2269.8	130.9	2096.8	8.2	100%	YES		
724	25-Sep-12	6.92	1.7	11	963.00	5818561	594430	2094	147.0	2354.7	133.8	2143.3	9.8	102%	YES		
725	25-Sep-12	6.25	2.9	11	962.96	5818586	594369	2094	146.9	2353.1	134.6	2156.1	9.2	103%	YES		
726	25-Sep-12	5.28	1.4	11	963.04	5818620	594277	2094	143.6	2300.3	130.3	2087.2	10.2	100%	YES		
727	26-Sep-12	27.25	2.62	12	962.94	5818936	596168	2094	143.2	2293.8	132.3	2119.2	8.3	101%	YES		
728	26-Sep-12	26.29	2.60	12	962.93	5818878	596091	2094	140.3	2247.4	130.4	2088.8	7.6	100%	YES		
729	26-Sep-12	25.27	1.77	12	963.00	5818817	596011	2094	144.4	2313.1	133.8	2143.3	7.9	102%	YES		
730	26-Sep-12	24.31	4.11	12	962.94	5818761	595933	2094	144.5	2314.7	133.7	2141.7	8.1	102%	YES		
731	26-Sep-12	23.30	3.08	12	962.97	5818699	595853	2094	145.3	2327.5	134.0	2146.5	8.5	103%	YES		
732	26-Sep-12	22.21	3.75	12	962.72	5818634	595765	2094	146.1	2340.3	135.1	2164.1	8.1	103%	YES		
733	26-Sep-12	20.36	1.15	12	962.96	5818533	595634	2094	142.2	2277.8	132.3	2119.2	7.5	101%	YES		
734	26-Sep-12	29.35	1.83	9	962.12	5819012	596172	2094	144.4	2313.1	130.3	2087.2	10.8	100%	YES		
735	26-Sep-12	29.04	4.62	9	962.12	5819068	596128	2094	140.6	2252.2	131.0	2098.4	8.3	100%	YES		Daily Moisture test
736	27-Sep-12	31.37	4.9	9	962.29	5819253	595988	2094	140.6	2252.2	124.8	1999.1	12.7	95%	YES		
737	27-Sep-12	30.42	1.3	9	962.27	5819180	596048	2094	141.7	2269.8	127.0	2034.3	11.6	97%	YES		
738	27-Sep-12				962.27			2094	142.0	2274.6	125.5	2010.3	13.1	96%	YES		
739	27-Sep-12	29.25	1.6	9	962.02	5819085	596118	2094	142.6	2284.2	126.9	2032.7	12.4	97%	YES		
740	27-Sep-12	32.31	4.5	9	962.25	5819319	595925	2094	141.7	2269.8	126.0	2018.3	12.5	96%	YES		
741	27-Sep-12	33.21	0.6	9	962.25	5819373	595852	2094	140.0	2242.6	124.8	1999.1	12.2	95%	YES		
742	27-Sep-12	34.28	0.5	9	962.25	5819433	595764	2094	139.2	2229.8	125.6	2011.9	10.87	96%	YES		
743	27-Sep-12	35.20	0.9	9	962.33	5819482	595689	2094	146.7	2349.9	130.7	2093.6	12.3	100%	YES		
744	27-Sep-12	35.17	0.3	9	962.19	5819537	595609	2094	142.2	2277.8	128.6	2063.2	10.3	99%	YES		
745	27-Sep-12	37.16	3.2	9	962.35	5819591	595523	2094	143.6	2300.3	127.5	2042.4	12.6	98%	YES		
746	27-Sep-12	38.14	2.4	9	961.92	5819647	595443	2094	147.7	2365.9	135.4	2168.9	9.1	104%	YES		
747	27-Sep-12	39.90	4.0	9	961.77	5819742	595297	2094	144.1	2308.3	128.8	2063.2	12.0	99%	YES		
748	27-Sep-12	5.04	1.1	12	963.25	5818629	594255	2094	139.9	2241.0	130.1	2084.0	7.5	100%	YES		
749	27-Sep-12	6.07	2.3	12	963.25	5818592	594351	2094	145.2	2325.9	133.9	2144.9	8.4	102%	YES		
750	27-Sep-12	7.02	4.5	12	963.22	5818560	594441	2094	142.9	2289.0	133.1	2132.1	7.3	102%	YES		
751	27-Sep-12	39.09	4.4	9	961.84	5819697	595342	2094	141.8	2271.4	125.9	2016.7	12.6	96%	YES		Daily Moisture Test
752	28-Sep-12	39.90	2.2	9	962.07	5819744	595297	2094	145.2	2325.9	132.9	2128.9	9.3	102%	YES		
753	28-Sep-12	39.90	2.5	9	962.35			2094	139.2	2229.8	128.7	2061.6	8.2	98%	YES		
754	28-Sep-12	40.90	1.0	9	962.35			2094	148.5	2378.7	135.8	2175.3	9.4	104%	YES		
755	28-Sep-12	41.75	4.5	9	962.35			2094	146.6	2348.3	135.9	2176.9	7.8	104%	YES		
756	28-Sep-12	42.45	2.5	9	962.35			2094	140.0	2242.6	128.3	2055.2	9.2	98%	YES		
757	28-Sep-12	42.95	3.5	9	962.35	5819914	595042	2094	139.8	2239.4	129.0	2065.4	8.5	99%	YES		
758	28-Sep-12	43.46	3.2	9	962.49	5819936	594997	2094	143.4	2297.0	133.0	2130.5	7.9	102%	YES		
759	28-Sep-12	44.02	0.9	9	962.49	5819950	594945	2094	141.5	2266.6	131.5	2106.4	7.6	101%	YES		
760	28-Sep-12	44.85	2.8	9	962.42	5819964	594863	2094	148.1	2368.4	137.9	2208.9	8.2	105%	YES		
761	28-Sep-12	45.85	3.1	9	962.46	5819981	594765	2094	142.6	2284.2	130.9	2096.8	8.9	100%	YES		
762	28-Sep-12	46.57	1.0	9	962.56	5819997	594694	2094	142.1	2276.2	131.1	2100.0	8.3	100%	YES		
763	28-Sep-12	47.55	3.2	9	962.35	5820012	594598	2094	136.4	2184.9	124.4	1992.7	9.6	95%	YES		
764	28-Sep-12	48.34	4.3	9	962.21	5820026	594519	2094	143.4	2297.0	132.5	2122.4	8.2	101%	YES		
765	28-Sep-12	7.79	1.7	12	963.27	5818529	594511	2094	144.8	2319.5	134.3	2151.3	7.9	103%	YES		
766	1-Oct-12	27.86	1.9	10	962.55	5818971	596200	2094	143.9	2305.1	127.5	2042.4	12.8	98%	YES		
767	1-Oct-12	28.84	2.9	10	962.49	5819050	596142	2094	141.3	2263.4	124.4	1992.7	13.6	95%	YES		
768	1-Oct-12	29.85	4.5	10	962.51	5819132	596079	2094	140.8	2255.4	125.1	2003.9	12.6	96%	YES		
769	3-Oct-12	19.88	2.6	12	963.12	5818493	595579	2094	144.9	2321.1	1341.0	21480.8	8.0	1026%	YES		
770	3-Oct-12	18.85	0.2	12	963.09	5818432	595502	2094	139.0	2226.6	129.2	2069.6	7.6	99%	YES		
771	3-Oct-12	17.97	4.0	12	963.22	5818380	595426	2094	141.3	2263.4	131.5	2106.4	7.5	101%	YES		
772	3-Oct-12	16.86	2.8	12	963.25	5818312	595338	2094	142.2	2277.8	129.8	2079.2	9.5	99%	YES		
773	3-Oct-12	15.86	3.5	12	963.11	5818250	595250	2094	139.0	2226.6	128.4	2056.8	8.2	98%	YES		

27 March 2013

Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
774	3-Oct-12	14.71	4.0	12	963.39	5818279	595157	2094	137.4	2200.9	127.0	2034.3	8.2	97%	YES		
775	3-Oct-12	13.72	1.1	12	963.58	5818312	595063	2094	146.6	2348.3	133.6	2143.3	9.5	102%	YES		
776	3-Oct-12	12.74	4.6	12	963.49	5818352	594974	2094	137.9	2208.9	126.1	2019.9	9.4	96%	YES		
777	3-Oct-12	11.76	1.8	12	963.55	5818304	594881	2094	145.1	2324.3	133.9	2144.9	8.4	102%	YES		
778	3-Oct-12	10.77	4.9	12	963.62	5818424	594789	2094	138.2	2213.8	126.1	2019.9	9.6	96%	YES		
779	3-Oct-12	9.77	1.6	12	963.70	5818457	594695	2094	148.9	2385.1	135.8	2175.3	9.6	104%	YES		
780	3-Oct-12	8.67	3.7	12	963.71	5818499	594594	2094	141.9	2273.0	131.7	2109.6	7.8	101%	YES		
781	3-Oct-12	27.08	3.5	12	963.30	5818927	596155	2094	145.6	2332.3	133.0	2130.5	9.5	102%	YES		
782	3-Oct-12	26.11	1.0	12	963.28	5818866	596078	2094	145.6	2332.3	135.1	2164.1	7.7	103%	YES		
783	3-Oct-12	25.05	0.9	12	963.19	5818804	595994	2094	143.0	2290.6	132.2	2117.6	8.2	101%	YES		
784	3-Oct-12	24.08	4.5	12	963.30	5818747	595913	2094	138.9	2225.0	126.5	2026.3	9.8	97%	YES		
785	3-Oct-12	23.09	2.1	12	963.21	5818686	595836	2094	145.4	2329.1	133.6	2140.1	8.8	102%	YES		
786	3-Oct-12	22.12	0.4	12	962.96	5818626	595759	2094	142.4	2281.0	131.6	2108.0	8.2	101%	YES		
787	3-Oct-12	21.12	2.8	12	963.15	5818568	595679	2094	142.7	2285.8	130.4	2088.8	9.5	100%	YES		
788	3-Oct-12	20.54	0.7	12	963.29	5818531	595633	2094	147.9	2369.1	136.2	2181.7	8.6	104%	YES		
789	4-Oct-12	39.46	3.8	10	962.80	5819719	595333	2094	142.3	2279.4	132.0	2114.4	7.8	101%	YES		
790	4-Oct-12	38.44	4.9	10	962.30	5819661	595417	2094	135.4	2168.9	124.6	1995.9	9.2	95%	YES		
791	4-Oct-12	37.46	2.6	10	962.79	5819608	59499	2094	140.1	2244.2	125.2	2005.5	11.9	96%	YES		
792	4-Oct-12	36.45	1.1	10	962.81	5819552	595584	2094	141.8	2271.4	129.2	2069.6	9.8	99%	YES		
793	4-Oct-12	35.47	4.3	10	962.67	5819495	595663	2094	138.9	2225.0	124.4	1992.7	11.7	95%	YES		
794	4-Oct-12	34.46	4.1	10	962.73	5819440	595717	2094	137.0	2194.5	125.9	2016.7	8.8	96%	YES		
795	4-Oct-12	33.44	0.5	10	962.63	5819385	595834	2094	145.4	2329.1	131.3	2103.2	10.7	100%	YES		
796	4-Oct-12	32.46	4.4	10	962.63	5819328	595913	2094	142.0	2274.6	127.4	2040.8	11.4	97%	YES		
797	4-Oct-12	31.44	1.7	10	962.57	5819251	595986	2094	143.4	2297.0	130.6	2095.2	9.8	100%	YES		
798	4-Oct-12	30.48	3.8	10	962.56	5819182	596042	2094	138.6	2220.2	126.4	2024.7	9.6	97%	YES		
799	9-Oct-12	27.09	1.9	14	963.56	5818826	596156	2094	142.2	2277.8	131.4	2104.8	8.2	101%	YES		
800	9-Oct-12	26.08	4.5	14	963.61	5818867	596074	2094	133.7	2141.7	126.9	2032.7	5.4	97%	YES		
801	9-Oct-12	25.13	2.2	14	963.52	5818809	594999	2094	144.8	2319.5	135.9	2176.9	6.5	104%	YES		
802	9-Oct-12	24.12	1.1	14	963.67	5818748	595919	2094	140.2	2245.8	131.0	2098.4	7.0	100%	YES		
803	9-Oct-12	23.12	4.0	14	963.42	5818689	595837	2094	144.8	2319.5	134.4	2152.9	7.7	103%	YES		
804	9-Oct-12	22.15	2.0	14	963.38	5818630	595761	2094	144.2	2309.9	134.4	2152.9	7.3	103%	YES		
805	9-Oct-12	21.10	0.4	14	963.49	5818565	595678	2094	143.7	2301.9	134.8	2159.3	6.6	103%	YES		
806	9-Oct-12	8.67	3.8	14	964.03	5818499	594594	2094	137.9	2208.9	128.4	2056.8	7.4	98%	YES		
807	9-Oct-12	9.66	1.1	14	964.06	5818460	594686	2094	137.0	2194.5	128.7	2061.6	6.4	98%	YES		
808	9-Oct-12	10.67	2.0	14	964.06	5818425	594780	2094	147.7	2365.8	137.5	2202.5	7.5	105%	YES		
809	9-Oct-12	11.70	4.4	14	963.81	5818389	594877	2094	140.2	2245.8	131.1	2100.0	6.9	100%	YES		
810	9-Oct-12	12.69	2.0	14	963.96	5818350	594967	2094	145.2	2325.9	135.8	2175.3	6.9	104%	YES		
811	9-Oct-12	13.67	2.9	14	963.89	5818316	595059	2094	148.0	2370.7	137.0	2194.5	8.1	105%	YES		
812	9-Oct-12	14.69	4.7	14	963.63	5818281	595154	2094	134.4	2152.9	127.1	2035.9	5.8	97%	YES		
813	9-Oct-12	15.71	2.5	14	963.43	5818248	595241	2094	138.0	2210.5	129.4	2072.8	6.7	99%	YES		
814	9-Oct-12	16.69	0.2	14	963.57	5818300	595325	2094	139.5	2234.6	131.6	2108.0	6.0	101%	YES		
815	9-Oct-12	17.69	3.2	14	963.62	5818362	595404	2094	139.1	2228.2	130.4	2088.8	6.7	100%	YES		
816	9-Oct-12	18.70	4.3	14	963.30	5818425	595484	2094	133.7	2141.7	124.3	1991.1	7.6	95%	YES		
817	9-Oct-12	19.69	2.6	14	963.39	5818482	595564	2094	147.2	2357.9	136.2	2213.8	8.5	106%	YES		
818	9-Oct-12	6.23	1.9	13	963.62	5818586	594366	2094	141.9	2273.0	129.6	2076.0	9.5	99%	YES		
819	9-Oct-12	7.25	1.8	13	962.62	5818549	594461	2094	143.6	2300.3	131.0	2098.4	9.6	100%	YES		
820	9-Oct-12	5.57	4.5	13	963.48	5818613	594306	2094	140.6	2252.2	126.9	2064.8	9.1	99%	YES		
821	9-Oct-12	4.57	3.0	13	963.65	5818645	594219	2094	147.8	2367.5	136.1	2180.1	8.6	104%	YES		
822	11-Oct-12	27.94	1.7	11	962.79	5818980	596196	2094	137.8	2207.3	137.8	2207.3	8.3	105%	YES		
823	11-Oct-12	28.91	2.2	11	962.87	5819058	596137	2094	144.9	2321.1	144.9	2321.1	8.3	111%	YES		
824	11-Oct-12	29.94	3.9	11	962.84	5819139	596074	2094	144.4	2313.1	144.4	2313.1	8.1	110%	YES		
825	11-Oct-12	30.94	4.6	11	962.84	5819218	596014	2094	141.1	2260.2	141.1	2260.2	7.8	108%	YES		
826	11-Oct-12	31.98	5.0	11	963.03	5819301	595951	2094	144.1	2308.3	144.1	2308.3	7.9	110%	YES		
827	11-Oct-12	32.92	2.5	11	962.96	5819354	595876	2094	139.9	2241.0	139.9	2241.0	9.0	107%	YES		
828	11-Oct-12	33.95	0.5	11	962.96	5819414	595791	2094	132.6	2124.0	132.6	2124.0	7.3	101%	YES		
829	11-Oct-12	34.93	3.0	11	963.07	5819466	595709	2094	144.7	2317.9	144.7	2317.9	8.9	111%	YES		
830	11-Oct-12	35.94	3.8	11	962.96	5819522	595624	2094	141.3	2263.4	141.3	2263.4	8.9	108%	YES		
831	11-Oct-12	36.94	0.6	11	962.92	5819581	595543	2094	144.1	2308.3	144.1	2308.3	8.7	110%	YES		
832	11-Oct-12	37.94	3.3	11	962.85	5819634	595458	2094	143.6	2300.3	143.6	2300.3	10.2	110%	YES		
833	11-Oct-12	38.93	2.2	11	962.51	5819690	595377	2094	142.1	2276.2	142.1	2276.2	10.1	109%	YES		
834	15-Oct-12	48.54	0.7	10	962.83	5820032	594501	2094	143.8	2303.5	128.1	2052.0	12.2	98%	YES		
835	15-Oct-12	47.19	3.2	10	962.87	5820005	594633	2094	149.5	2394.8	134.6	2156.1	11.1	103%	YES		
836	15-Oct-12	46.22	4.6	10	962.83	5819987	594729	2094	144.7	2317.9	127.3	2039.2	13.7	97%	YES		
837	15-Oct-12	45.19	0.3	10	962.85	5819972	594831	2094	141.0	2258.6	124.5	1994.3	12.5	95%	YES		
838	15-Oct-12	44.21	3.4	10	962.90	5819951	594926	2094	147.4	2361.1	130.7	2093.6	12.8	100%	YES		
839	15-Oct-12	43.21	2.0	10	962.82	5819929	595022	2094	144.9	2321.1	126.1	2019.9	14.9	96%	YES		
840	15-Oct-12	42.21	1.7	10	962.96	5819874	595105	2094	142.6	2284.2	125.3	2007.1	13.8	96%	YES		
841	15-Oct-12	41.19	3.7	10	963.08	5819815	595189	2094	138.4	2217.0	125.0	2002.3	11.1	96%	YES		
842	15-Oct-12	40.21	1.5	10	962.84	5819762	595271	2094	140.8	2255.4	124.3	1991.1	12.5	95%	YES		
843	16-Oct-12	45.88	4.8	11	963.07	5819980	594762	2094	144.4	2313.1	135.0	2162.5	6.9	103%	YES		

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Compaction Testing Results (MPMC)

Test #	Date Tested	Stn	Offset S/F	Lift	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (lb/ft^3)	Wet Density (kg/m^3)	Dry Density (lb/ft^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Re-tests	Comments
844	16-Oct-12	44.85	2.8	11	963.03	5819863	594864	2094	140.8	2255.4	128.7	2061.6	9.4	98%	YES		
845	16-Oct-12	43.97	1.0	11	963.13	5819949	594951	2094	141.5	2266.6	130.3	2087.2	8.6	100%	YES		
846	16-Oct-12	42.96	3.5	11	963.03	5819914	595041	2094	142.3	2279.4	130.4	2088.8	9.2	100%	YES		Daily Moisture Test
847	16-Oct-12	41.92	4.3	11	963.31	5819858	595123	2094	138.3	2215.4	126.4	2024.7	9.2	97%	YES		
848	16-Oct-12	40.98	4.4	11	963.22	5819501	595208	2094	138.7	2221.8	127.4	2040.8	8.9	97%	YES		
849	16-Oct-12	48.63	0.3	11	963.30	5820034	594492	2094	135.2	2165.7	124.3	1991.1	8.7	95%	YES		
850	16-Oct-12	47.76	3.2	11	962.87	5820051	594577	2094	141.6	2268.2	130.1	2084.0	8.8	100%	YES		
851	16-Oct-12	46.73	4.0	11	963.05	5819996	594678	2094	137.5	2202.5	125.3	2007.1	9.7	96%	YES		
852	17-Oct-12	27.46	3.1	12	963.14	5818950	596185	2094	145.1	2324.3	133.3	2135.3	8.9	102%	YES		
853	17-Oct-12	28.68	0.7	12	963.02	5819040	596153	2094	144.2	2309.9	132.0	2114.4	9.3	101%	YES		
854	17-Oct-12	29.71	3.4	12	963.14	5819121	596089	2094	145.0	2322.7	133.0	2130.5	9.0	102%	YES		
855	17-Oct-12	30.74	4.6	12	963.15	5819203	596026	2094	143.1	2292.2	130.6	2092.0	9.5	100%	YES		
856	17-Oct-12	31.69	0.4	12	963.15	5819281	595972	2094	146.5	2346.7	134.1	2148.1	9.3	103%	YES		
857	17-Oct-12	32.69	2.2	12	963.28	5819342	595895	2094	139.5	2234.6	127.2	2037.5	9.7	97%	YES		
858	17-Oct-12	33.70	3.9	12	963.16	5819397	595810	2094	148.7	2381.9	136.8	2191.3	8.7	105%	YES		
859	17-Oct-12	34.71	0.5	12	963.29	5819456	595728	2094	141.6	2268.2	131.2	2101.6	7.9	100%	YES		
860	17-Oct-12	35.70	2.7	12	963.29			2094	147.3	2359.5	137.6	2204.1	7.1	105%	YES		
861	17-Oct-12	36.71	4.3	12	963.30	5819664	595562	2094	140.8	2255.4	131.0	2098.4	7.6	100%	YES		
862	17-Oct-12	37.70	0.3	12	963.21	5819623	595480	2094	142.4	2281.0	130.6	2092.0	9.0	100%	YES		
863	17-Oct-12	38.70	2.6	12	962.80	5819677	595396	2094	142.8	2287.4	131.9	2112.8	8.3	101%	YES		
864	17-Oct-12	39.73	4.1	12	963.24	5819733	595309	2094	145.5	2330.7	135.3	2167.3	7.5	104%	YES		
865	17-Oct-12	40.44	1.9	12	963.30	5819774	595252	2094	141.7	2269.8	129.9	2080.8	9.1	99%	YES		
866	17-Oct-12	41.42	2.8	12	963.54	5819829	595170	2094	140.8	2255.4	128.4	2056.8	9.7	98%	YES		
867	17-Oct-12	42.36	4.6	12	963.61	5819881	595089	2094	138.7	2221.8	126.9	2032.7	9.8	97%	YES		Daily Moisture Test
868	18-Oct-12	43.54	0.9	12	963.38	5819941	594992	2094	148.2	2373.9	137.7	2205.7	7.6	105%	YES		
869	18-Oct-12	44.56	3.2	12	963.36	5819958	594892	2094	143.3	2295.4	132.6	2124.0	8.1	101%	YES		
870	18-Oct-12	45.54	4.3	12	963.39	5819974	594799	2094	138.9	2225.0	129.1	2068.0	7.6	99%	YES		
871	18-Oct-12	46.54	1.3	12	963.48	5819985	594698	2094	140.9	2257.0	130.5	2090.4	8.0	100%	YES		
872	18-Oct-12	47.56	5.0	12	963.31	5820010	594596	2094	142.7	2285.8	127.7	2045.6	11.8	98%	YES		
873	18-Oct-12	48.33	2.1	12	963.38	5820027	594522	2094	137.8	2207.3	125.1	2003.9	10.1	96%	YES		Daily Moisture Test
874	23-Oct-12	27.91	2.2	13	963.50	5818976	596197	2094	139.8	2239.4	127.8	2047.2	9.4	98%	YES		
875	23-Oct-12	28.90	1.3	13	963.37	5819058	596138	2094	143.5	2298.6	130.5	2090.4	9.9	100%	YES		
876	23-Oct-12	29.90	3.8	13	963.48	5819136	596077	2094	140.9	2257.0	128.4	2056.8	9.8	98%	YES		
877	23-Oct-12	30.90	1.5	13	963.53	5819217	596019	2094	137.5	2202.5	124.9	2000.7	10.2	96%	YES		
878	23-Oct-12	31.90	5.1	13	963.51	5819294	595957	2094	134.4	2152.8	127.1	2036.9	5.8	97%	YES		
879	23-Oct-12	32.88	3.1	13	963.54	5819352	595878	2094	137.3	2199.3	125.8	2015.1	9.2	96%	YES		

Compaction Testing Results (AMEC)

Test #	Date Tested	Stn	Offset S/F	Elevation	Northing	Easting	Max Density (kg/m^3)	Wet Density (kg/m^3)	Dry Density (kg/m^3)	Moisture (%)	Density (%)	Pass	Depth (mm)	Comments
1	6-Jul-12	4.70	-8.0	963.5			2094	2242.0	1983.0	13.0%	95%	YES	300	native
2	6-Jul-12	4.80	-2.0	962.2	5818644	594221	2094	2248.7	1986.3	13.2%	95%	YES	300	native
3	6-Jul-12	4.90	-7.0	962.0	5818627	594224	2094	2150.3	1873.0	14.7%	89%	NO	300	native
4	6-Jul-12	4.90	-7.0	962.0	5818627	594224	2094	2190.3	1879.9	16.5%	90%	NO	200	native
5	6-Jul-12	4.90	-7.0	962.0	5818627	594224	2094	2183.2	1879.1	16.1%	90%	NO	300	native
6	9-Jul-12	24.42	1.3	960.4	5818765	595043	2094	2224.8	2035.5	9.2%	97%	YES	300	Test # 169
7	9-Jul-12	24.42	1.3	960.4	5818765	595943	2094	2246.3	2059.0	9.2%	98%	YES	200	Test # 169
8	10-Jul-12	27.20	1.8	960.4	5818932	596166	2094	2291.7	2098.6	9.2%	100%	YES	300	Test # 173
9	10-Jul-12	27.20	1.8	960.4	5818932	596166	2094	2303.7	2103.0	9.5%	100%	YES	200	Test # 173
10	28-Aug-12	5.63	2.9	962.2	5818608.4	594310	2094	2278.0	2053.0	10.9%	98%	YES	300	
11	28-Aug-12	4.96	0.5	962.2	5818627.5	594256	2094	2222.3	2012.4	10.4%	96%	YES	300	
12	28-Aug-12	5.11	0.5	962.2	5818625.7	594261	2094	2233.1	1995.6	11.8%	95%	YES	300	
13	29-Aug-12	27.15	3.0	961.6	5818931	596161	2094	2316.7	2094.3	10.6%	100%	YES	300	
14	29-Aug-12	27.15	3.0	961.6	5818931	596161	2094	2292.4	2072.5	10.6%	99%	YES	200	
15	29-Aug-12	27.15	3.0	961.6	5818931	596161	2094	2289.6	2062.1	11.0%	98%	YES	100	
16	20-Sep-12	17.79	4.5	962.7	5818369	595412	2094	2267.3	2049.9	10.6%	98%	YES	300	
17	20-Sep-12	17.79	4.5	962.7	5818369	595412	2094	2265.3	2050.5	10.4%	98%	YES	200	
18	21-Sep-12	21.77	5.0	962.7	5818943	596174	2094	2274.3	2056.0	10.6%	98%	YES	300	
19	21-Sep-12	21.40	0.3	962.6	5818894	596116	2094	2135.4	1905.0	12.0%	91%	NO	300	
20	21-Sep-12	21.40	0.3	962.6	5818894	596116	2094	2330.8	2170.2	7.3%	104%	YES	300	retest 19
21	21-Sep-12	20.93	0.5	962.7	5818841	596044	2094	2330.1	2140.3	10.7%	102%	YES	300	
22	21-Sep-12	20.36	3.0	968.6	5818181	595959	2094	2330.5	2112.8	10.3%	101%	YES	300	
23	21-Sep-12	19.45	0.5	962.6	5818670	595819	2094	2217.9	1988.2	11.5%	95%	YES	300	
24	21-Sep-12	18.88	5.0	962.5	5818613	59536	2094	2236.4	2000.5	11.7%	96%	YES	300	

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MOISTURE TESTING RESULTS (Zone S) - AMEC LABORATORY

Sample #	Date	Pan Tare (g)	Total Weight of Sample Wet (g)	Weight of >19mm (g)	Wet Sample + Tare (Min 700g)	Dry Sample + Tare (g)	Total Weight of Sample Dry (g)	Oversize (%)	Moisture (%)	FIELD MOISTURE	Moisture Variance
79	22-Jun-12	629.90	5190.5	0.0	1659.5	1547.3	4624.9	0.0%	12.2%	10.8%	1.4%
101	28-Jun-12	0	7114.8	247.5	6867.3	6221.2	6445.4	3.8%	10.4%	12.1%	-1.7%
136	30-Jun-12	0	8237.4	306.4	7931.0	7207.6	7485.1	4.1%	10.0%	8.3%	1.7%
169	9-Jul-12	609	11181.6	590.4	1693.6	1583.3	10044.5	5.9%	11.3%	10.2%	1.1%
194	12-Jul-12	703.89	10002.1	795.2	1683.7	1573.5	8876.9	9.0%	12.7%	10.5%	2.2%
213	13-Jul-12	692.38	10000.9	924.9	1704.0	1592.8	8901.0	10.4%	12.4%	11.0%	1.4%
240	16-Jul-12	692.39	7131.3	711.4	1987.9	1835.8	6293.9	11.3%	13.3%	11.5%	1.8%
269	18-Jul-12	509.3	4593.8	349.0	2031.2	1920.1	4258.4	8.2%	7.9%	9.2%	-1.3%
273	20-Jul-12	509.2	5342.2	430.0	2561.4	2413.1	4956.2	8.7%	7.8%	9.0%	-1.2%
281	26-Jul-12	693.8	8647.6	713.1	2102.4	1961.4	7782.0	9.2%	11.1%	12.8%	-1.6%
289	29-Jul-12	893.14	7978.7	858.6	2016.4	1887.2	7060.8	12.2%	13.0%	12.7%	0.3%
308	31-Jul-12	700.21	6359.8	791.8	2748.0	2525.6	5669.2	14.0%	12.2%	11.4%	0.8%
319	1-Aug-12	696.6	7381.6	319.5	1986.1	1838.7	6536.5	4.9%	12.9%	12.2%	0.7%
335	3-Aug-12	594.2	3745.1	643.5	3695.8	3399.2	3387.0	19.0%	10.6%	12.2%	-1.6%
353	8-Aug-12	692.14	4187.6	432.8	2846.7	2647.5	3800.4	11.4%	10.2%	12.5%	-2.3%
364	11-Aug-12	692.2	5197.2	493.2	1969.4	1842.3	4680.0	10.5%	11.1%	12.7%	-1.6%
392	13-Aug-12	689.23	4904.9	331.0	2647.5	2441.3	4388.4	7.5%	11.6%	13.6%	-2.0%
428	17-Aug-12	0	5158.0	501.9	4648.2	4162.8	4619.4	10.9%	11.7%	13.0%	-1.3%
449	20-Aug-12	0	4548.5	523.8	4024.7	3615.8	4086.4	12.8%	11.3%	13.2%	-1.9%
463	21-Aug-12	0	4169.1	593.2	3575.9	3192.8	3722.4	15.9%	12.0%	12.1%	-0.1%
480	22-Aug-12	688.12	3560.8	454.4	2110.6	1961.3	3188.9	14.3%	11.7%	13.0%	-1.3%
487	23-Aug-12	691.1	4107.6	390.4	2938.5	2719.3	3707.0	10.5%	10.6%	11.2%	-0.4%
500	24-Aug-12	698.6	5102.4	599.2	3115.9	2865.2	4573.2	13.1%	11.6%	12.7%	-1.1%
552	4-Sep-12	692.1	4955.2	1751.1	3896.2	3600.0	4497.1	38.9%	10.2%	12.0%	-1.8%
565	5-Sep-12	0	4011.8	232.3	3779.3	3355.0	3355.0	6.9%	12.6%	13.5%	-0.9%
566	6-Sep-12	0	7684.0	891.9	6146.2	5482.7	5482.7	16.3%	12.1%	13.5%	-1.4%
577	7-Sep-12	0	5183.0	396.1	4777.9	4343.2	4343.2	9.1%	10.0%	11.3%	-1.3%
601	10-Sep-12	0	3746.5	541.7	3203.3	2949.8	2849.8	19.0%	8.6%	12.2%	-3.6%
645	13-Sep-12	0	4156.3	653.2	3503.1	3215.2	3814.7	17.1%	9.0%	12.6%	-3.6%
678	17-Sep-12	0	3326.8	421.5	2905.3	2576.0	2949.7	14.3%	12.8%	12.6%	0.2%
735	26-Sep-12	0	4188.4	143.2	4023.6	3586.9	3586.9	4.0%	12.2%	8.3%	3.9%
751	27-Sep-12	0	4186.9	222.7	3963.2	3571.2	3571.2	6.2%	11.0%	12.6%	-1.6%
767	1-Oct-12	0	5869.4	104.5	5762.7	5118.4	5118.4	2.0%	12.6%	13.6%	-1.0%
848	16-Oct-12	0	3724.8	353.6	3370.3	3144.6	3144.6	11.2%	7.2%	9.2%	-2.0%
867	17-Oct-12	0	3702.1	128.2	3572.6	3910.6	3309.2	3.9%	8.0%	9.8%	-1.8%
874	18-Oct-12	0	3683.3	275.5	3408.4	3099.2	3099.2	8.9%	9.9%	10.1%	-0.2%
							Minimum	0.0%	7.2%	8.3%	-3.6%
							Maximum	38.9%	13.3%	13.8%	3.9%
							Mean	10.5%	11.3%	12.1%	-1.2%
							Average	10.7%	11.0%	11.6%	-0.6%

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ZONE S (TILL) LABORATORY TESTING SUMMARY (AMEC LAB)

Sample ID	Atterberg Limits				Particle Size Distribution (%Retained)				Standard Proctor					MC (%)	Deviation from Optimum	Comments
	LL (%)	PL (%)	PI (%)	Class	Gravel (%)	Sand (%)	Silt (%)	Clay (%)	Uncorrected MAX D. D.	Ucorrected Opt. MC	Rock Correction	Corrected MAX D. D.	Corrected Opt. MC			
S12-01	21	13	8	CL	11	42	34	13	2070	10.0	5.0	2094	9.5	9.5	0.0	Borrow Pit
S12-02	23	14	9	CL	10	26	46	18	1967	12.0	10.0	2022	11.0	20.4	9.4	GLU Blend
S12-03	22	13	9	CL	14	33	42	10	2054	9.0	10.0	2104	8.0	10.7	2.7	Borrow Pit
S12-04	25	15	10	CL	15	25	46	14	1987	11.5	10.0	2041	10.5	14.8	4.3	GLU Blend
S12-05	25	14	11	CL	17	34	37	12	1980	11.5	10.0	2034	10.5	13.9	3.4	GLU Blend
S12-06	27	14	12	CL	0	33	47	21	1935	13.0	5.0	1963	12.5	12.2	-0.3	Corner 4
S12-07	25	13	12	CL	12	38	36	15	1986	11.5	10.0	2040	10.5	11.3	0.8	Borrow Pit
S12-08	25	14	11	CL	25	31	31	13	1942	13.5	25.0	2089	10.5	12.1	1.6	36+00
S12-09	24	15	9	CL	2	36	47	15	N/A	N/A	N/A	N/A	N/A	13.3	N/A	Corner 51.0m
S12-10	26	16	10	CL	7	29	52	12	N/A	N/A	N/A	N/A	N/A	15.6	N/A	Corner 5 0.3m
S12-11	24	14	10	CL	18	35	32	14	1995	10.5	10.0	2048	9.5	9.9	0.4	Borrow Pit
S12-12	25	15	10	CL	11	34	39	16	1915	12.5	10.0	1972	11.5	9.2	-2.3	Main Embankment
S12-13	25	15	10	CL	16	26	41	17	2003	11.0	10.0	2056	10.0	12.7	2.7	Borrow Pit
S12-14	24	13	11	CL	23	31	31	14	2010	11.5	10.0	2090	10.0	12.0	2.0	Borrow Pit
S12-15	27	16	11	CL	27	25	33	15	N/A	N/A	N/A	N/A	N/A	12.0	N/A	Perimeter Embankment
S12-16	26	15	11	CL	14	34	38	15	2056	9.5	15.0	2132	8.0	9.7	1.7	27+44
S12-17	20	16	4	CL	13	41	38	8	2065	9.5	15.0	2141	8.0	8.8	0.8	Borrow Pit
S12-18	27	15	12	CL	12	30	41	18	1947	12.5	10.0	2003	11.5	15.5	4.0	Perimeter Embankment
MEAN	25	15	10	CL	14	33	39	14	1987	11.5	10.0	2048	10.5	12.1	1.7	
AVERAGE	25	14	10	CL	14	32	39	14	1994	11.3	11.0	2055	10.1	12.4	2.1	
MAXIMUM	27	16	12	CL	27	42	52	21	2070	13.5	25.0	2141	12.5	20.4	9.4	
MINIMUM	20	13	4	CL	0	25	31	8	1915	9.0	5.0	1963	8.0	8.8	-2.3	

GRAIN SIZE DISTRIBUTION

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Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 29-May-12

PROJECT NAME: Mt. Polley

TEST No:

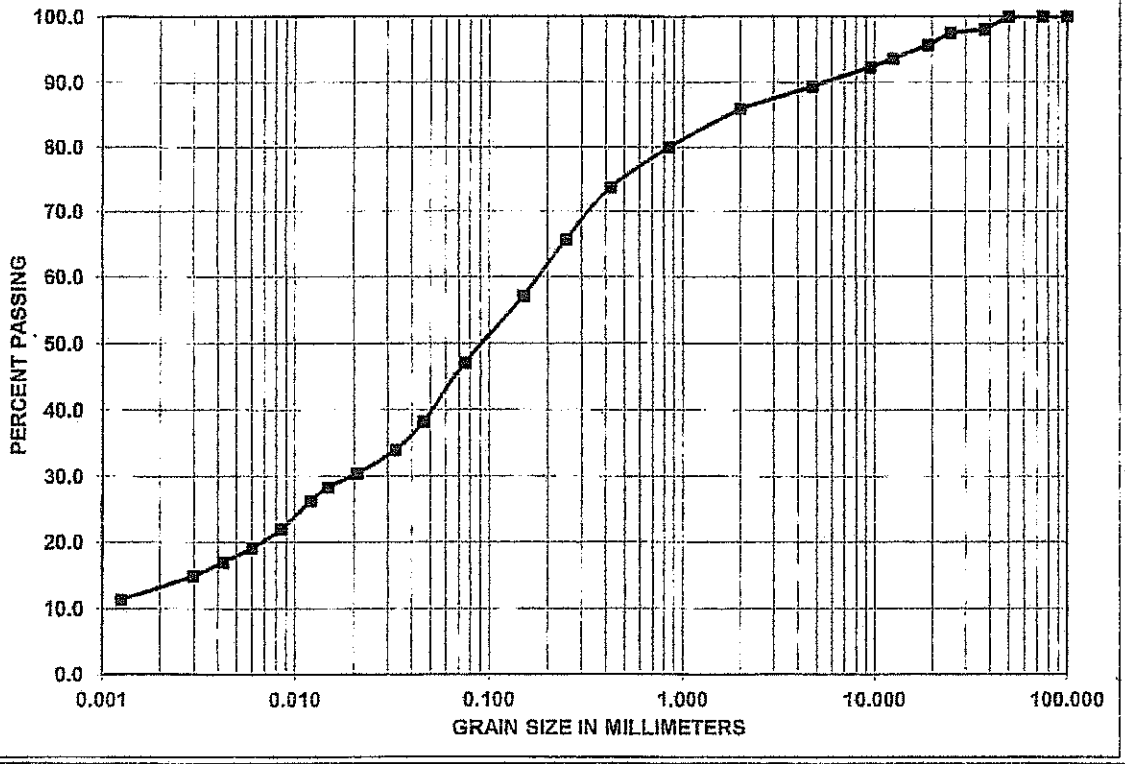
SAMPLED BY: L. Wiebe

DATE SAMPLED: 15-May-12

SOURCE: East/West Borrow

DATE TESTED: 28-May-12

DEPTH:



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	98.0
25.0	97.5
19.0	95.7
12.5	93.6
9.5	92.3
4.75	89.4
2.00	86.0
0.850	79.9
0.425	73.7
0.250	65.7
0.150	57.1
0.075	47.1
0.0459	38.2
0.0329	34.0
0.0208	30.4
0.0147	28.3
0.0120	26.2
0.0085	21.9
0.0060	19.1
0.0043	17.0
0.0030	14.9
0.0013	11.3

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	10.61%
SAND	42.34%
SILT	34.17%
CLAY	12.89%

TECHNICIAN: LM Richard

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	East/West Borrows
Project Number:	VM00560A.B.3	Date Sampled:	15-May-12
Technician:	G. Michaud	Depth:	
Date:	25-May-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	14	37	25	
Tare ID	AB	Q	N	
Mass Wet + Tare	38.28	38.01	36.39	
Mass Dry + Tare	35.17	35.27	33.78	
Mass Tare	21.46	21.57	21.32	
Mass of Water	3.11	2.74	2.61	
Dry Soil Mass	13.71	13.70	12.46	
Moisture Content	22.7	20.0	20.9	
Liquid Limit	21.1	21.1	21.0	

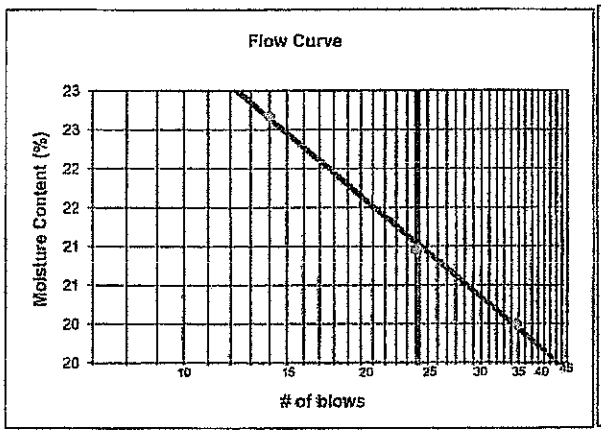
Average Liquid Limit: 21

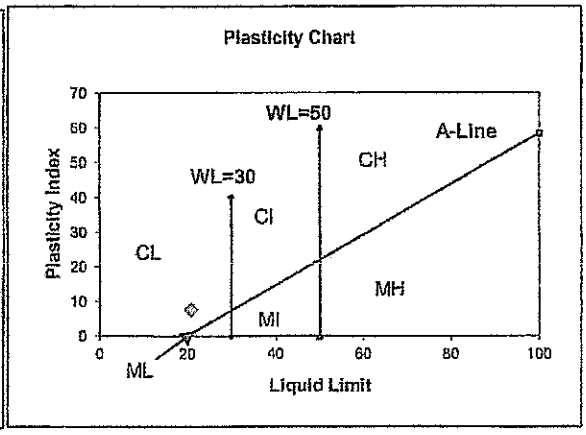
Plastic Limit

Trial No.	1	2	3	
Tare ID	46	42	2	
Mass Wet + Tare	33.33	31.17	32.65	
Mass Dry + Tare	31.94	30.04	31.35	
Mass Tare	21.37	21.42	21.58	
Mass of Water	1.39	1.13	1.30	
Dry Soil Mass	10.57	8.62	9.77	
Moisture Content	13.2	13.1	13.3	

Average Plastic Limit	13
Plasticity Index	8
Received Moisture	9.5

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

amec

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

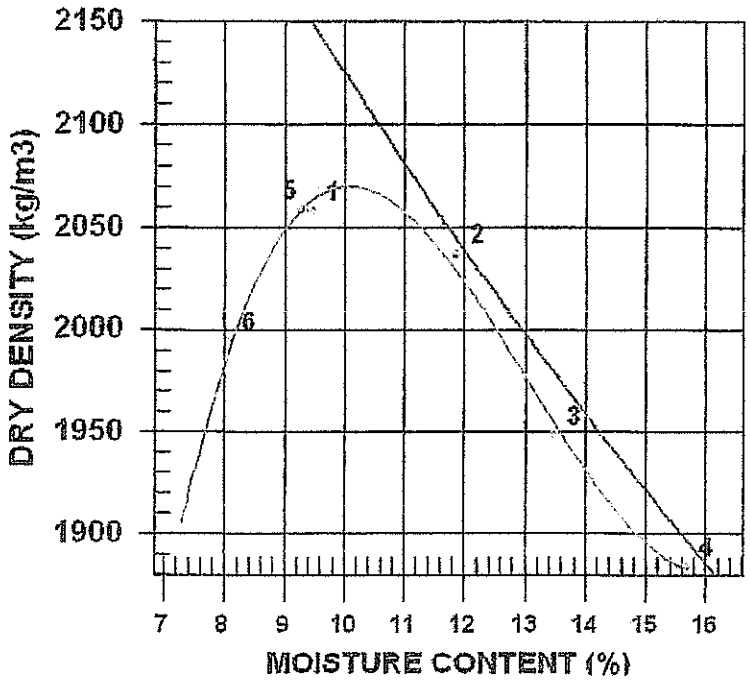
TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

PROJECT Mount Polley

CONTRACTOR

PROCTOR NO. 6 DATE TESTED 2012.May.24 DATE RECEIVED 2012.May.22 DATE SAMPLED 2012.May

INSITU MOISTURE	9.5 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
SAMPLED BY	L. Wiebe	COMPACTION PROCEDURE	C: 152.4mm Mold, Passing 19mm
TESTED BY	M. Tennant	RAMMER TYPE	Automatic
SUPPLIER	Mt. Polley	PREPARATION	Dry
SOURCE	East/West Borrows	OVERSIZE CORRECTION METHOD	ASTM 4718
MATERIAL IDENTIFICATION		RETAINED 19mm SCREEN	5.0 %
MAJOR COMPONENT	Till	OVERSIZE SPECIFIC GRAVITY	2.70
SIZE	-50mm	TOTAL NUMBER OF TRIALS	6
DESCRIPTION			
ROCK TYPE			



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2253	2058	9.5
2	2279	2037	11.9
3	2211	1948	13.5
4	2180	1884	15.7
5	2251	2059	9.3
6	2156	1994	8.1

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	2070	10.0
OVERSIZE CORRECTED	2094	9.5

COMMENTS

 2012.May.29 AMEC Environment & Infrastructure PER. G Michaud

GRAIN SIZE DISTRIBUTION

amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 12-Jun-12

PROJECT NAME: Mt. Polley

TEST No:

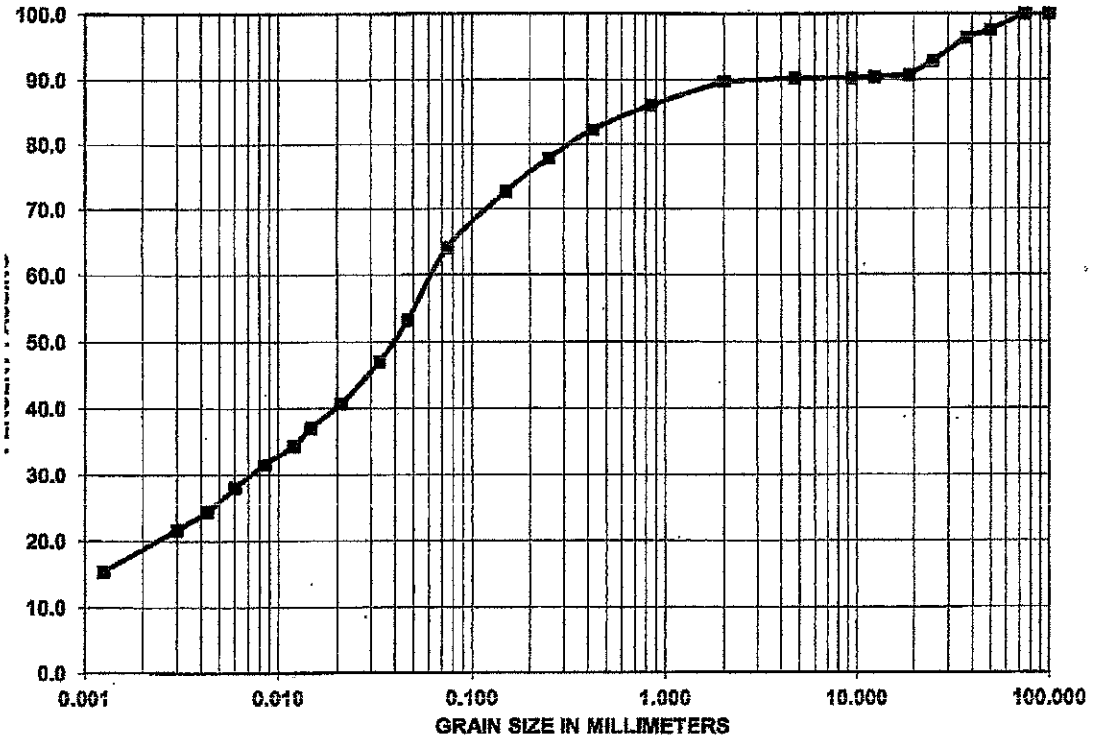
SAMPLED BY: L. Wiebe

DATE SAMPLED: 31-May-12

SOURCE: West Borrow

DATE TESTED: 11-Jun-12

DEPTH: N: 5819784m
E: 595592m



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	97.5
37.5	96.4
25.0	92.8
19.0	90.7
12.5	90.5
9.5	90.2
4.75	90.2
2.00	89.7
0.850	86.0
0.425	82.2
0.250	77.8
0.150	72.6
0.075	64.1
0.0467	53.3
0.0330	47.0
0.0209	40.7
0.0148	37.0
0.0121	34.3
0.0085	31.6
0.0060	28.0
0.0043	24.4
0.0030	21.7
0.0013	15.4

EMARKS:

D_{10} =	N/A	GRAVEL	9.80%
D_{30} =	N/A	SAND	26.11%
D_{60} =	N/A	SILT	46.04%
Cu =	N/A	CLAY	18.04%
Cc =	N/A		

CHNICIAN: YMichaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	West Borrow
Project Number:	VM00560A.B.3	Date Sampled:	31-May-12
Technician:	M. Tennant	Depth:	N: 5819784m
Date:	11-Jun-12	Comments:	E: 595592m

Liquid Limit

Trial No.	1	2	3	
No. of Blows	13	26	39	
Tare ID	AE	V	AL	
Mass Wet + Tare	49.59	34.40	35.62	
Mass Dry + Tare	44.06	32.00	33.09	
Mass Tare	22.14	21.66	21.73	
Mass of Water	5.53	2.40	2.53	
Dry Soil Mass	21.92	10.34	11.36	
Moisture Content	25.2	23.2	22.3	
Liquid Limit	23.3	23.3	23.7	

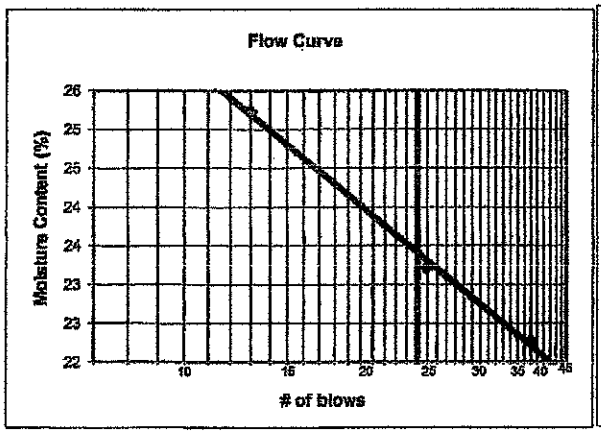
Average Liquid Limit: 23

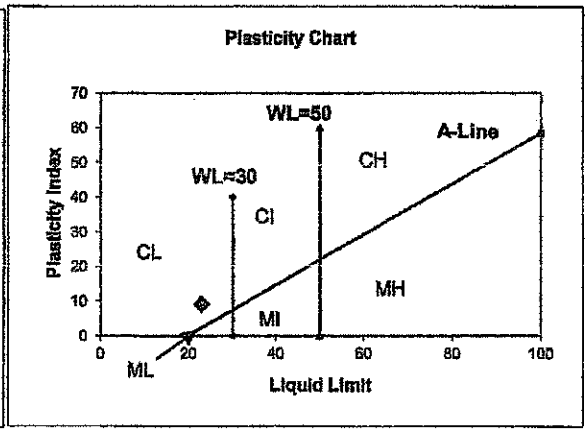
Plastic Limit

Trial No.	1	2	3	
Tare ID	14	47	37	
Mass Wet + Tare	28.12	29.94	31.59	
Mass Dry + Tare	27.30	28.90	30.36	
Mass Tare	21.40	21.46	21.51	
Mass of Water	0.82	1.04	1.23	
Dry Soil Mass	5.90	7.44	8.85	
Moisture Content	13.9	14.0	13.9	

Average Plastic Limit	14
Plasticity Index	9
Received Moisture	20.4

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





:C Environment & Infrastructure
A division of AMEC Americas Limited
Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

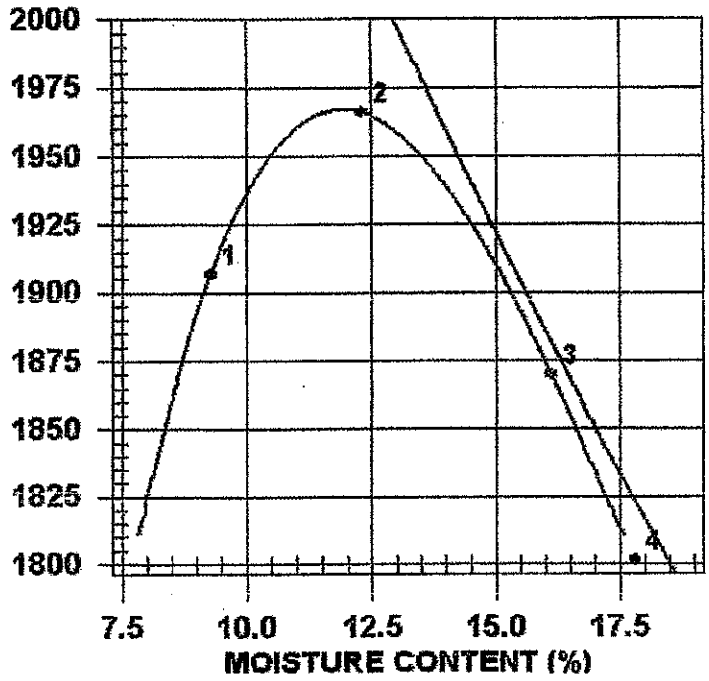
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

IECT Mount Polley

TRACTOR

TOR NO. 7 DATE TESTED 2012.Jun.11 DATE RECEIVED 2012.Jun.07 DATE SAMPLED 2012.May.31

U MOISTURE	20.4 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
LED BY	L. Wiebe		
ED BY	M. Tennant	COMPACTION PROCEDURE	C: 152.4mm Mold, Passing 19mm
LIER	West Borrow		
RCE	N:5819784m, E:595592m	RAMMER TYPE	Automatic
RIAL IDENTIFICATION		PREPARATION	Moist
OR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
E	-25mm	RETAINED 19mm SCREEN	10.0 %
CRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
K TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2084	1907	9.3
2	2208	1966	12.3
3	2171	1870	16.1
4	2121	1801	17.8

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1967	12.0
OVERSIZE CORRECTED	2022	11.0

MENTS

 2012.Jun.22 AMEC Environment & Infrastructure PER M Michaud

GRAIN SIZE DISTRIBUTION

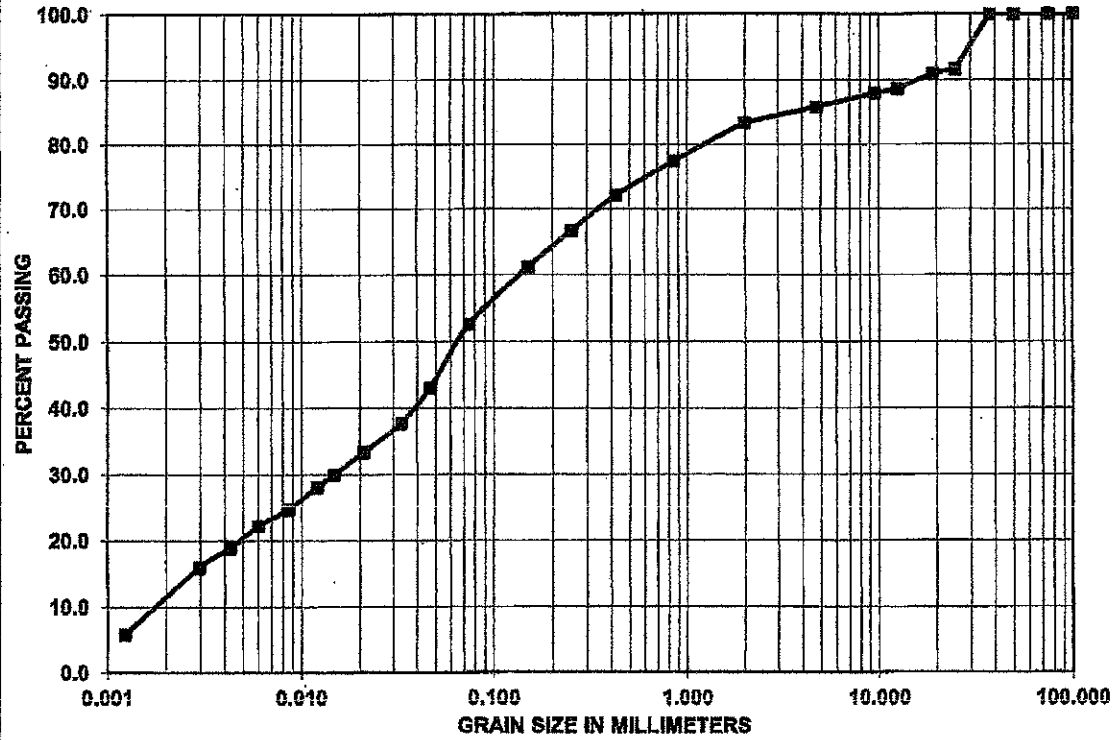
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 22-Jun-12

PROJECT NAME: Mt. Polley

TEST No:
SAMPLED BY: MPMC staff
DATE SAMPLED: 13-Jun-12
SOURCE: STA 37+00, ZSI-A
DATE TESTED: 20-Jun-12
DEPTH: elv. 960.45m



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	100.0
25.0	91.6
19.0	91.0
12.5	88.5
9.5	87.9
4.75	85.7
2.00	83.4
0.850	77.4
0.425	72.1
0.250	66.6
0.150	61.2
0.075	52.6
0.0467	43.0
0.0330	37.7
0.0209	33.3
0.0148	30.0
0.0121	28.0
0.0085	24.6
0.0060	22.2
0.0043	18.8
0.0030	15.9
0.0012	5.8

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	14.26%
SAND	33.13%
SILT	42.29%
CLAY	10.32%

TECHNICIAN: J Michaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	STA 37+00/ZSI-A
Project Number:	VM00560A.B.3	Date Sampled:	13-Jun-12
Technician:	M. Tennant	Depth:	elv. 960.45m
Date:	20-Jun-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	15	39	23	
Tare ID	AL	AM	AQ	
Mass Wet + Tare	43.22	40.48	44.04	
Mass Dry + Tare	39.18	37.34	39.96	
Mass Tare	21.77	21.56	21.48	
Mass of Water	4.04	3.14	4.08	
Dry Soil Mass	17.41	15.78	18.48	
Moisture Content	23.2	19.9	22.1	
Liquid Limit	21.8	21.1	21.8	

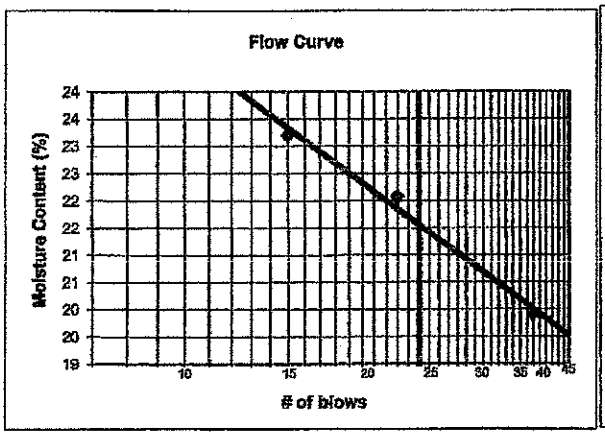
Average Liquid Limit: 22

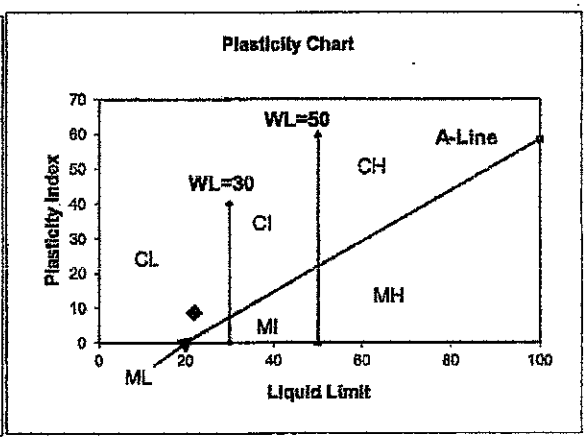
Plastic Limit

Trial No.	1	2	3	
Tare ID	42	43	48	
Mass Wet + Tare	30.55	31.91	30.88	
Mass Dry + Tare	29.47	30.68	29.78	
Mass Tare	21.43	21.44	21.43	
Mass of Water	1.08	1.23	1.10	
Dry Soil Mass	8.04	9.24	8.35	
Moisture Content	13.4	13.3	13.2	

Average Plastic Limit	13
Plasticity Index	9
Received Moisture	10.7

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

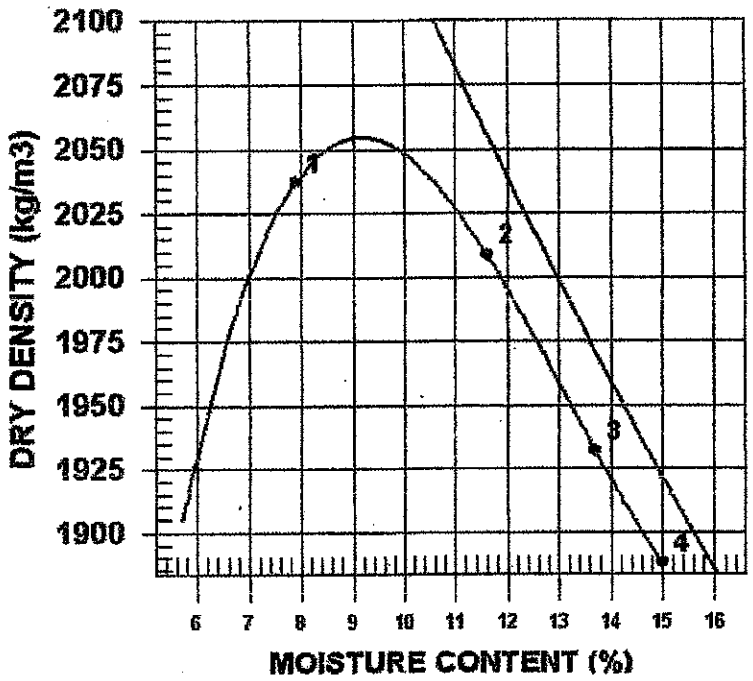
PROJECT Mount Polley

CONTRACTOR

PROCTOR NO. 8 DATE TESTED 2012.Jun.19 DATE RECEIVED 2012.Jun.15 DATE SAMPLED 2012.Jun.

INSITU MOISTURE	10.7 %
SAMPLED BY	MPMC staff
TESTED BY	M. Tennnant
SUPPLIER	elv. 960.45m
SOURCE	STA 37+00 ZS1-A
MATERIAL IDENTIFICATION	
MAJOR COMPONENT	Till
SIZE	-50mm
DESCRIPTION	
ROCK TYPE	

COMPACTION STANDARD	Standard Proctor, ASTM D698
COMPACTION PROCEDURE	C: 152.4mm Mold, Passing 19mm
RAMMER TYPE	Automatic
PREPARATION	Moist
OVERSIZE CORRECTION METHOD	ASTM 4718
RETAINED 19mm SCREEN	10.0 %
OVERSIZE SPECIFIC GRAVITY	2.70
TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2198	2037	7.9
2	2242	2009	11.6
3	2197	1932	13.7
4	2171	1888	15.0

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	2054	9.0
OVERSIZE CORRECTED	2104	8.0

COMMENTS

 2012.Jun.22 AMEC Environment & Infrastructure PER. GMichaud

GRAIN SIZE DISTRIBUTION

amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 06-Jul-12

PROJECT NAME: Mt. Polley

TEST No:

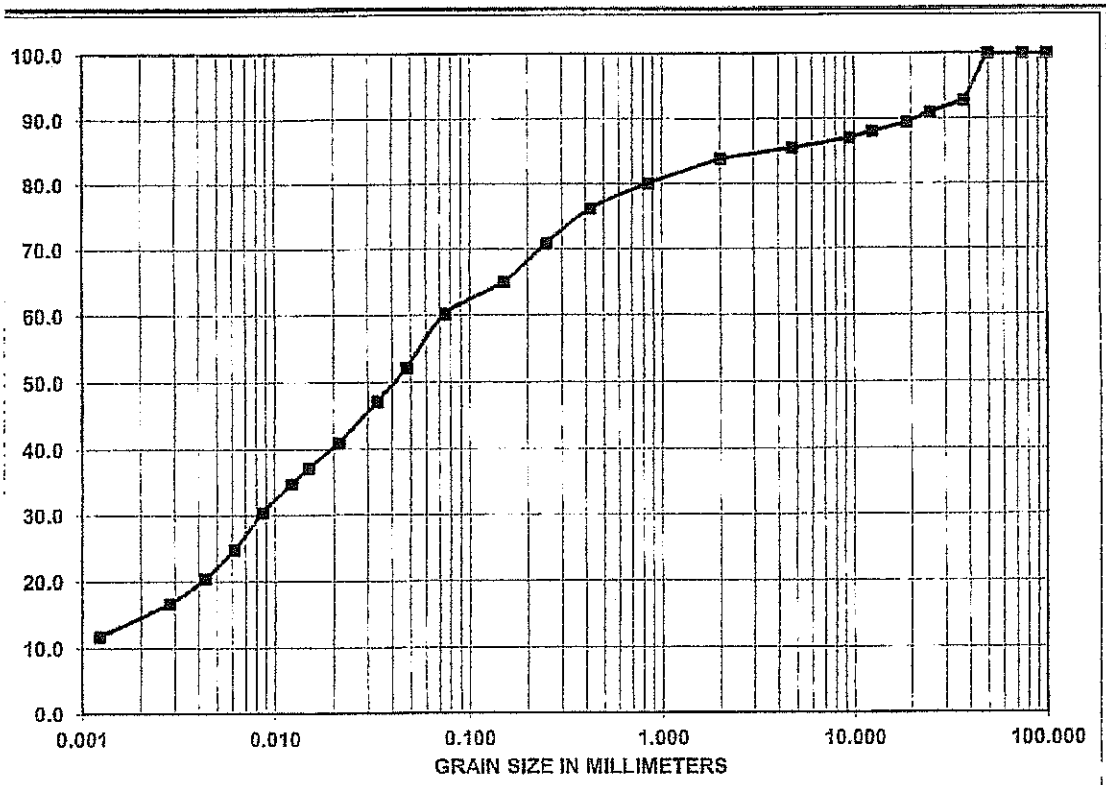
SAMPLED BY: MPMC staff

DATE SAMPLED: 22-Jun-12

SOURCE: S12-04

DATE TESTED: 5-Jul-12

DEPTH:



SUMMARY	
Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	92.8
25.0	91.0
19.0	89.4
12.5	88.0
9.5	87.0
4.75	85.5
2.00	83.8
0.850	80.0
0.425	76.1
0.250	70.8
0.150	65.0
0.075	60.2
0.0476	52.1
0.0337	47.2
0.0213	41.0
0.0151	37.2
0.0123	34.8
0.0087	30.4
0.0061	24.8
0.0043	20.5
0.0028	16.8
0.0012	11.8

EMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
Cu =	N/A
Cc =	N/A

GRAVEL	14.53%
SAND	25.30%
SILT	45.99%
CLAY	14.19%

ECHNICIAN: JM Michaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-04
Project Number:	VM00560A.B.3	Date Sampled:	22-Jun-12
Technician:	M. Tennant	Depth:	
Date:	5-Jul-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	24	29	39	
Tare ID	H	S	O	
Mass Wet + Tare	47.15	47.71	46.73	
Mass Dry + Tare	42.06	42.60	42.07	
Mass Tare	21.69	21.55	22.06	
Mass of Water	5.09	5.11	4.66	
Dry Soil Mass	20.37	21.05	20.01	
Moisture Content	25.0	24.3	23.3	
Liquid Limit	24.9	24.8	24.7	

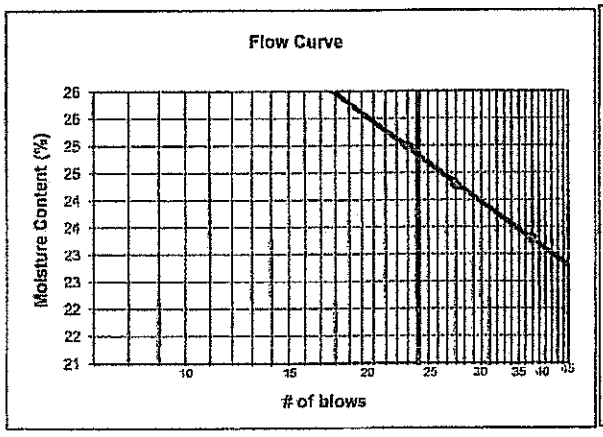
Average Liquid Limit: 25

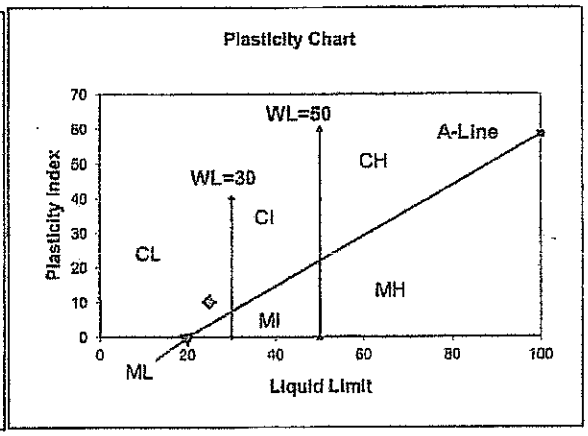
Plastic Limit

Trial No.	1	2	3	
Tare ID	30	42	24	
Mass Wet + Tare	31.99	31.50	31.54	
Mass Dry + Tare	30.60	30.20	30.25	
Mass Tare	21.36	21.42	21.55	
Mass of Water	1.39	1.30	1.29	
Dry Soil Mass	9.24	8.78	8.70	
Moisture Content	15.0	14.8	14.8	

Average Plastic Limit	15
Plasticity Index	10
Received Moisture	14.8

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





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A division of AMEC Americas Limited
Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

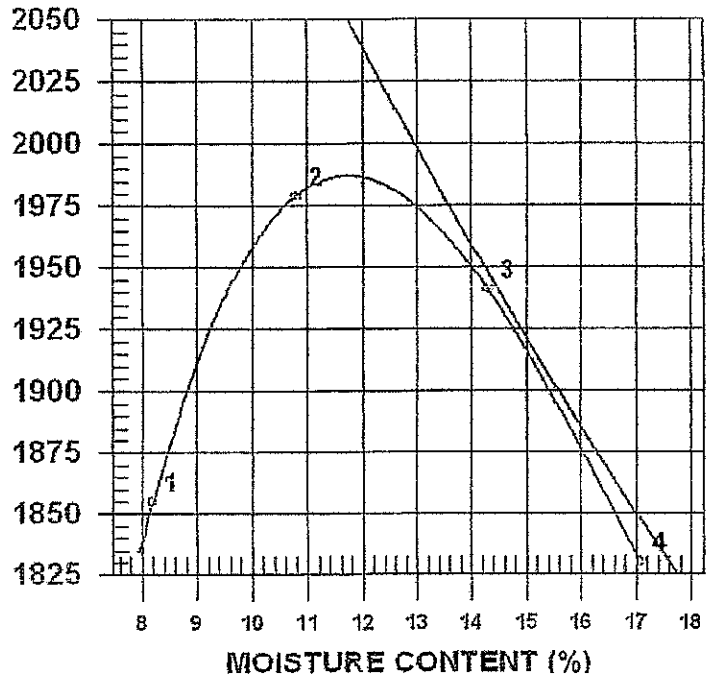
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

JECT Mount Polley

TRACTOR

CTOR NO. 9 DATE TESTED 2012.Jul.02 DATE RECEIVED 2012.Jun.28 DATE SAMPLED 2012.Jun.22

U MOISTURE	14.8 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
PLED BY	MPMC staff		
ED BY	M. Tennant	COMPACTION PROCEDURE	C: 152.4mm Mold, Passing 19mm
PLIER			
RCE	S12-04	RAMMER TYPE	Automatic
ERIAL IDENTIFICATION		PREPARATION	Dry
JOR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
E	-50mm	RETAINED 19mm SCREEN	10.0 %
SCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
CK TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2007	1855	8.2
2	2193	1979	10.8
3	2219	1941	14.3
4	2143	1830	17.1

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1987	11.5
OVERSIZE CORRECTED	2041	10.5

MENTS

 2012.Jul.06 AMEC Environment & Infrastructure PER. YM Richard

GRAIN SIZE DISTRIBUTION

amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 06-Jul-12

PROJECT NAME: Mt. Polley

TEST No:

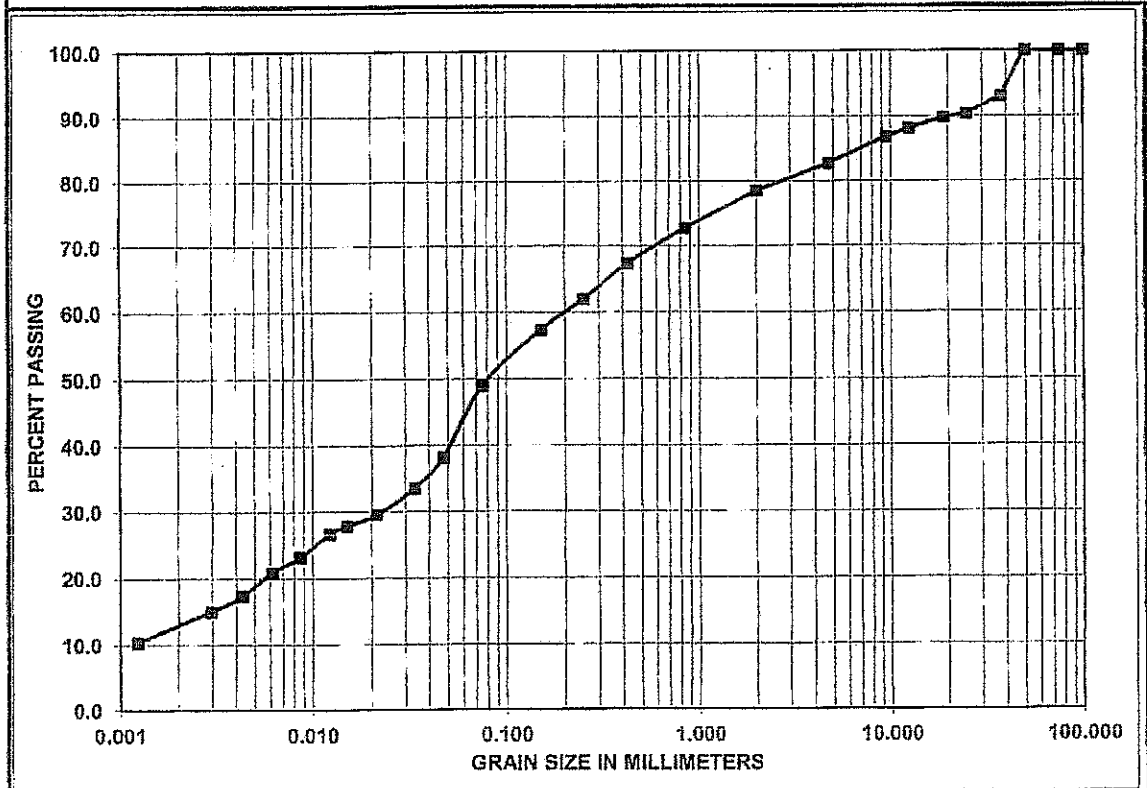
SAMPLED BY: MPMC staff

DATE SAMPLED: 27-Jun-12

SOURCE: S12-05

DATE TESTED: 5-Jul-12

DEPTH:



SUMMARY	
Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	93.0
25.0	90.4
19.0	89.8
12.5	88.1
9.5	86.8
4.75	82.7
2.00	78.5
0.850	72.7
0.425	67.3
0.250	61.9
0.150	57.3
0.075	49.0
0.0476	38.2
0.0337	33.6
0.0213	29.5
0.0151	27.8
0.0123	26.6
0.0087	23.2
0.0061	20.8
0.0043	17.4
0.0030	15.1
0.0012	10.4

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	17.30%
SAND	33.74%
SILT	36.48%
CLAY	12.49%

TECHNICIAN: J Michaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-05
Project Number:	VM00560A.B.3	Date Sampled:	27-Jun-12
Technician:	M. Tennant	Depth:	
Date:	5-Jul-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	18	30	38	
Tare ID	V	K	R	
Mass Wet + Tare	44.28	44.66	43.45	
Mass Dry + Tare	39.67	40.19	39.37	
Mass Tare	21.69	21.55	21.57	
Mass of Water	4.61	4.47	4.08	
Dry Soil Mass	17.98	18.64	17.80	
Moisture Content	25.6	24.0	22.9	
Liquid Limit	24.6	24.6	24.3	

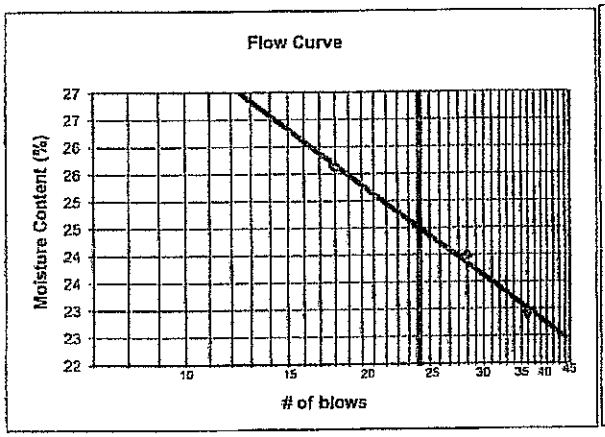
Average Liquid Limit: 25

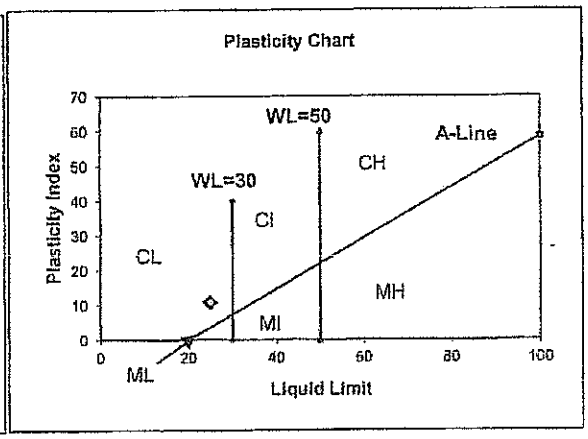
Plastic Limit

Trial No.	1	2	3	
Tare ID	7	29	13	
Mass Wet + Tare	32.96	31.36	32.00	
Mass Dry + Tare	31.54	30.16	30.68	
Mass Tare	21.45	21.53	21.42	
Mass of Water	1.42	1.20	1.32	
Dry Soil Mass	10.09	8.63	9.26	
Moisture Content	14.1	13.9	14.3	

Average Plastic Limit	14
Plasticity Index	11
Received Moisture	13.9

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

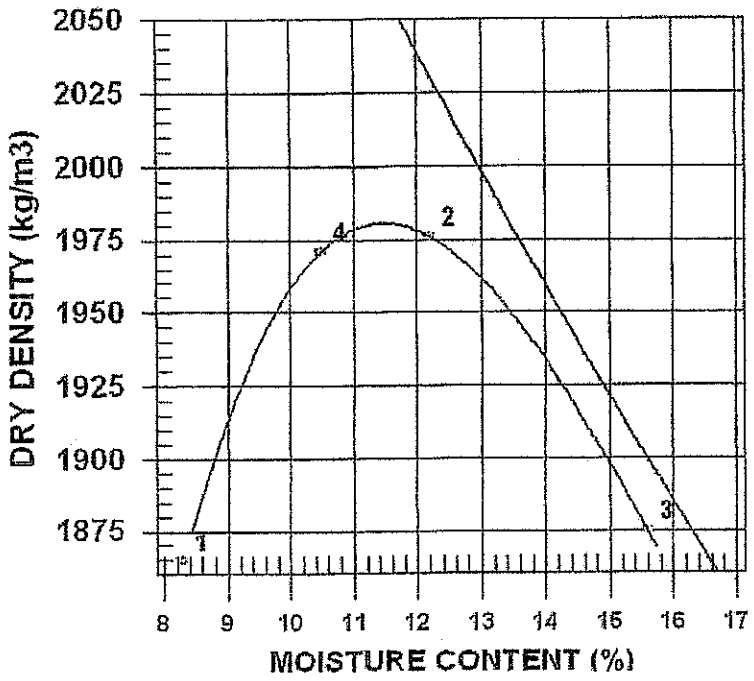
TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

PROJECT Mount Polley

CONTRACTOR

PROCTOR NO. 10 DATE TESTED 2012.Jul.02 DATE RECEIVED 2012.Jun.28 DATE SAMPLED 2012.Jun.

INSITU MOISTURE	13.9 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
SAMPLED BY	MPMC staff		
TESTED BY	M. Tennant	COMPACTION PROCEDURE	C: 152.4mm Mold, Passing 19mm
SUPPLIER			
SOURCE	S12-05	RAMMER TYPE	Automatic
MATERIAL IDENTIFICATION		PREPARATION	Dry
MAJOR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
SIZE	-50mm	RETAINED 19mm SCREEN	10.0 %
DESCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
ROCK TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2020	1865	8.3
2	2217	1976	12.2
3	2168	1875	15.6
4	2178	1971	10.5

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1980	11.5
OVERSIZE CORRECTED	2034	10.5

COMMENTS

 2012.Jul.06 AMEC Environment & Infrastructure PER. MW Richard

GRAIN SIZE DISTRIBUTION

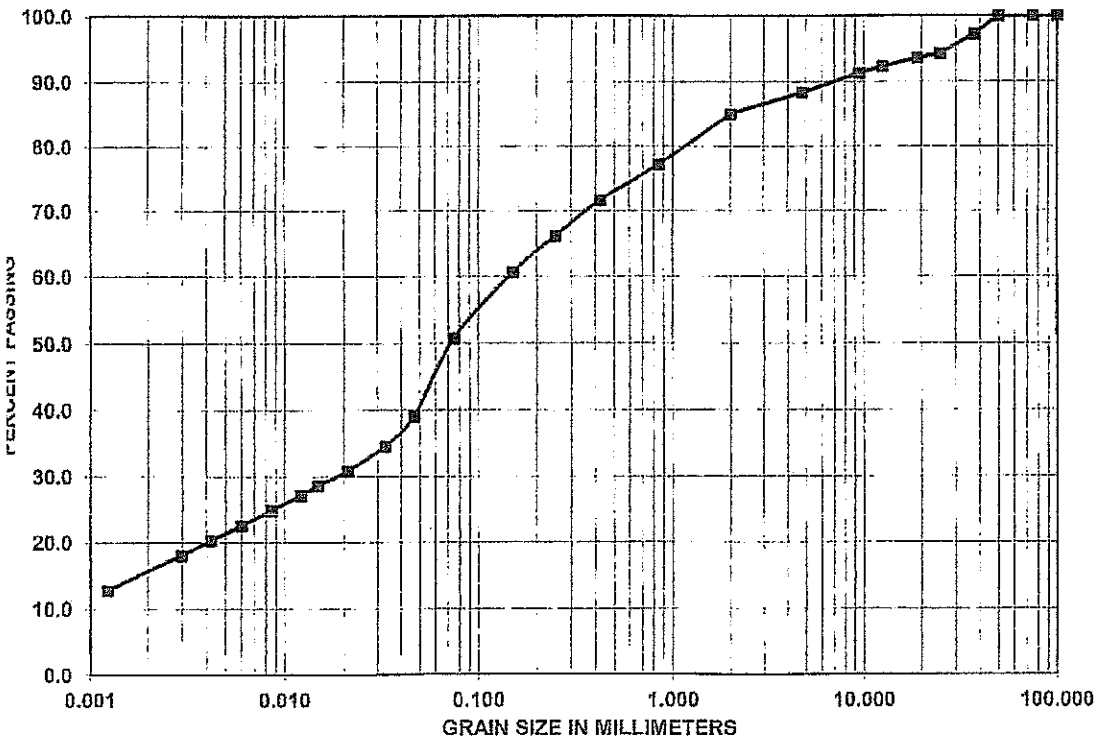
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 25-Jul-12

PROJECT NAME: Mt. Polley

TEST No: S12-07
SAMPLED BY: MPMC
DATE SAMPLED: 8-Jul-12
SOURCE: Borrow Pit
DATE TESTED: 23-Jul-12
DEPTH:



SUMMARY	
Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	97.2
25.0	94.2
19.0	93.6
12.5	92.3
9.5	91.3
4.75	88.3
2.00	84.9
0.850	77.2
0.425	71.6
0.250	66.1
0.150	60.6
0.075	50.8
0.0467	39.1
0.0330	34.6
0.0209	30.8
0.0148	28.6
0.0121	27.1
0.0085	24.8
0.0060	22.5
0.0042	20.3
0.0030	18.0
0.0012	12.8

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	11.70%
SAND	37.54%
SILT	35.64%
CLAY	15.12%

TECHNICIAN:

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	Borrow Pit, Sample 2
Project Number:	VM00560A.B.3	Date Sampled:	8-Jul-12
Technician:	M. Tennant	Depth:	S12-07
Date:	23-Jul-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	23	32	26	
Tare ID	H	A	S	
Mass Wet + Tare	47.05	42.64	44.47	
Mass Dry + Tare	41.93	38.61	39.92	
Mass Tare	21.47	21.72	21.53	
Mass of Water	5.12	4.03	4.55	
Dry Soil Mass	20.46	16.89	18.39	
Moisture Content	25.0	23.9	24.7	
Liquid Limit	24.8	24.7	24.9	

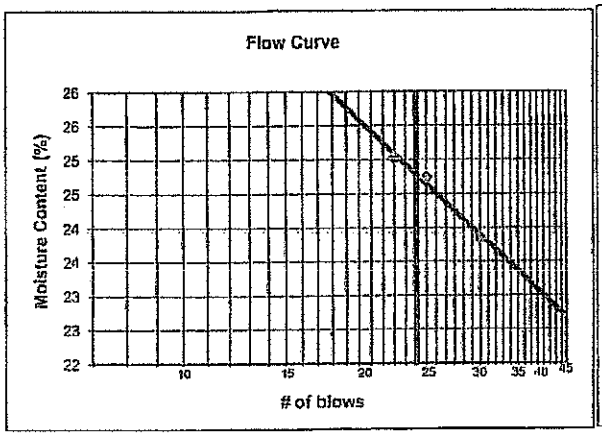
Average Liquid Limit: 25

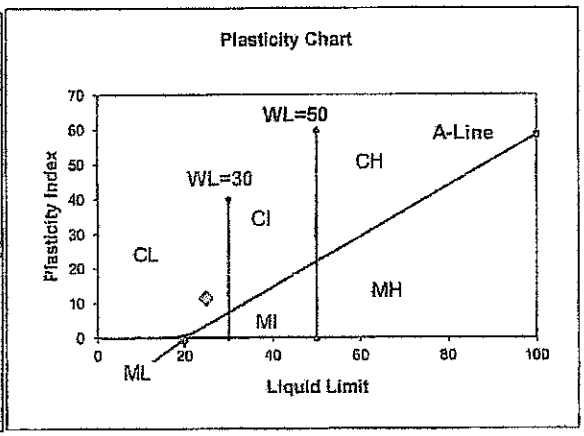
Plastic Limit

Trial No.	1	2	3	
Tare ID	25	27	41	
Mass Wet + Tare	31.14	33.73	32.37	
Mass Dry + Tare	30.00	32.29	31.07	
Mass Tare	21.44	21.44	21.45	
Mass of Water	1.14	1.44	1.30	
Dry Soil Mass	8.56	10.85	9.62	
Moisture Content	13.3	13.3	13.5	

Average Plastic Limit	13
Plasticity Index	12
Received Moisture	11.3

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





EC Environment & Infrastructure
A division of AMEC Americas Limited
36 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

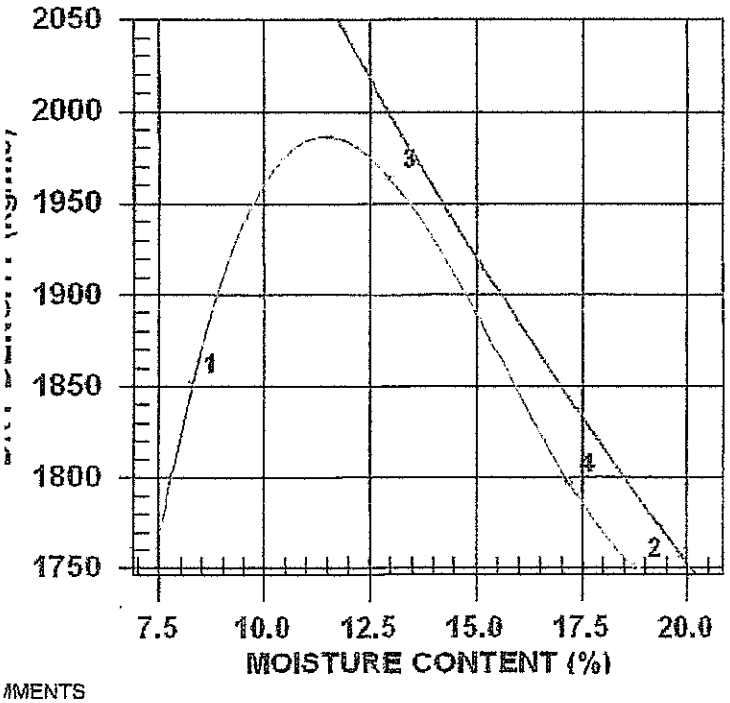
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

OJECT Mount Polley

NTRACTOR

OCTOR NO. 12 DATE TESTED 2012.Jul.18 DATE RECEIVED 2012.Jul.14 DATE SAMPLED 2012.Jul.08

ITU MOISTURE	11.3 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
MPLED BY	MPMC		
TED BY	D. deSousa	COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
PLIER	Borrow Pit		
URCE	S12-07	RAMMER TYPE	Automatic
TERIAL IDENTIFICATION		PREPARATION	Moist
AJOR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
ZE	-37.5mm	RETAINED 4.75mm SCREEN	10.0 %
ESCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
OCK TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2006	1852	8.3
2	2080	1751	18.8
3	2219	1964	13.0
4	2106	1797	17.2

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1986	11.5
OVERSIZE CORRECTED	2040	10.5

MMENTS

 2012.Aug.02 AMEC Environment & Infrastructure PER. _____

GRAIN SIZE DISTRIBUTION

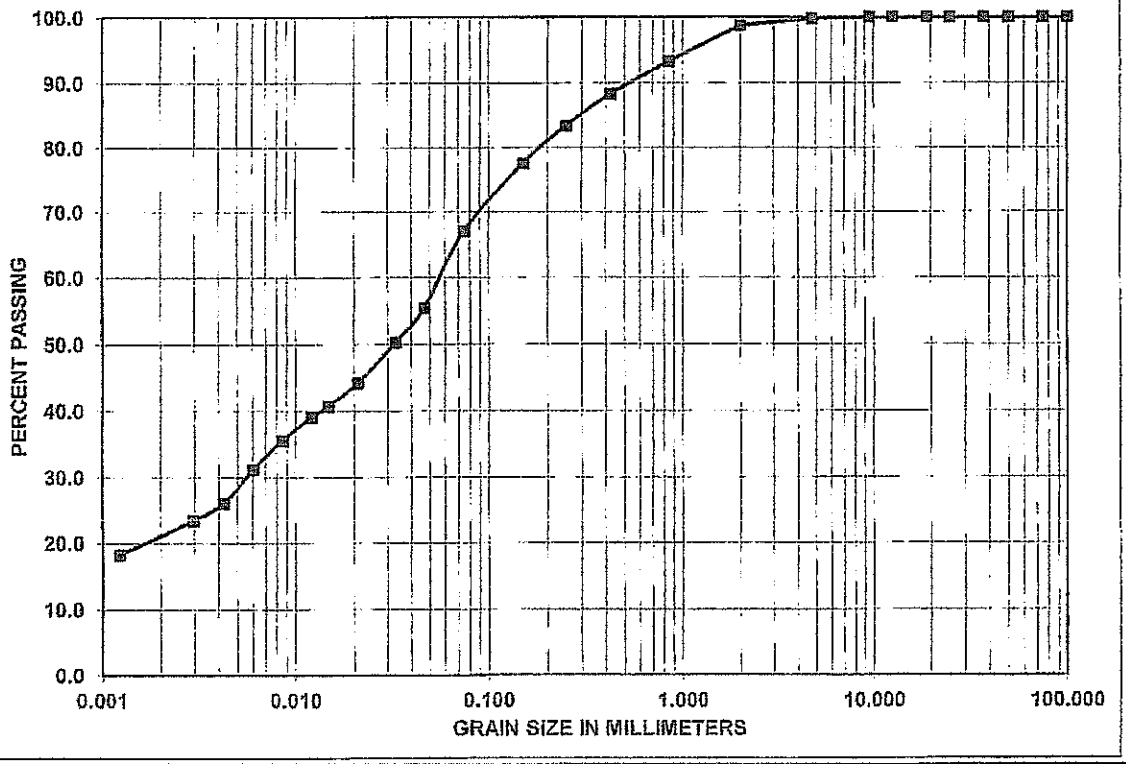
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 25-Jul-12

PROJECT NAME: Mt. Polley

TEST No: S12-06
SAMPLED BY: MPMC
DATE SAMPLED: 10-Jul-12
SOURCE: Corner 4, South Pit
DATE TESTED: 23-Jul-12
DEPTH:



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	100.0
25.0	100.0
19.0	100.0
12.5	100.0
9.5	100.0
4.75	99.8
2.00	98.7
0.850	93.3
0.425	88.3
0.250	83.4
0.150	77.5
0.075	67.0
0.0467	55.5
0.0330	50.3
0.0209	44.2
0.0148	40.7
0.0121	39.0
0.0085	35.5
0.0060	31.2
0.0043	26.0
0.0030	23.4
0.0012	18.2

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	0.15%
SAND	32.83%
SILT	46.50%
CLAY	20.52%

TECHNICIAN: JMarcaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	Corner 4, South Pit
Project Number:	VM00560A.B.3	Date Sampled:	10-Jul-12
Technician:	M. Tennant	Depth:	S12-06
Date:	23-Jul-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	33	16	24	
Tare ID	AS	Z	G	
Mass Wet + Tare	45.29	44.59	45.16	
Mass Dry + Tare	40.40	39.46	40.12	
Mass Tare	21.56	21.54	21.41	
Mass of Water	4.89	5.13	5.04	
Dry Soil Mass	18.84	17.92	18.71	
Moisture Content	26.0	28.6	26.9	
Liquid Limit	26.9	27.1	26.8	

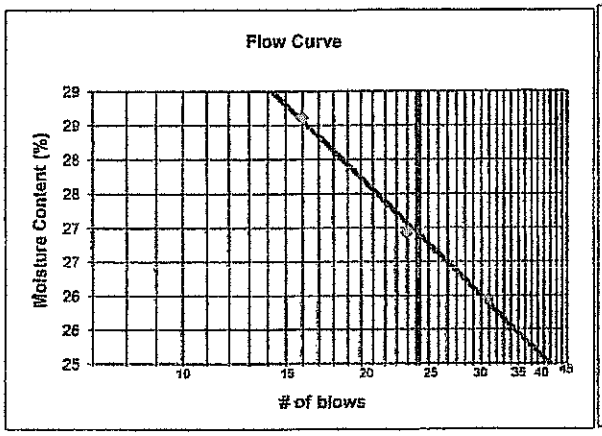
Average Liquid Limit: 27

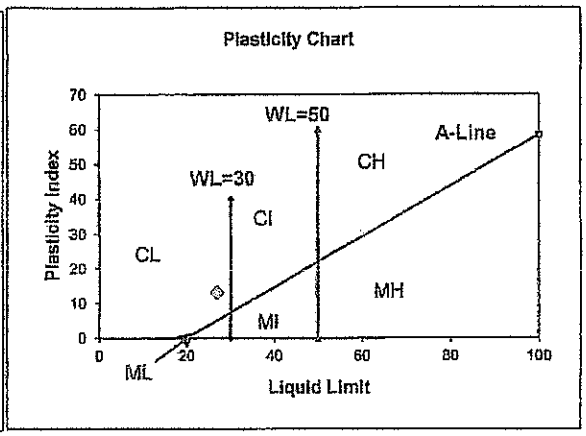
Plastic Limit

Trial No.	1	2	3	
Tare ID	29	32	42	
Mass Wet + Tare	34.24	28.46	32.93	
Mass Dry + Tare	32.70	27.63	31.55	
Mass Tare	21.51	21.53	21.43	
Mass of Water	1.54	0.83	1.38	
Dry Soil Mass	11.19	6.10	10.12	
Moisture Content	13.8	13.6	13.6	

Average Plastic Limit	14
Plasticity Index	13
Received Moisture	12.2

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

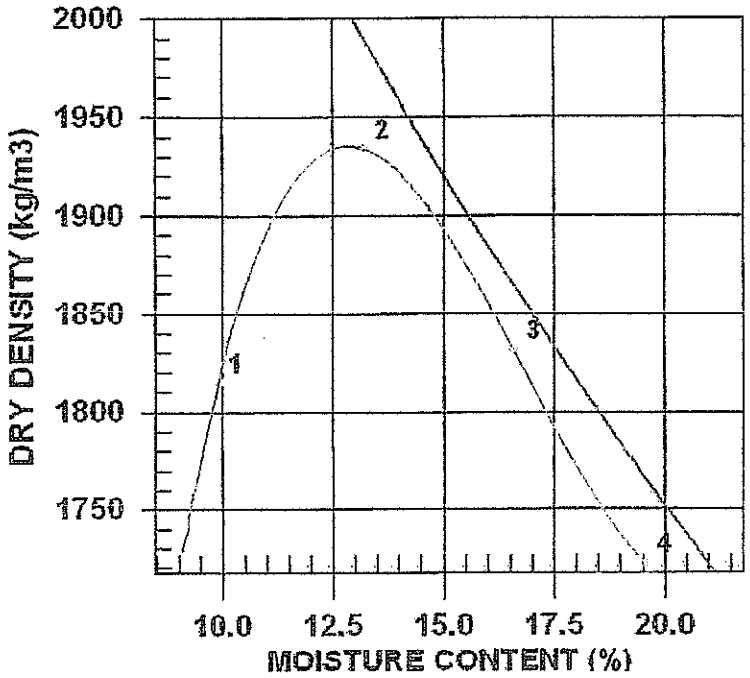
TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

PROJECT Mount Polley

CONTRACTOR

PROCTOR NO. 11 DATE TESTED 2012.Jul.14 DATE RECEIVED 2012.Jul.14 DATE SAMPLED 2012.Jul.

INSITU MOISTURE	12.2 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
SAMPLED BY	MPMC		
TESTED BY	M.Tennant	COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
SUPPLIER	Corner 4, South Pit		
SOURCE	S12-06	RAMMER TYPE	Automatic
MATERIAL IDENTIFICATION		PREPARATION	Moist
MAJOR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
SIZE	-4.75mm	RETAINED 4.75mm SCREEN	5.0 %
DESCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
ROCK TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	1995	1815	9.9
2	2189	1934	13.2
3	2135	1831	16.6
4	2060	1722	19.6

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1935	13.0
OVERSIZE CORRECTED	1963	12.5

COMMENTS

 2012.Jul.28 AMEC Environment & Infrastructure PER

GRAIN SIZE DISTRIBUTION

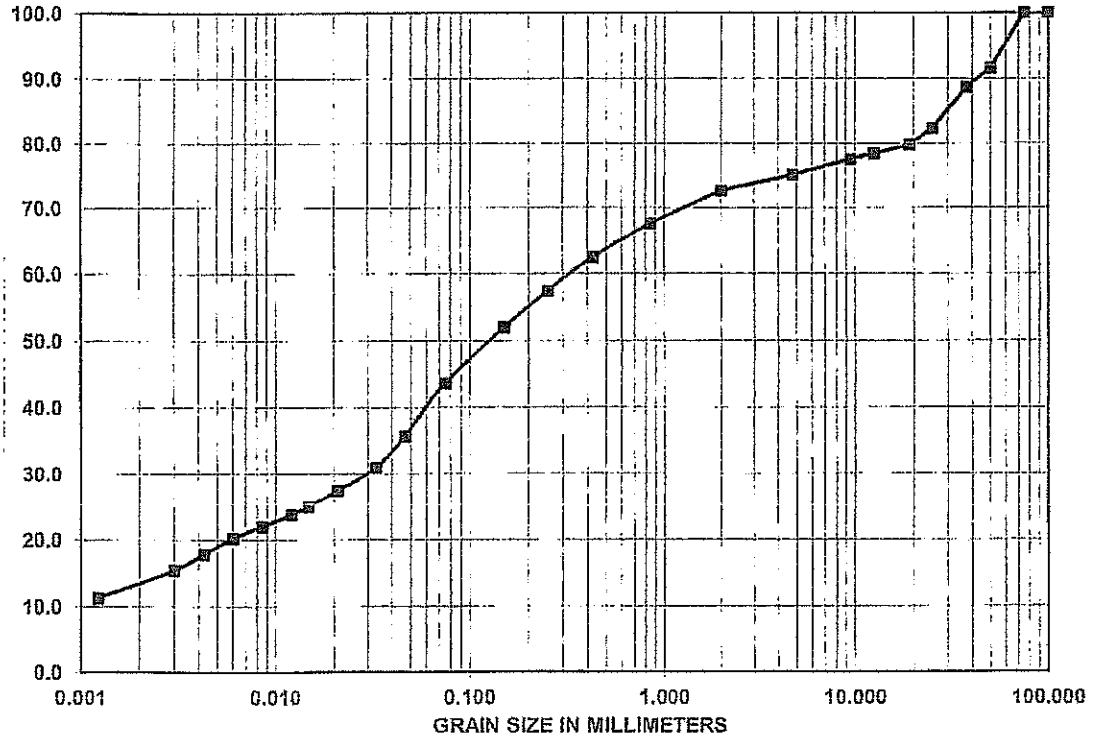
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 25-Jul-12

PROJECT NAME: Mt. Polley

TEST No: S12-08
SAMPLED BY: MPMC
DATE SAMPLED: 13-Jul-12
SOURCE: 36+00
DATE TESTED: 23-Jul-12
DEPTH:



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	91.6
37.5	88.6
25.0	82.3
19.0	79.8
12.5	78.4
9.5	77.5
4.75	75.1
2.00	72.7
0.850	67.6
0.425	62.4
0.250	57.4
0.150	52.0
0.075	43.6
0.0467	35.7
0.0330	30.9
0.0209	27.4
0.0148	25.0
0.0121	23.8
0.0085	22.0
0.0060	20.2
0.0043	17.8
0.0030	15.5
0.0012	11.3

REMARKS:

D_{10} =	N/A	GRAVEL	24.89%
D_{30} =	N/A	SAND	31.49%
D_{60} =	N/A	SILT	30.52%
C_U =	N/A	CLAY	13.09%
C_c =	N/A		

TECHNICIAN: LJ Michaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	36+00, Sample 3
Project Number:	VM00560A.B.3	Date Sampled:	13-Jul-12
Technician:	M. Tennant	Depth:	S12-08
Date:	23-Jul-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	16	36	22	
Tare ID	E	K	AL	
Mass Wet + Tare	50.90	47.99	45.62	
Mass Dry + Tare	44.78	42.96	40.82	
Mass Tare	21.32	21.55	21.77	
Mass of Water	6.12	5.03	4.80	
Dry Soil Mass	23.46	21.41	19.05	
Moisture Content	26.1	23.5	25.2	
Liquid Limit	24.7	24.7	24.8	

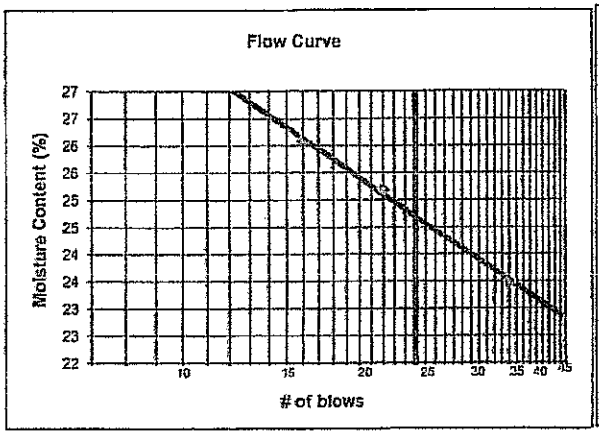
Average Liquid Limit: 25

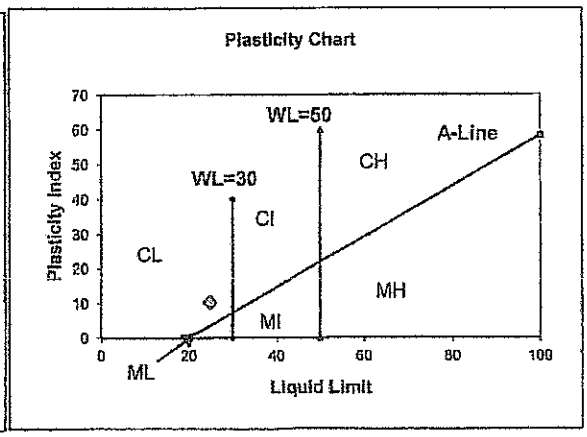
Plastic Limit

Trial No.	1	2	3	
Tare ID	46	16	47	
Mass Wet + Tare	33.03	32.30	32.16	
Mass Dry + Tare	31.55	30.92	30.81	
Mass Tare	21.39	21.39	21.45	
Mass of Water	1.48	1.38	1.35	
Dry Soil Mass	10.16	9.53	9.36	
Moisture Content	14.6	14.5	14.4	

Average Plastic Limit	14
Plasticity Index	11
Received Moisture	12.1

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





EC Environment & Infrastructure
A division of AMEC Americas Limited
6 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

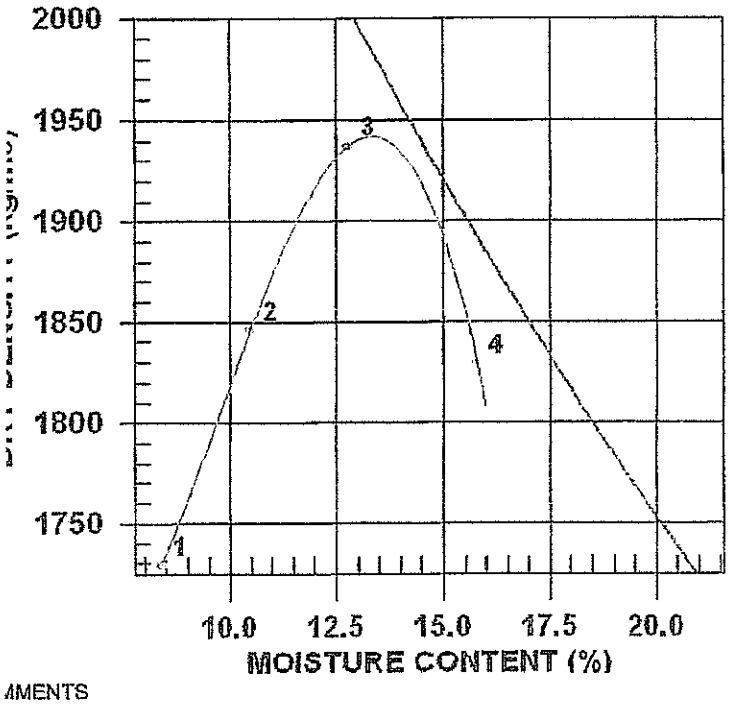
JECT Mount Polley

NTRACTOR

CTOR NO. 13 DATE TESTED 2012.Jul.18 DATE RECEIVED 2012.Jul.14 DATE SAMPLED 2012.Jul.13

TU MOISTURE	12.1 %
IPLED BY	MPMC
TED BY	D. deSousa
PLIER	36+00
URCE	S12-08
TERIAL IDENTIFICATION	
AJOR COMPONENT	Till
ZE	-75mm
ESCRIPTION	
OCK TYPE	

COMPACTION STANDARD	Standard Proctor, ASTM D698
COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
RAMMER TYPE	Automatic
PREPARATION	Moist
OVERSIZE CORRECTION METHOD	ASTM 4718
RETAINED 4.75mm SCREEN	25.0 %
OVERSIZE SPECIFIC GRAVITY	2.70
TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	1874	1729	8.4
2	2040	1846	10.5
3	2185	1937	12.8
4	2118	1829	15.8

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1942	13.5
OVERSIZE CORRECTED	2089	10.5

MMENTS

 2012.Jul.28 AMEC Environment & Infrastructure PER RMichaud

GRAIN SIZE DISTRIBUTION

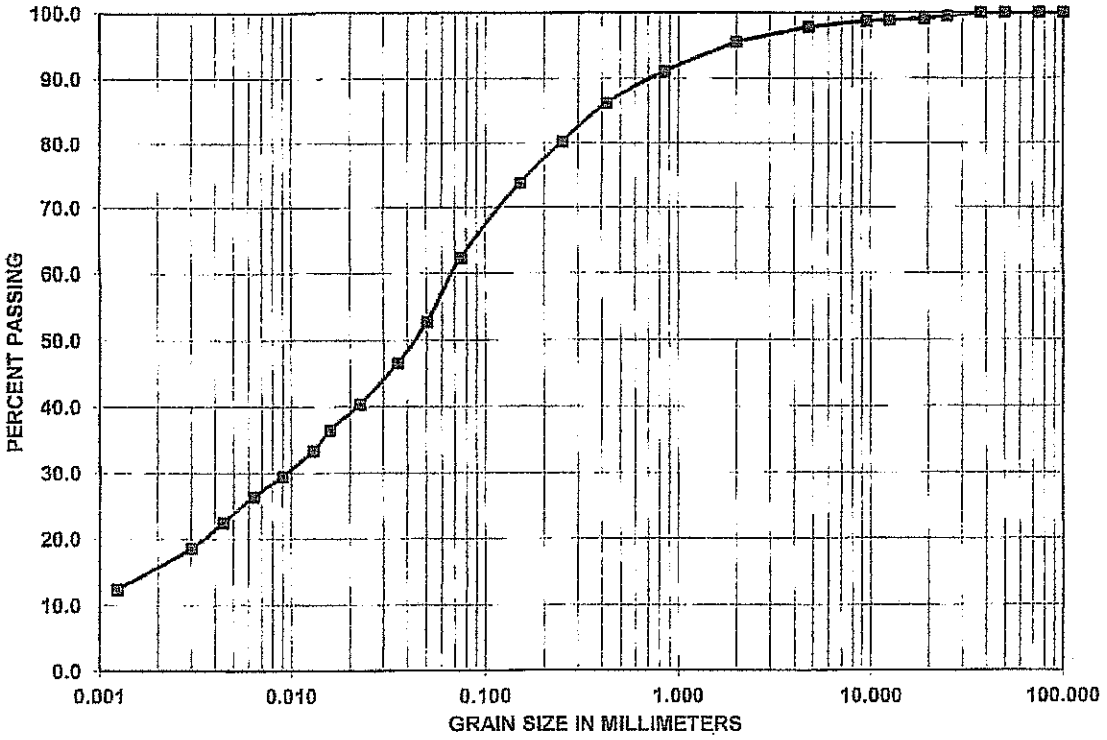
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 26-Jul-12

PROJECT NAME: Mt. Polley

TEST No: S12-09
SAMPLED BY: D. Ostritchenko
DATE SAMPLED: 18-Jul-12
SOURCE: Corner 5
DATE TESTED: 25-Jul-12
DEPTH: 1.0m



SUMMARY	
Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	100.0
25.0	99.5
19.0	99.0
12.5	98.9
9.5	98.7
4.75	97.8
2.00	95.6
0.850	91.1
0.425	86.2
0.250	80.3
0.150	73.7
0.075	62.3
0.0503	52.8
0.0356	46.5
0.0225	40.3
0.0159	36.5
0.0130	33.4
0.0090	29.5
0.0064	26.4
0.0044	22.5
0.0030	18.6
0.0012	12.4

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
Cu =	N/A
Cc =	N/A

GRAVEL	2.17%
SAND	35.51%
SILT	47.22%
CLAY	15.10%

TECHNICIAN: D Richard

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-09
Project Number:	VM00560A.B.3	Date Sampled:	18-Jul-12
Technician:	M. Tennant	Depth:	1.0m below grade
Date:	25-Jul-12	Comments:	Corner 5

Liquid Limit

Trial No.	1	2	3	
No. of Blows	14	24	33	
Tare ID	R	M	H	
Mass Wet + Tare	45.99	48.82	50.58	
Mass Dry + Tare	41.05	43.58	45.19	
Mass Tare	21.56	21.54	21.67	
Mass of Water	4.94	5.24	5.39	
Dry Soil Mass	19.49	22.04	23.52	
Moisture Content	25.3	23.8	22.9	
Liquid Limit	23.6	23.7	23.8	

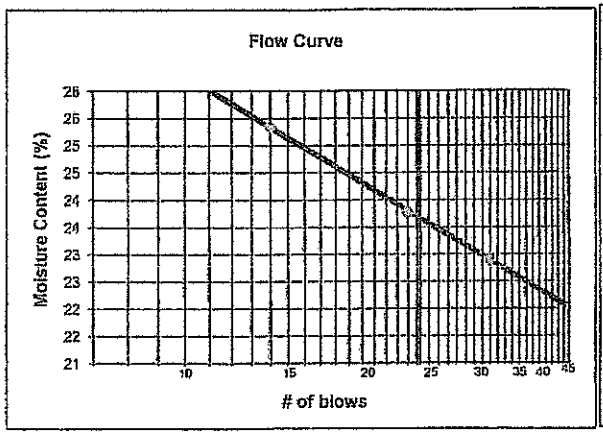
Average Liquid Limit: 24

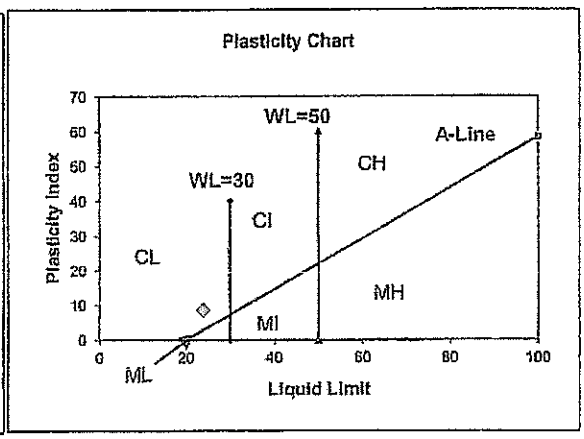
Plastic Limit

Trial No.	1	2	3	
Tare ID	22	38	40	
Mass Wet + Tare	30.99	30.22	30.69	
Mass Dry + Tare	29.74	29.04	29.48	
Mass Tare	21.47	21.33	21.47	
Mass of Water	1.25	1.18	1.21	
Dry Soil Mass	8.27	7.71	8.01	
Moisture Content	15.1	15.3	15.1	

Average Plastic Limit	15
Plasticity Index	9
Received Moisture	13.3

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





GRAIN SIZE DISTRIBUTION

amec

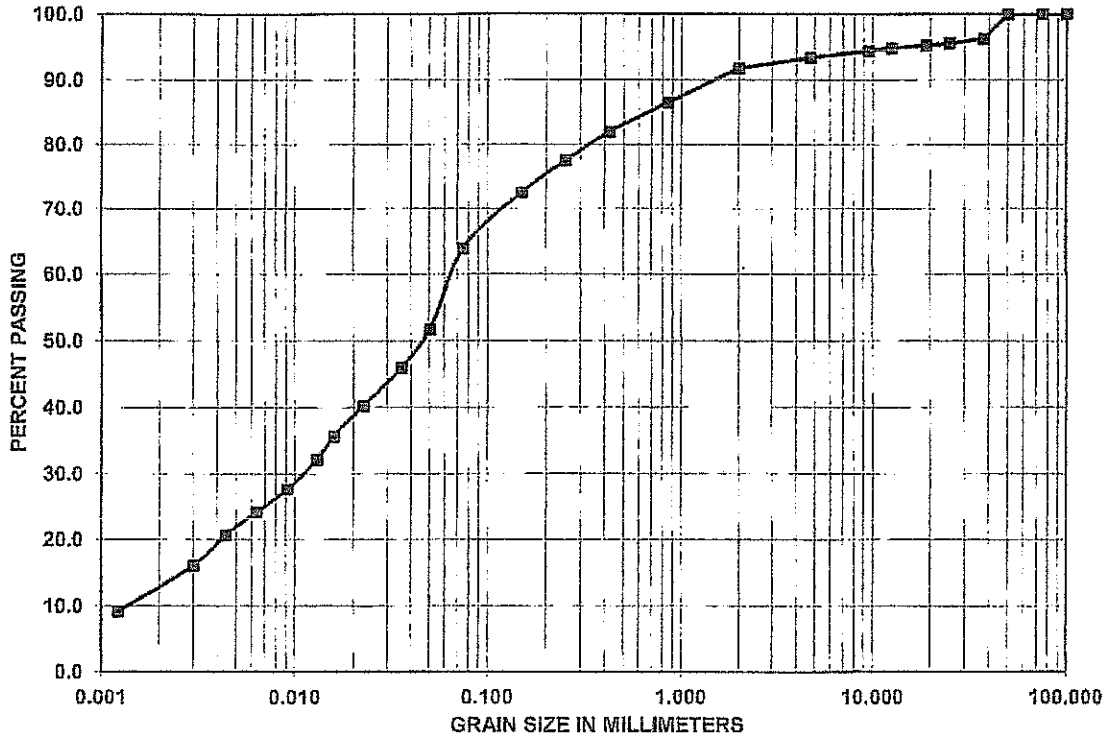
Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 26-Jul-12

PROJECT NAME: Mt. Polley

TEST No: S12-10
DATE SAMPLED: 18-Jul-12
DATE TESTED: 26-Jul-12

SAMPLED BY: D. Ostritchenko
SOURCE: Corner 5
DEPTH: 0.3m



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	96.2
25.0	95.5
19.0	95.3
12.5	94.8
9.5	94.4
4.75	93.4
2.00	91.8
0.850	86.4
0.425	81.9
0.250	77.5
0.150	72.5
0.075	63.9
0.0503	51.7
0.0356	46.0
0.0225	40.2
0.0159	35.6
0.0130	32.2
0.0092	27.6
0.0064	24.1
0.0044	20.7
0.0030	16.1
0.0012	9.2

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_C =	N/A

GRAVEL	6.64%
SAND	29.49%
SILT	51.68%
CLAY	12.19%

TECHNICIAN: JMcLeod

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-10
Project Number:	VM00560A.B.3	Date Sampled:	18-Jul-12
Technician:	M. Tennant	Depth:	0.3m below grade
Date:	25-Jul-12	Comments:	Corner 5

Liquid Limit

Trial No.	1	2	3	
No. of Blows	14	24	32	
Tare ID	AT	AG	AD	
Mass Wet + Tare	46.32	43.69	46.42	
Mass Dry + Tare	41.01	39.12	41.46	
Mass Tare	21.81	21.43	21.42	
Mass of Water	5.31	4.57	4.96	
Dry Soil Mass	19.20	17.69	20.04	
Moisture Content	27.7	25.8	24.8	
Liquid Limit	25.7	25.7	25.6	

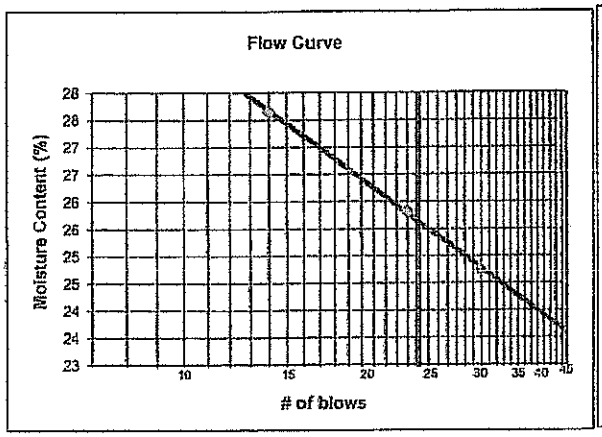
Average Liquid Limit: 26

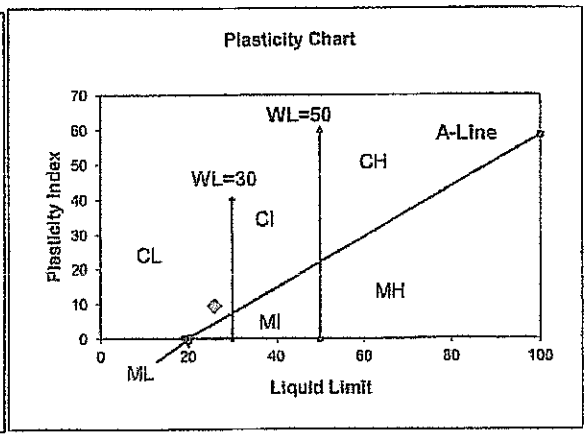
Plastic Limit

Trial No.	1	2	3	
Tare ID	1	2	4	
Mass Wet + Tare	31.45	36.55	31.41	
Mass Dry + Tare	30.06	34.43	30.02	
Mass Tare	21.55	21.60	21.51	
Mass of Water	1.39	2.12	1.39	
Dry Soil Mass	8.51	12.83	8.51	
Moisture Content	16.3	16.5	16.3	

Average Plastic Limit	16
Plasticity Index	10
Received Moisture	15.6

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





GRAIN SIZE DISTRIBUTION

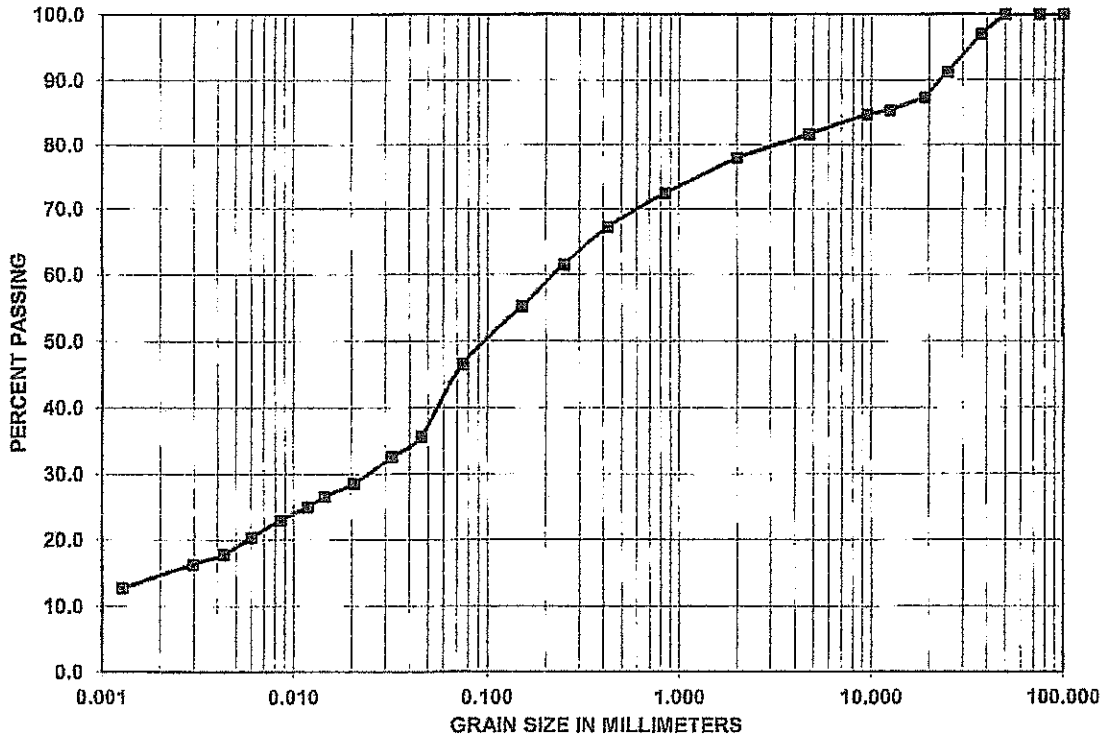
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 10-Aug-12

PROJECT NAME: Mt. Polley

TEST No: S12-11
SAMPLED BY: MPMC
DATE SAMPLED: 28-Jul-12
SOURCE: Borrow
DATE TESTED: 9-Aug-12
DEPTH:



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	97.0
25.0	91.2
19.0	87.3
12.5	85.3
9.5	84.7
4.75	81.6
2.00	78.0
0.850	72.5
0.425	67.2
0.250	61.5
0.150	55.2
0.075	46.6
0.0459	35.7
0.0324	32.6
0.0205	28.5
0.0145	26.5
0.0118	25.0
0.0085	22.9
0.0060	20.4
0.0043	17.8
0.0030	16.3
0.0013	12.7

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_C =	N/A

GRAVEL	18.36%
SAND	35.05%
SILT	32.32%
CLAY	14.27%

TECHNICIAN: M Michaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-11
Project Number:	VM00560A.B.3	Date Sampled:	28-Jul-12
Technician:	M. Tennant	Depth:	Borrow Pit
Date:	9-Aug-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	24	18	32	
Tare ID	H	AS	K	
Mass Wet + Tare	48.32	48.89	46.74	
Mass Dry + Tare	43.23	43.51	42.05	
Mass Tare	21.65	21.66	21.60	
Mass of Water	5.09	5.38	4.69	
Dry Soil Mass	21.58	21.85	20.45	
Moisture Content	23.6	24.6	22.9	
Liquid Limit	23.5	23.6	23.7	

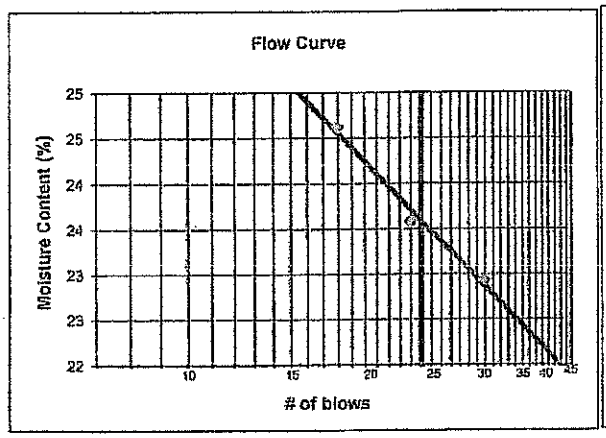
Average Liquid Limit: 24

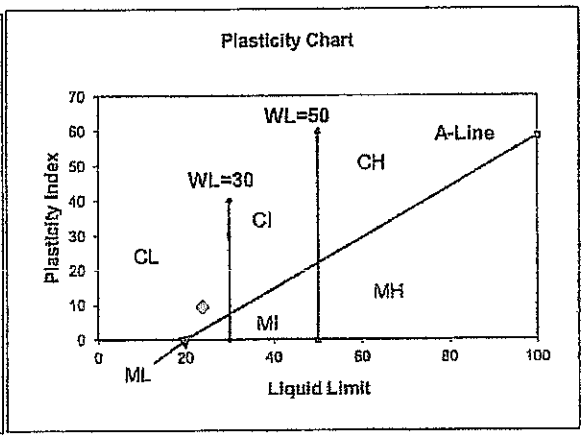
Plastic Limit

Trial No.	1	2	3	
Tare ID	35	24	28	
Mass Wet + Tare	33.32	31.41	31.65	
Mass Dry + Tare	31.81	30.18	30.34	
Mass Tare	21.37	21.56	21.31	
Mass of Water	1.51	1.23	1.31	
Dry Soil Mass	10.44	8.62	9.03	
Moisture Content	14.5	14.3	14.5	

Average Plastic Limit	14
Plasticity Index	10
Received Moisture	9.9

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





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A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

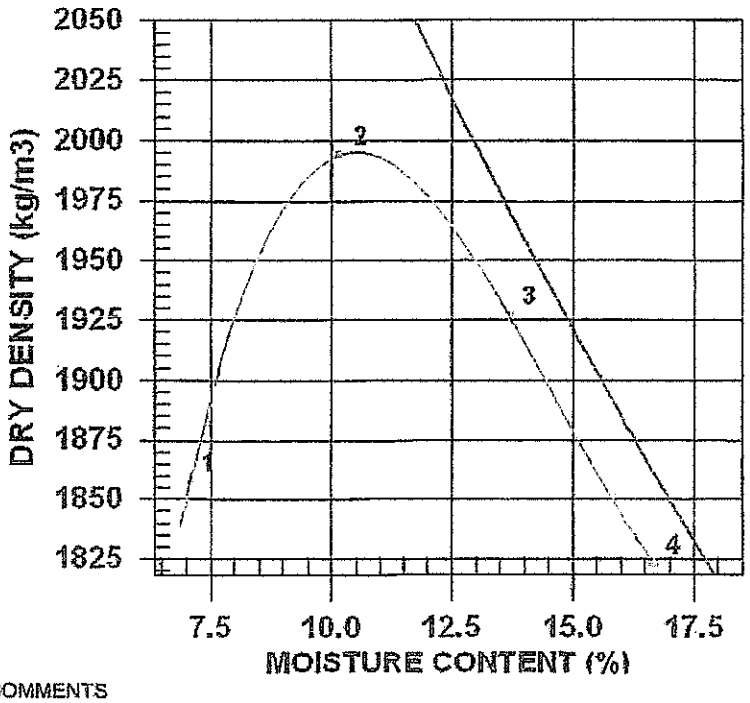
TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

PROJECT Mount Polley

CONTRACTOR

PROCTOR NO. 14 DATE TESTED 2012.Aug.02 DATE RECEIVED 2012.Jul.29 DATE SAMPLED 2012.Jul

INSITU MOISTURE	9.9 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
SAMPLED BY	MPMC		
TESTED BY	M. deHart	COMPACTION PROCEDURE	C: 152.4mm Mold, Passing 19mm
SUPPLIER	Borrow Pit		
SOURCE	S12-11	RAMMER TYPE	Automatic
MATERIAL IDENTIFICATION		PREPARATION	Moist
MAJOR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
SIZE	-50mm	RETAINED 19mm SCREEN	10.0 %
DESCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
ROCK TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	1990	1858	7.1
2	2197	1994	10.2
3	2191	1927	13.7
4	2127	1823	16.7

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1995	10.5
OVERSIZE CORRECTED	2048	9.5

COMMENTS

 2012.Aug.10 AMEC Environment & Infrastructure PER. LMichaud

GRAIN SIZE DISTRIBUTION

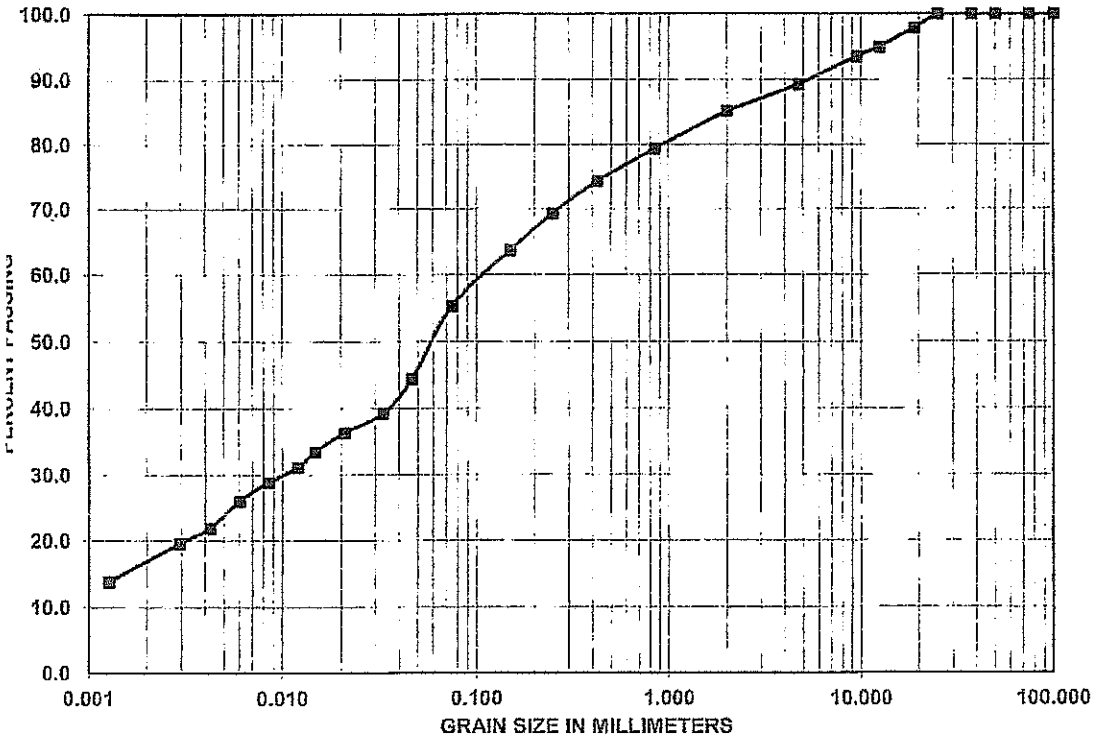
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 28ug12

PROJECT NAME: Stage 8 Dam Raise - 2012

TEST No: S12-12
SAMPLED BY: MPMC staff
DATE SAMPLED: 4-Aug-12
SOURCE: Main Embankment
DATE TESTED: 16-Aug-12
DEPTH: Sta 22+25, elv. 960.9m



SUMMARY	
Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	100.0
25.0	100.0
19.0	97.8
12.5	95.0
9.5	93.5
4.75	89.3
2.00	85.2
0.850	79.4
0.425	74.3
0.250	69.3
0.150	63.7
0.075	55.3
0.0466	44.4
0.0329	39.2
0.0209	36.3
0.0148	33.6
0.0121	31.1
0.0085	28.8
0.0060	26.0
0.0043	21.9
0.0030	19.6
0.0013	13.8

REMARKS:

D_{10} =	N/A	GRAVEL	10.70%
D_{30} =	N/A	SAND	33.98%
D_{60} =	N/A	SILT	38.99%
C_u =	N/A	CLAY	16.33%
C_c =	N/A		

TECHNICIAN: M Michaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-12 - Main Embankment
Project Number:	VM00560A.B.3	Date Sampled:	4-Aug-12
Technician:	M. Tennant	Depth:	Elv. 960.9m
Date:	10-Aug-12	Comments:	Sta 22+25

Liquid Limit

Trial No.	1	2	3	
No. of Blows	32	12	24	
Tare ID	R	A	AF	
Mass Wet + Tare	41.75	49.01	45.20	
Mass Dry + Tare	37.90	43.11	40.46	
Mass Tare	22.02	21.75	21.75	
Mass of Water	3.85	5.90	4.74	
Dry Soil Mass	15.88	21.36	18.71	
Moisture Content	24.2	27.6	25.3	
Liquid Limit	25.1	25.2	25.2	

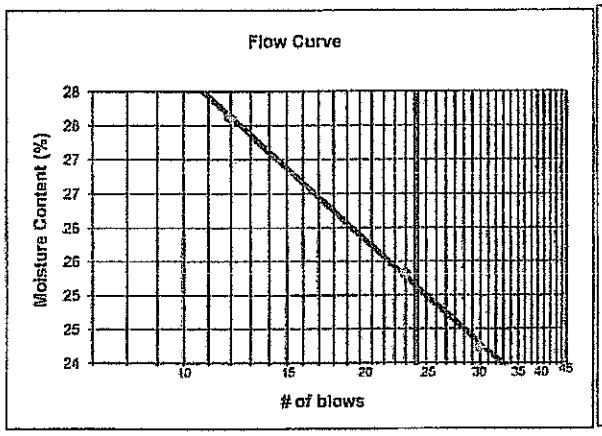
Average Liquid Limit: 25

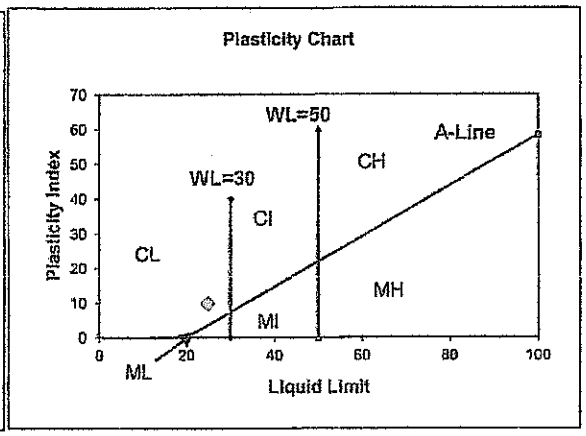
Plastic Limit

Trial No.	1	2	3	
Tare ID	25	40	22	
Mass Wet + Tare	31.49	33.13	34.14	
Mass Dry + Tare	30.19	31.61	32.50	
Mass Tare	21.43	21.48	21.47	
Mass of Water	1.30	1.52	1.64	
Dry Soil Mass	8.76	10.13	11.03	
Moisture Content	14.8	15.0	14.9	

Average Plastic Limit	15
Plasticity Index	10
Received Moisture	9.2

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





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6 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

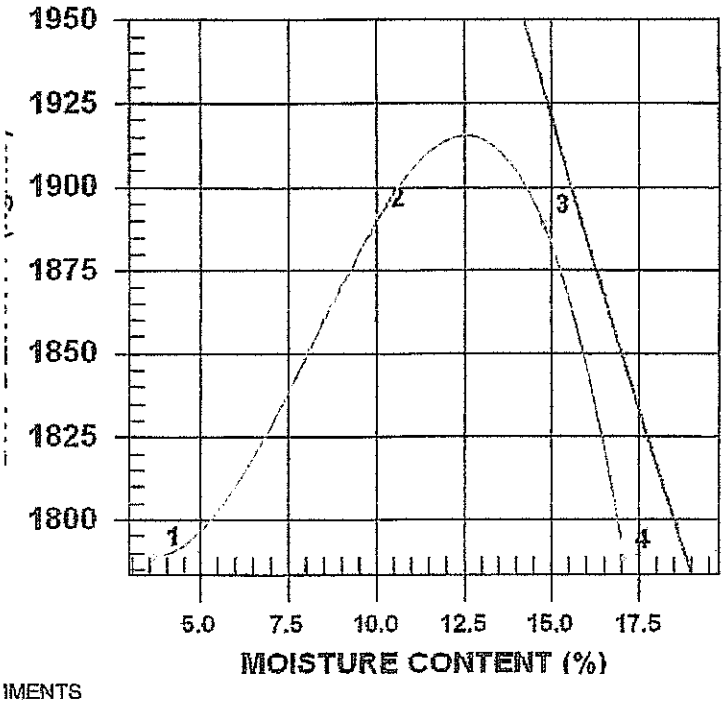
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

JECT Mount Polley

ITRACTOR

CTOR NO. 15 DATE TESTED 2012.Aug.10 DATE RECEIVED 2012.Aug.09 DATE SAMPLED 2012.Aug.04

TU MOISTURE	9.2 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
IPLED BY	MPMC staff		
TED BY	J. McDonald	COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
PLIER	Main Embankment		
IRCE	S12-12	RAMMER TYPE	Automatic
ERIAL IDENTIFICATION		PREPARATION	Moist
JOR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
E	19mm	RETAINED 4.75mm SCREEN	10.0 %
SCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
CK TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	1855	1789	3.7
2	2082	1891	10.1
3	2168	1889	14.8
4	2094	1788	17.1

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1915	12.5
OVERSIZE CORRECTED	1972	11.5

IMENTS

 2012.Aug.23 AMEC Environment & Infrastructure PER. M Nichaick

GRAIN SIZE DISTRIBUTION

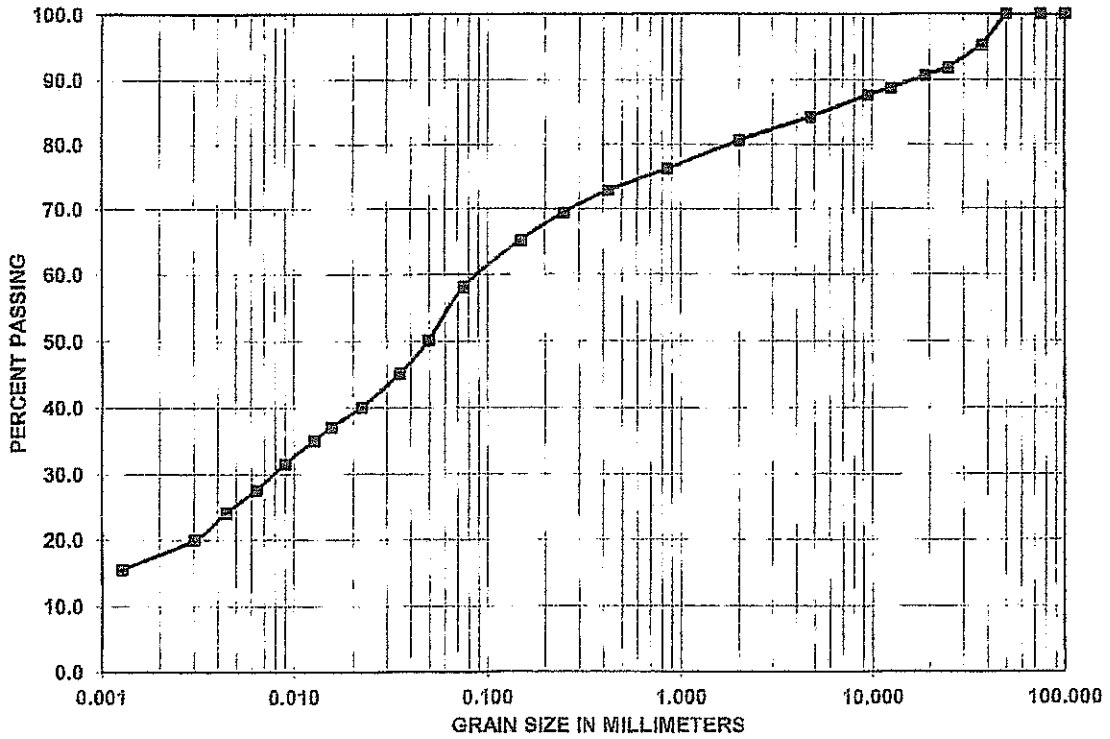
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 23-Aug-12

PROJECT NAME: Mt. Polley

TEST No: S12-13
SAMPLED BY: MPMC staff
DATE SAMPLED: 12-Aug-12
SOURCE: Till Borrow
DATE TESTED: 22-Aug-12
DEPTH:



SUMMARY	
Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	95.2
25.0	91.8
19.0	90.7
12.5	88.8
9.5	87.6
4.75	84.2
2.00	80.7
0.850	76.3
0.425	72.9
0.250	69.4
0.150	65.2
0.075	58.1
0.0494	50.1
0.0349	45.1
0.0221	40.1
0.0156	37.1
0.0128	35.1
0.0090	31.6
0.0064	27.6
0.0044	24.1
0.0030	20.0
0.0013	15.5

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	15.76%
SAND	26.16%
SILT	40.67%
CLAY	17.42%

TECHNICIAN: YMichaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-13
Project Number:	VM00560A.B.3	Date Sampled:	12-Aug-12
Technician:	M. Tennant	Depth:	
Date:	17-Aug-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	18	27	30	
Tare ID	H	Q	AR	
Mass Wet + Tare	39.27	43.98	47.20	
Mass Dry + Tare	35.60	39.49	42.18	
Mass Tare	21.68	21.60	22.02	
Mass of Water	3.67	4.49	5.02	
Dry Soil Mass	13.92	17.89	20.16	
Moisture Content	26.4	25.1	24.9	
Liquid Limit	25.3	25.4	25.5	

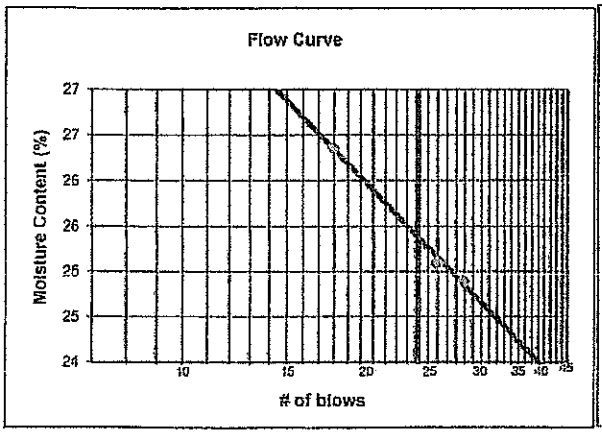
Average Liquid Limit: 25

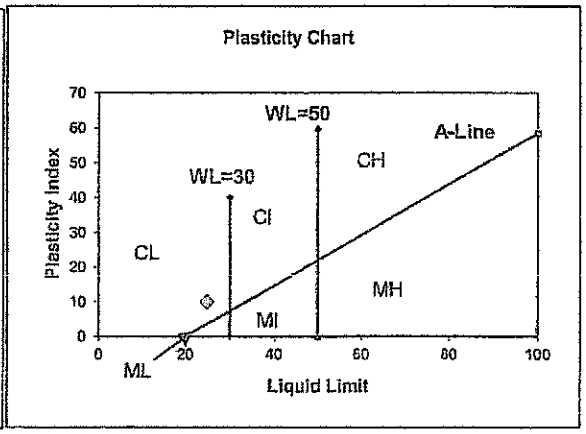
Plastic Limit

Trial No.	1	2	3	
Tare ID	18	27	35	
Mass Wet + Tare	32.99	29.39	31.83	
Mass Dry + Tare	31.48	28.37	30.48	
Mass Tare	21.36	21.46	21.35	
Mass of Water	1.51	1.02	1.35	
Dry Soil Mass	10.12	6.91	9.13	
Moisture Content	14.9	14.8	14.8	

Average Plastic Limit	15
Plasticity Index	10
Received Moisture	12.7

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





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A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

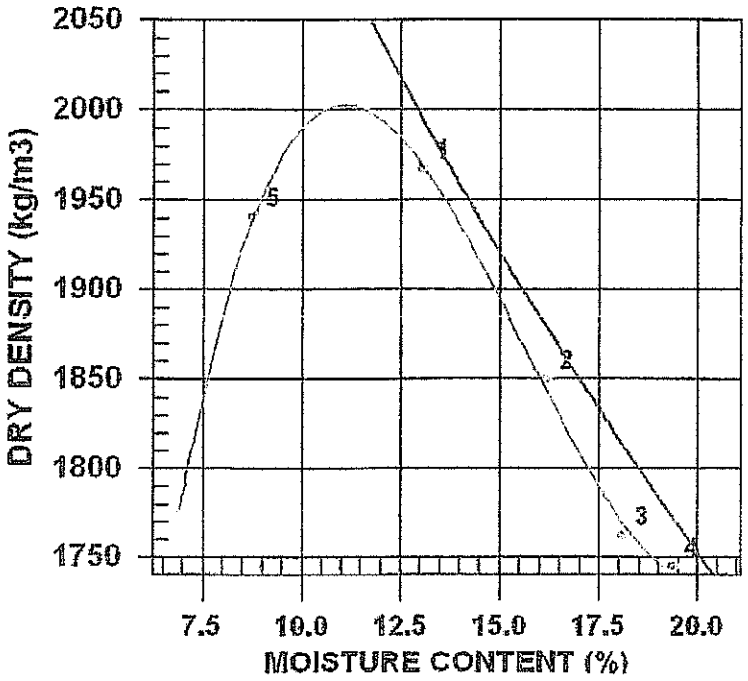
TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

PROJECT Mount Polley

CONTRACTOR

PROCTOR NO. 16 DATE TESTED 2012.Aug.18 DATE RECEIVED 2012.Aug.16 DATE SAMPLED 2012.Aug.

INSITU MOISTURE	12.7 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
SAMPLED BY	MPMC staff		
TESTED BY	M. deHart	COMPACTION PROCEDURE	C: 152.4mm Mold, Passing 19mm
SUPPLIER	S12-04		
SOURCE	S12-13	RAMMER TYPE	Automatic
MATERIAL IDENTIFICATION		PREPARATION	Moist
MAJOR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
SIZE	37.5mm	RETAINED 19mm SCREEN	10.0 %
DESCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
ROCK TYPE		TOTAL NUMBER OF TRIALS	5



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2225	1967	13.1
2	2150	1850	16.2
3	2081	1762	18.1
4	2084	1745	19.4
5	2112	1941	8.8

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	2003	11.0
OVERSIZE CORRECTED	2056	10.0

COMMENTS

 2012.Aug.23 AMEC Environment & Infrastructure PER. AMichaud

GRAIN SIZE DISTRIBUTION

amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 06-Sep-12

PROJECT NAME: Mt. Polley

TEST No:

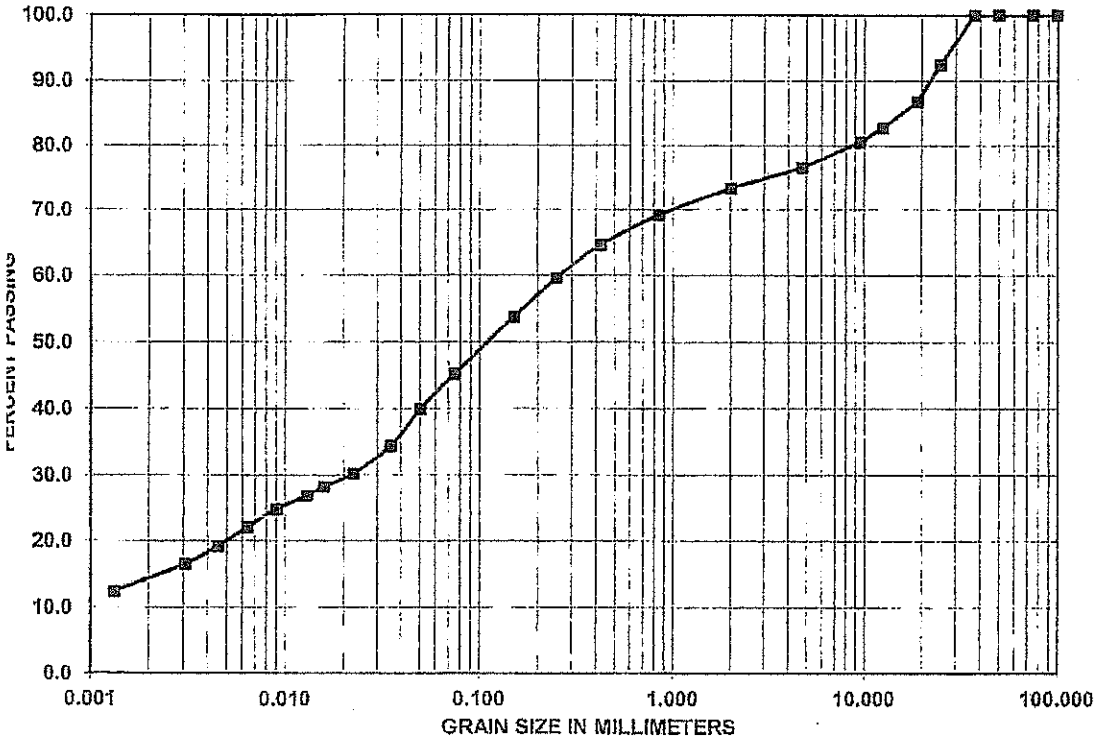
SAMPLED BY: MPMC

DATE SAMPLED: 27-Aug-12

SOURCE: Till Borrow

DATE TESTED: 3-Sep-12

DEPTH:



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	100.0
25.0	92.5
19.0	86.8
12.5	82.7
9.5	80.5
4.75	76.6
2.00	73.4
0.850	69.2
0.425	64.6
0.250	59.6
0.150	53.8
0.075	45.2
0.0502	39.9
0.0355	34.4
0.0224	30.3
0.0159	28.2
0.0130	26.8
0.0090	24.8
0.0064	22.0
0.0045	19.3
0.0031	16.5
0.0013	12.4

EMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	23.40%
SAND	31.42%
SILT	31.19%
CLAY	13.98%

ECHNICIAN: JJ Michaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-04
Project Number:	VM00560A.B.3	Date Sampled:	27-Aug-12
Technician:	J. McDonald	Depth:	
Date:	4-Sep-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	34	24	13	
Tare ID	CD	B	E	
Mass Wet + Tare	35.46	44.51	43.78	
Mass Dry + Tare	31.38	40.11	39.20	
Mass Tare	13.48	21.80	21.50	
Mass of Water	4.08	4.40	4.58	
Dry Soil Mass	17.90	18.31	17.70	
Moisture Content	22.8	24.0	25.9	
Liquid Limit	23.8	23.9	23.9	

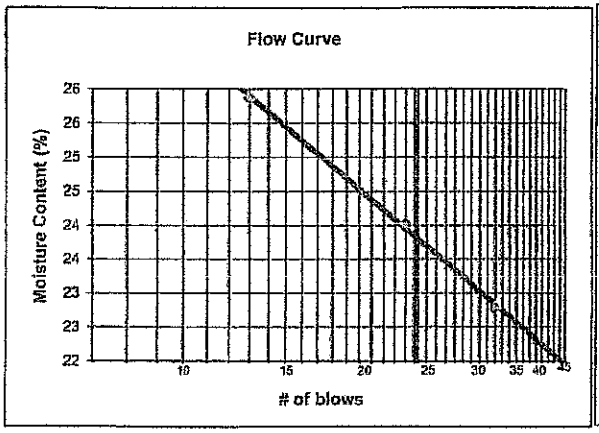
Average Liquid Limit: 24

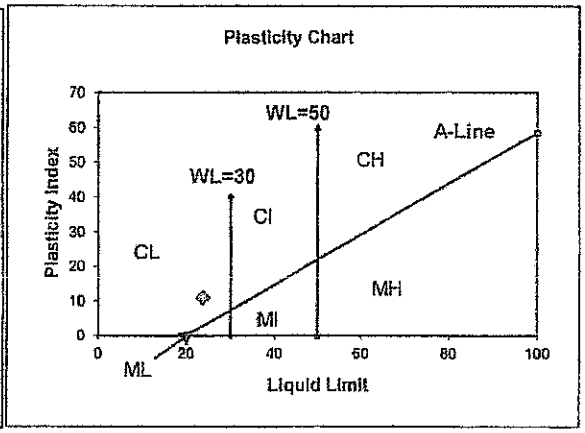
Plastic Limit

Trial No.	1	2	3	
Tare ID	25	22	8	
Mass Wet + Tare	34.26	33.41	23.64	
Mass Dry + Tare	32.78	32.06	22.63	
Mass Tare	21.48	21.46	14.71	
Mass of Water	1.48	1.35	1.01	
Dry Soil Mass	11.30	10.60	7.92	
Moisture Content	13.1	12.7	12.8	

Average Plastic Limit	13
Plasticity Index	11
Received Moisture	12.0

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





EC Environment & Infrastructure
A division of AMEC Americas Limited
6 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

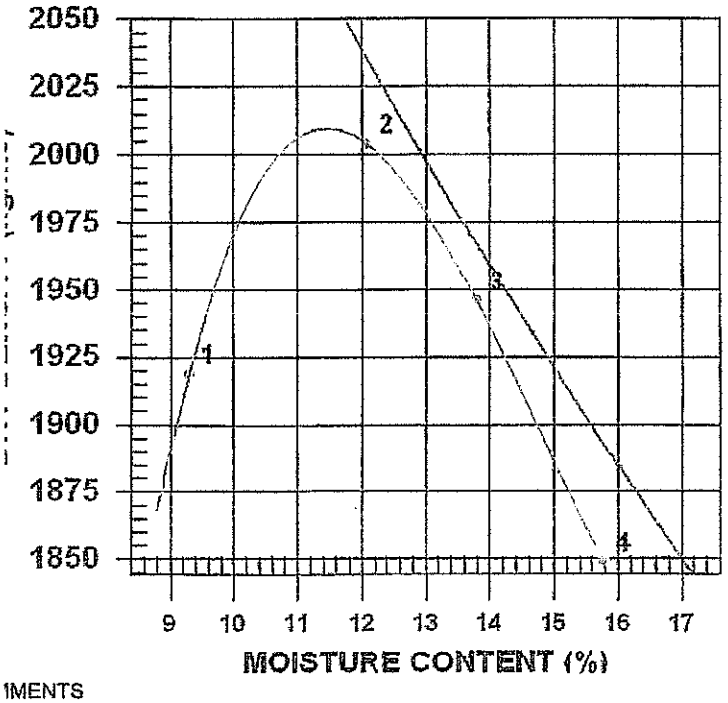
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

JECT Mount Polley

ITRACTOR

CTOR NO. 17 DATE TESTED 2012.Sep.04 DATE RECEIVED 2012.Aug.30 DATE SAMPLED 2012.Aug.27

TU MOISTURE	12.0 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
IPLED BY	MPMC		
TED BY	M. Tennant	COMPACTION PROCEDURE	C: 152.4mm Mold, Passing 19mm
PLIER	S12-04		
IRCE	S12-14	RAMMER TYPE	Automatic
ERIAL IDENTIFICATION		PREPARATION	Moist
JOR COMPONENT	Till	OVERSIZE CORRECTION METHOD	ASTM 4718
ZE	37.5mm	RETAINED 19mm SCREEN	15.0 %
SCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
CK TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2097	1919	9.3
2	2246	2004	12.1
3	2214	1946	13.8
4	2141	1849	15.8

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	2010	11.5
OVERSIZE CORRECTED	2090	10.0

MENTS

 2012.Sep.06 AMEC Environment & Infrastructure PER. HMichaud

GRAIN SIZE DISTRIBUTION

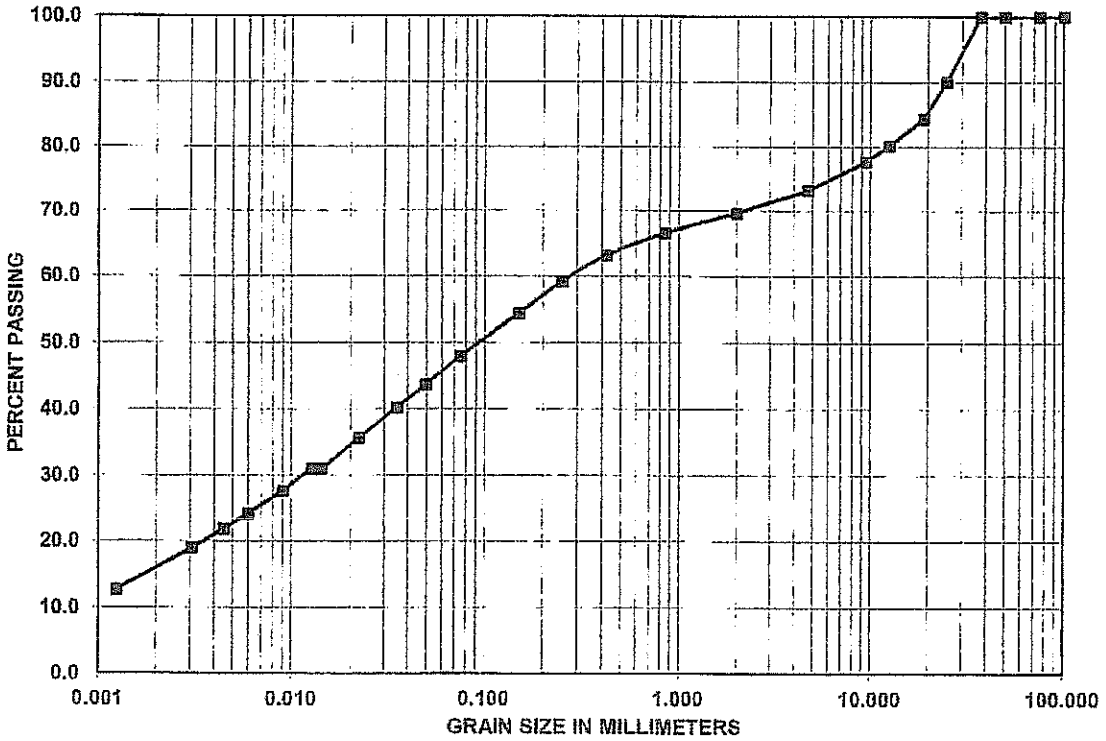
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 06-Oct-12

PROJECT NAME: Mt. Polley

TEST No: S12-15
SAMPLED BY: MPMC staff
DATE SAMPLED: 10-Sep-12
SOURCE: Sta 38+88 Perimeter Eembankme
DATE TESTED: 23-Sep-12
DEPTH: Elv. 951.0m



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	100.0
25.0	90.0
19.0	84.3
12.5	80.1
9.5	77.7
4.75	73.2
2.00	69.6
0.850	66.6
0.425	63.1
0.250	59.2
0.150	54.4
0.075	47.9
0.0494	43.7
0.0349	40.2
0.0221	35.6
0.0143	31.0
0.0128	31.0
0.0090	27.6
0.0060	24.1
0.0045	21.8
0.0031	19.0
0.0012	12.6

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	26.78%
SAND	25.29%
SILT	32.67%
CLAY	15.26%

TECHNICIAN: JM Matawesh

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-15, Sta 38+88
Project Number:	VM00560A.B.3	Date Sampled:	10-Sep-12
Technician:	B. Garlick	Depth:	Elv. 961.0m
Date:	22-Sep-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	35	26	15	
Tare ID	44	4	27	
Mass Wet + Tare	41.25	44.25	40.45	
Mass Dry + Tare	37.19	39.43	36.18	
Mass Tare	21.46	21.54	21.48	
Mass of Water	4.06	4.82	4.27	
Dry Soil Mass	15.73	17.89	14.70	
Moisture Content	25.8	26.9	29.0	
Liquid Limit	27.0	27.1	27.2	

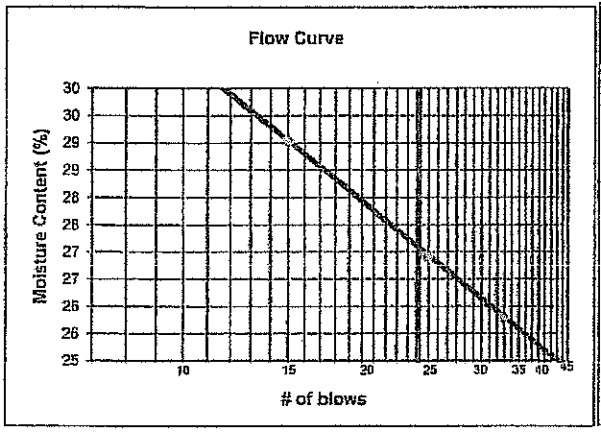
Average Liquid Limit: 27

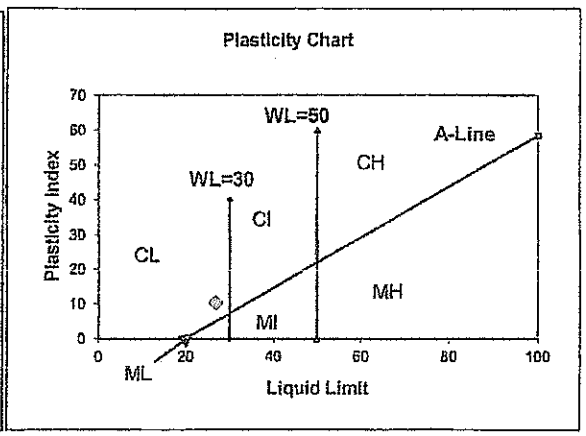
Plastic Limit

Trial No.	1	2	3	
Tare ID	15	19	2	
Mass Wet + Tare	33.94	34.96	33.63	
Mass Dry + Tare	32.28	33.13	31.97	
Mass Tare	22.08	22.11	21.64	
Mass of Water	1.66	1.83	1.66	
Dry Soil Mass	10.20	11.02	10.33	
Moisture Content	16.3	16.6	16.1	

Average Plastic Limit	16
Plasticity Index	11
Received Moisture	12.0

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





GRAIN SIZE DISTRIBUTION

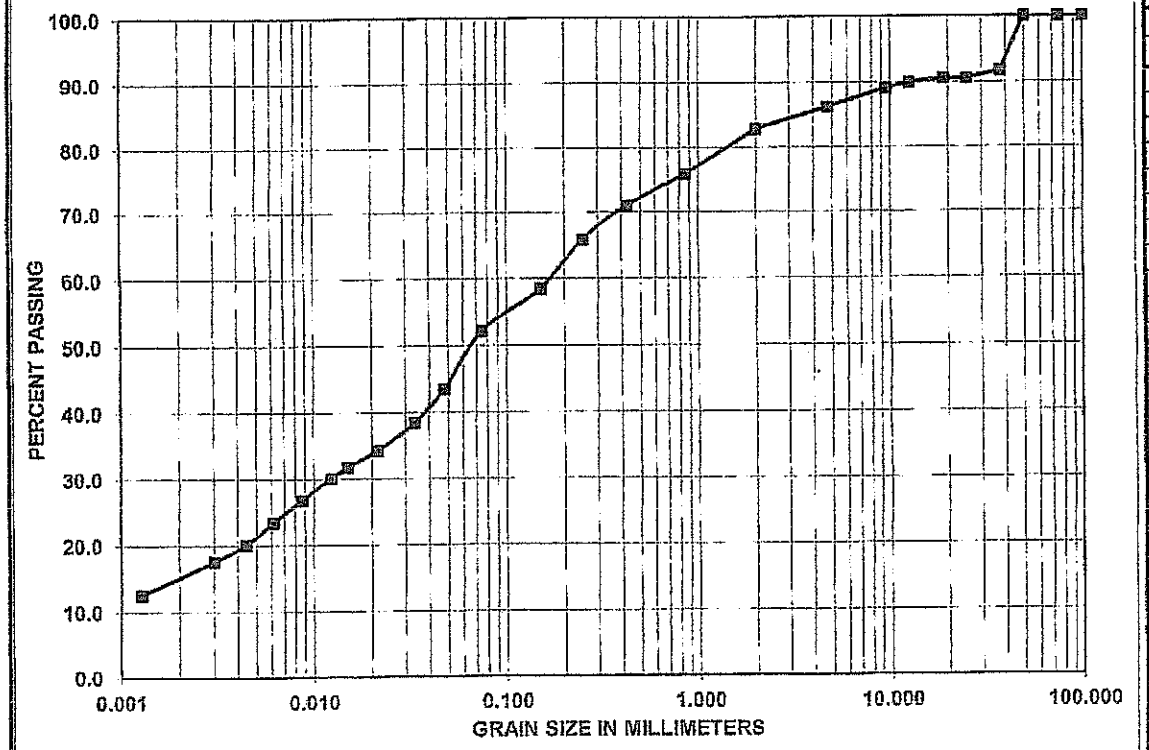
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 29-Oct-12

PROJECT NAME: Mt. Polley

TEST No: S12-16
SAMPLED BY: MPMC Staff
DATE SAMPLED: 15-Sep-12
SOURCE: Sta 27+44
DATE TESTED: 27-Oct-12
DEPTH: Elv. 962.37m



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	91.7
25.0	90.6
19.0	90.6
12.5	90.0
9.5	89.1
4.75	86.2
2.00	82.8
0.850	75.9
0.425	71.0
0.250	65.8
0.150	58.5
0.075	52.2
0.0476	43.5
0.0337	38.5
0.0213	34.3
0.0151	31.8
0.0123	30.1
0.0087	26.8
0.0061	23.4
0.0044	20.1
0.0030	17.6
0.0013	12.5

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	13.81%
SAND	33.99%
SILT	37.57%
CLAY	14.63%

TECHNICIAN: JMichaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-16 (Sta 27+44)
Project Number:	VM00560A.B.3	Date Sampled:	15-Sep-12
Technician:	J. McDonald	Depth:	Elv. 962.37m
Date:	25-Oct-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	24	29	36	
Tare ID	AT	AS	AG	
Mass Wet + Tare	35.10	34.62	35.25	
Mass Dry + Tare	32.34	31.99	32.54	
Mass Tare	21.76	21.62	21.58	
Mass of Water	2.76	2.63	2.71	
Dry Soil Mass	10.58	10.37	10.96	
Moisture Content	26.1	25.4	24.7	
Liquid Limit	26.0	25.9	26.0	

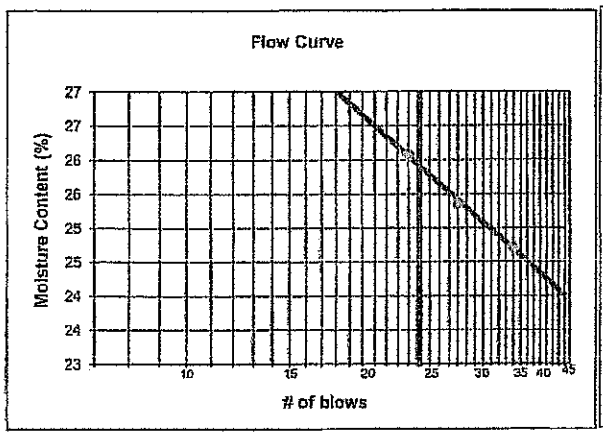
Average Liquid Limit: 26

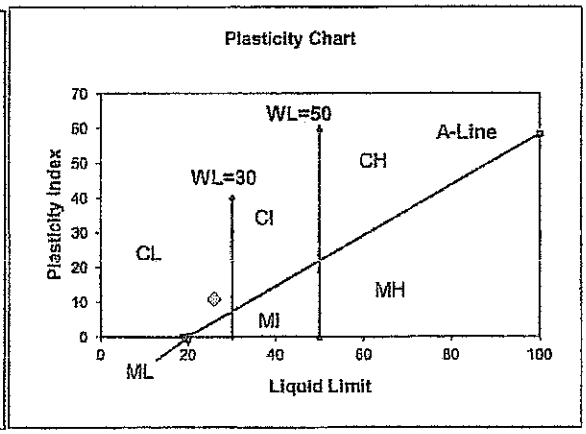
Plastic Limit

Trial No.	1	2	3	
Tare ID	30	2	23	
Mass Wet + Tare	33.27	33.18	33.42	
Mass Dry + Tare	31.72	31.68	31.88	
Mass Tare	21.35	21.63	21.48	
Mass of Water	1.55	1.50	1.54	
Dry Soil Mass	10.37	10.05	10.40	
Moisture Content	14.9	14.9	14.8	

Average Plastic Limit	15
Plasticity Index	11
Received Moisture	9.7

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

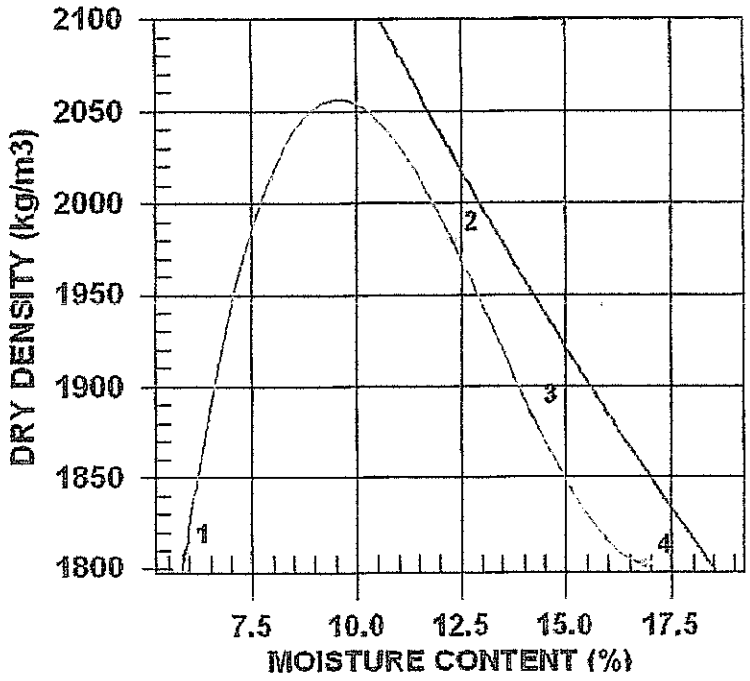
TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

PROJECT Mount Polley

CONTRACTOR

PROCTOR NO. 18 DATE TESTED 2012.Oct.24 DATE RECEIVED 2012.Sep.20 DATE SAMPLED 2012.Sep.

INSITU MOISTURE	10.0 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
SAMPLED BY	MPMC Staff		
TESTED BY	D. DeSousa	COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
SUPPLIER	Sta 27+44, Elv. 962.37m		
SOURCE	S12-16	RAMMER TYPE	Automatic
MATERIAL IDENTIFICATION		PREPARATION	Moist
MAJOR COMPONENT	Glacial Till	OVERSIZE CORRECTION METHOD	ASTM 4718
SIZE	-37.5mm	RETAINED 4.75mm SCREEN	15.0 %
DESCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
ROCK TYPE		TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	1916	1809	5.9
2	2223	1980	12.3
3	2153	1885	14.2
4	2106	1802	16.9

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	2056	9.5
OVERSIZE CORRECTED	2132	8.0

COMMENTS

 2012.Oct.29 AMEC Environment & Infrastructure PER. JMichaud

GRAIN SIZE DISTRIBUTION

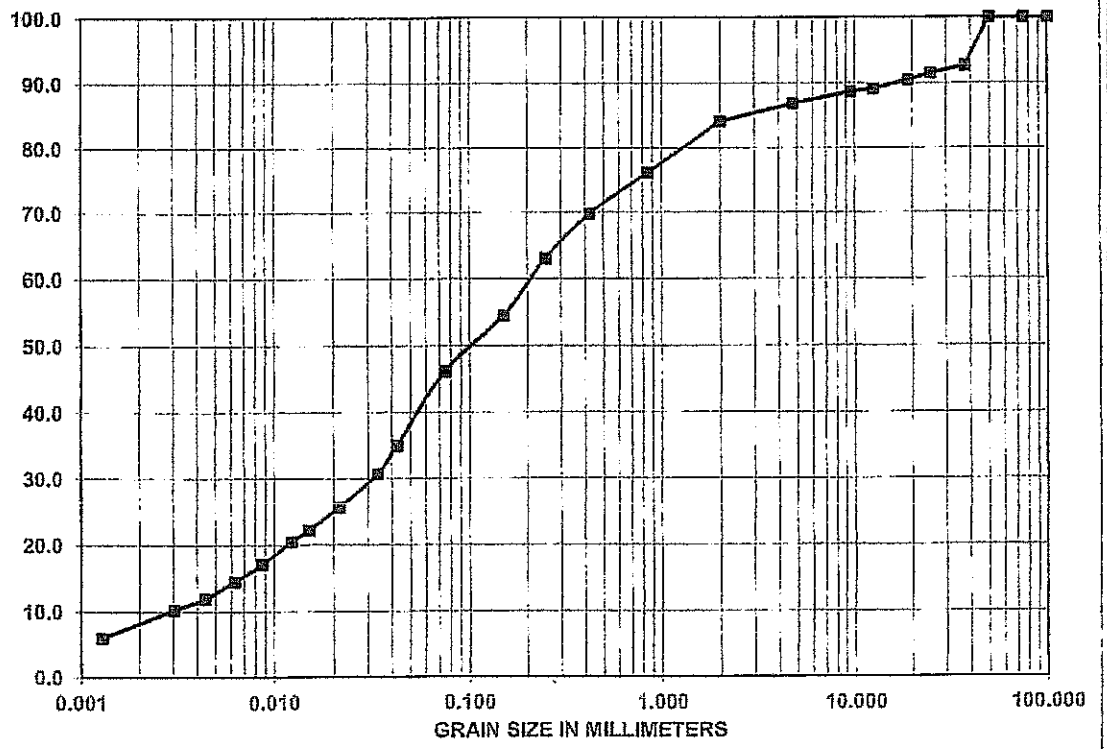
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 29-Oct-12

PROJECT NAME: Mt. Polley

TEST No: S12-17
SAMPLED BY: MPMC Staff
DATE SAMPLED: 21-Sep-12
SOURCE: Borrow Pit
DATE TESTED: 27-Oct-12
DEPTH:



SUMMARY	
Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	92.6
25.0	91.5
19.0	90.5
12.5	89.1
9.5	88.6
4.75	86.8
2.00	84.0
0.850	76.2
0.425	69.8
0.250	63.1
0.150	54.5
0.075	46.2
0.0426	35.0
0.0337	30.8
0.0213	25.6
0.0151	22.2
0.0123	20.5
0.0087	17.1
0.0062	14.5
0.0044	12.0
0.0030	10.3
0.0013	6.0

EMARKS:

D_{10} =	N/A	GRAVEL	13.21%
D_{30} =	N/A	SAND	40.58%
D_{60} =	N/A	SILT	38.46%
C_U =	N/A	CLAY	7.74%
C_c =	N/A		

ECHNICIAN: YMichaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-17 (Borrow Pit)
Project Number:	VM00560A.B.3	Date Sampled:	21-Sep-12
Technician:	J. McDonald	Depth:	
Date:	25-Oct-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	19	37	29	
Tare ID	BB	BH	BC	
Mass Wet + Tare	34.47	38.21	29.51	
Mass Dry + Tare	31.30	34.66	27.30	
Mass Tare	15.83	15.90	15.91	
Mass of Water	3.17	3.55	2.21	
Dry Soil Mass	15.47	18.76	11.39	
Moisture Content	20.5	18.9	19.4	
Liquid Limit	19.8	19.9	19.8	

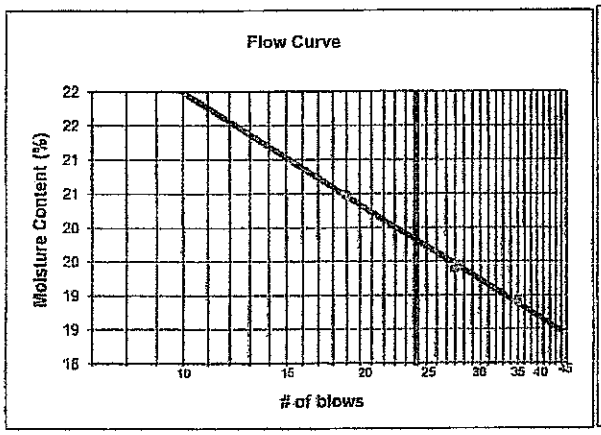
Average Liquid Limit: 20

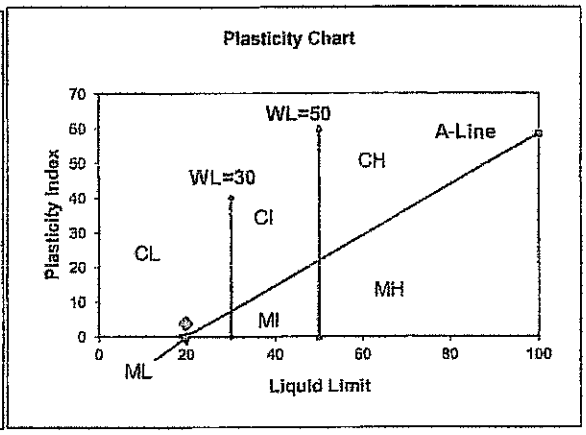
Plastic Limit

Trial No.	1	2	3	
Tare ID	10	41	5	
Mass Wet + Tare	38.22	36.11	39.49	
Mass Dry + Tare	35.92	34.10	37.02	
Mass Tare	21.63	21.50	21.64	
Mass of Water	2.30	2.01	2.47	
Dry Soil Mass	14.29	12.60	15.38	
Moisture Content	16.1	16.0	16.1	

Average Plastic Limit	16
Plasticity Index	4
Received Moisture	8.8

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





EC Environment & Infrastructure
A division of AMEC Americas Limited
6 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

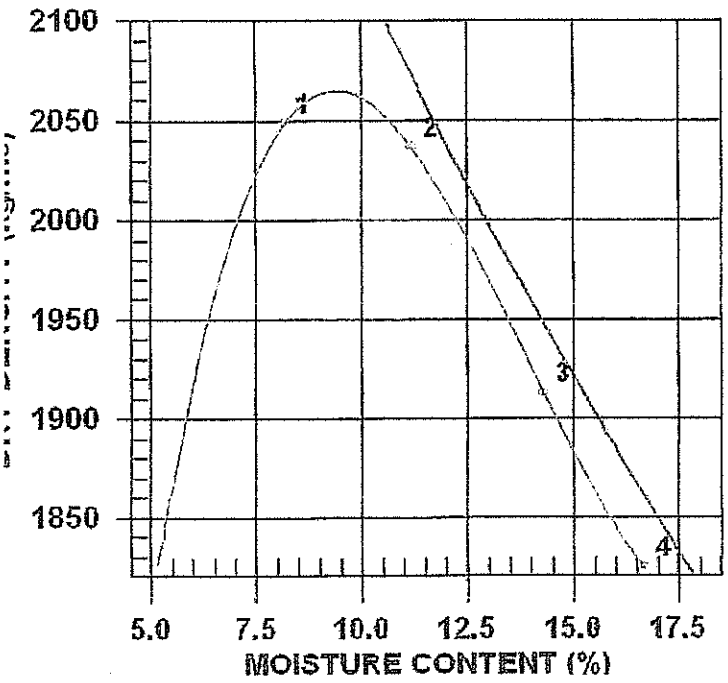
JECT Mount Polley

ITRACTOR

CTOR NO. 19 DATE TESTED 2012.Oct.25 DATE RECEIVED 2012.Sep.22 DATE SAMPLED 2012.Sep.21

TU MOISTURE	8.8 %
IPLED BY	MPMC Staff
TED BY	D. deSousa
PLIER	Borrow Pit
JRCE	S12-17
TERIAL IDENTIFICATION	
JOR COMPONENT	Till
ZE	-37.5mm
SCRIPTION	
CK TYPE	

COMPACTION STANDARD	Standard Proctor, ASTM D698
COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
RAMMER TYPE	Automatic
PREPARATION	Moist
OVERSIZE CORRECTION METHOD	ASTM 4718
RETAINED 4.75mm SCREEN	15.0 %
OVERSIZE SPECIFIC GRAVITY	2.70
TOTAL NUMBER OF TRIALS	4



TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	2217	2049	8.2
2	2265	2037	11.2
3	2186	1913	14.3
4	2130	1825	16.7

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	2065	9.5
OVERSIZE CORRECTED	2141	8.0

MMENTS

 2012.Oct.29 AMEC Environment & Infrastructure PER. YMichaud

GRAIN SIZE DISTRIBUTION

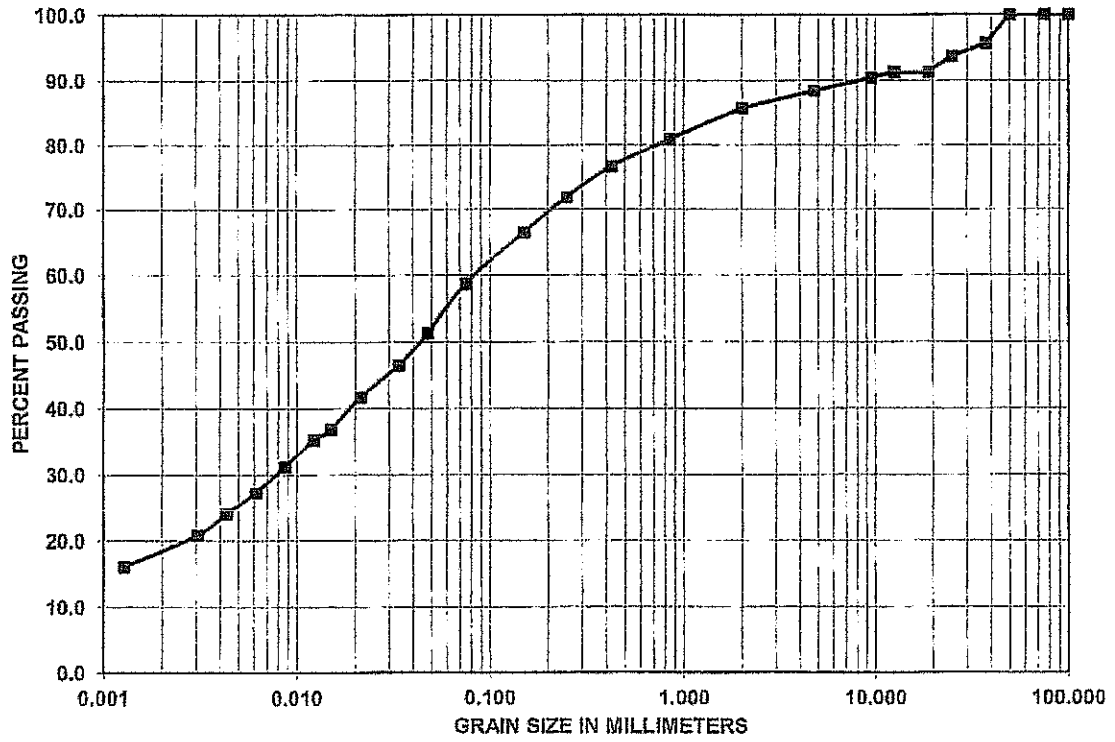
amec

Mount Polley Mining Corporation
P.O. Box 12
Likely, BC
V0L 2N0

OFFICE: Prince George, BC
PROJECT: VM00560A.B.3
DATE: 29-Oct-12

PROJECT NAME: Mt. Polley

TEST No: S12-18
SAMPLED BY: MPMC Staff
DATE SAMPLED: 26-Sep-12
SOURCE: Perimeter Embankmen
DATE TESTED: 27-Oct-12
DEPTH: Lift 9



SUMMARY

Grain size (mm)	Passing (%)
75.0	100.0
50.0	100.0
37.5	95.6
25.0	93.7
19.0	91.2
12.5	91.2
9.5	90.4
4.75	88.4
2.00	85.7
0.850	80.9
0.425	76.7
0.250	71.8
0.150	66.4
0.075	58.8
0.0476	51.3
0.0337	46.5
0.0213	41.7
0.0151	36.9
0.0123	35.3
0.0087	31.3
0.0061	27.3
0.0043	24.1
0.0031	20.8
0.0013	16.0

REMARKS:

D_{10} =	N/A
D_{30} =	N/A
D_{60} =	N/A
C_U =	N/A
C_c =	N/A

GRAVEL	11.63%
SAND	29.61%
SILT	40.77%
CLAY	17.99%

TECHNICIAN: MMichaud

ATTERBERG LIMITS
ASTM D4318

PROJECT:	Mt. Polley	Sample ID:	S12-18 (Perimeter Embankment)
Project Number:	VM00560A.B.3	Date Sampled:	26-Sep-12
Technician:	J. McDonald	Depth:	Lift 9
Date:	25-Oct-12	Comments:	

Liquid Limit

Trial No.	1	2	3	
No. of Blows	32	24	20	
Tare ID	AQ	AV	AA	
Mass Wet + Tare	34.56	35.80	34.73	
Mass Dry + Tare	31.86	32.76	31.91	
Mass Tare	21.57	21.64	21.79	
Mass of Water	2.70	3.04	2.82	
Dry Soil Mass	10.29	11.12	10.12	
Moisture Content	26.2	27.3	27.9	
Liquid Limit	27.1	27.2	27.1	

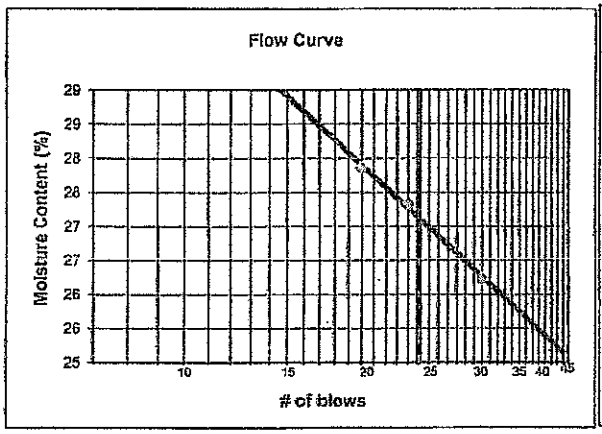
Average Liquid Limit: 27

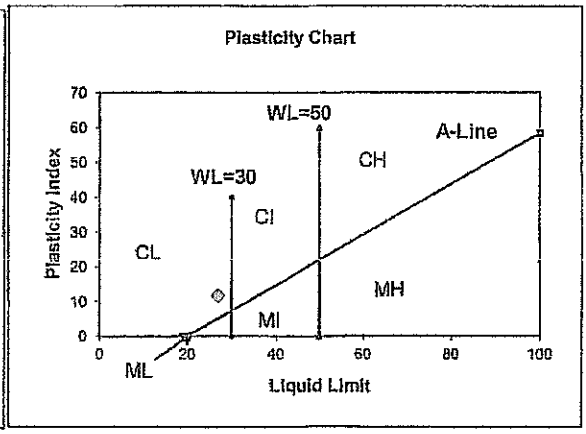
Plastic Limit

Trial No.	1	2	3	
Tare ID	28	33	44	
Mass Wet + Tare	30.97	34.72	33.35	
Mass Dry + Tare	29.71	33.05	31.81	
Mass Tare	21.32	21.95	21.51	
Mass of Water	1.26	1.67	1.54	
Dry Soil Mass	8.39	11.10	10.30	
Moisture Content	15.0	15.0	15.0	

Average Plastic Limit	15
Plasticity Index	12
Received Moisture	15.5

Plasticity Index	PI = LL - PL
Liquidity Index	LI = (MC - PL) / PI





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A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

MOISTURE - DENSITY RELATIONSHIP REPORT

amec

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

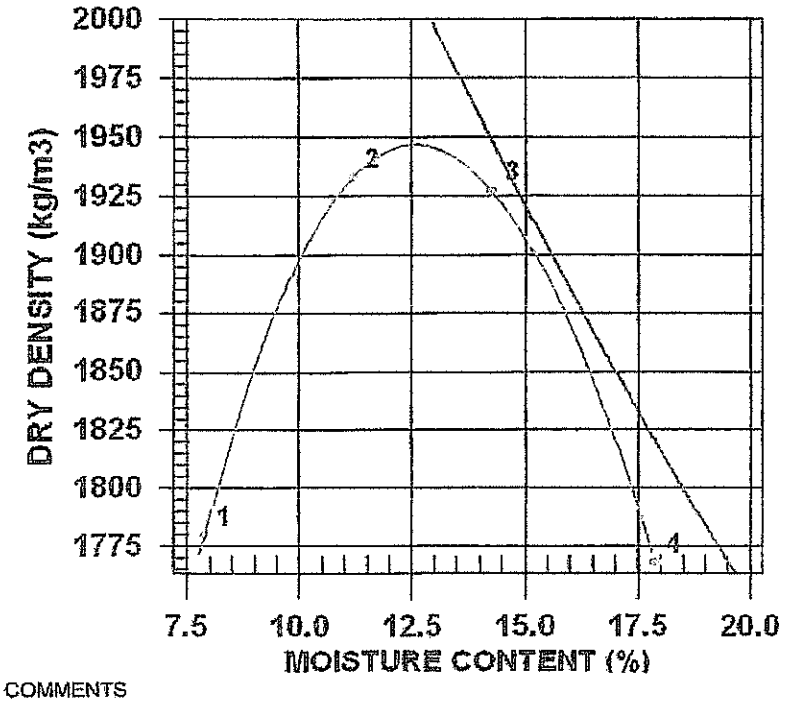
TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

PROJECT Mount Polley

CONTRACTOR

PROCTOR NO. 20 DATE TESTED 2012.Oct.24 DATE RECEIVED 2012.Oct.01 DATE SAMPLED 2012.Sep.

INSITU MOISTURE	15.5 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
SAMPLED BY	MPMC Staff		
TESTED BY	D. deSousa	COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
SUPPLIER	Perimeter, Lift 9		
SOURCE	S12-18	RAMMER TYPE	Automatic
MATERIAL IDENTIFICATION		PREPARATION	Moist
MAJOR COMPONENT	Glacial Till	OVERSIZE CORRECTION METHOD	ASTM 4718
SIZE	-37.5mm	RETAINED 4.75mm SCREEN	10.0 %
DESCRIPTION		OVERSIZE SPECIFIC GRAVITY	2.70
ROCK TYPE		TOTAL NUMBER OF TRIALS	4



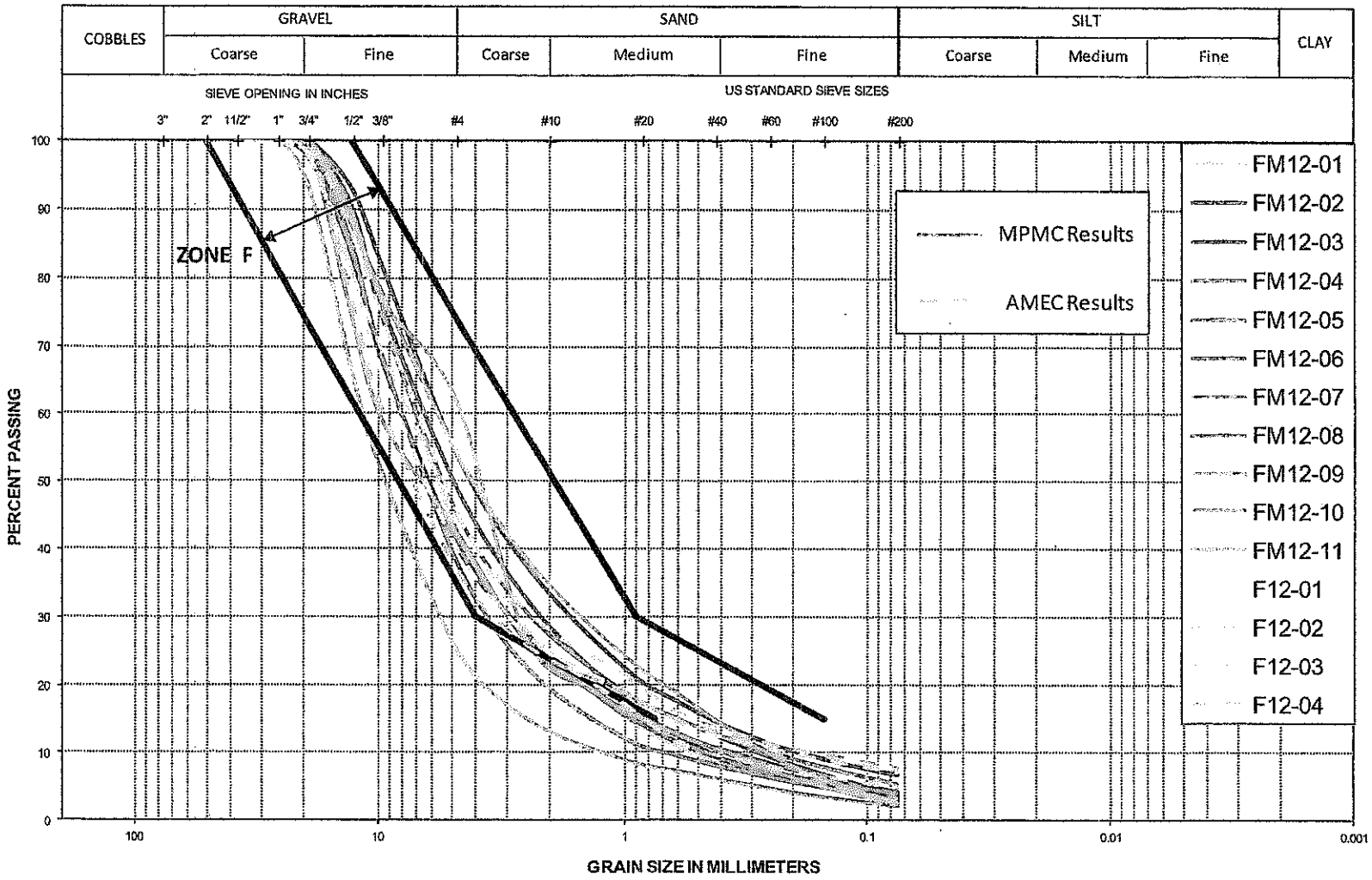
TRIAL NUMBER	WET DENSITY (kg/m3)	DRY DENSITY (kg/m3)	MOISTURE CONTENT (%)
1	1921	1780	7.9
2	2149	1933	11.2
3	2202	1927	14.3
4	2084	1768	17.9

ZERO AIR VOIDS CURVE FOR ESTIMATED SPECIFIC GRAVITY OF 2.70	MAXIMUM DRY DENSITY (kg/m3)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1947	12.5
OVERSIZE CORRECTED	2003	11.5

COMMENTS

 2012.Oct.29 AMEC Environment & Infrastructure PER. GMichaud

2012 Zone F (FILTER) GRADATIONS



AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

SIEVE ANALYSIS REPORT
8 16 30 50 SERIES

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

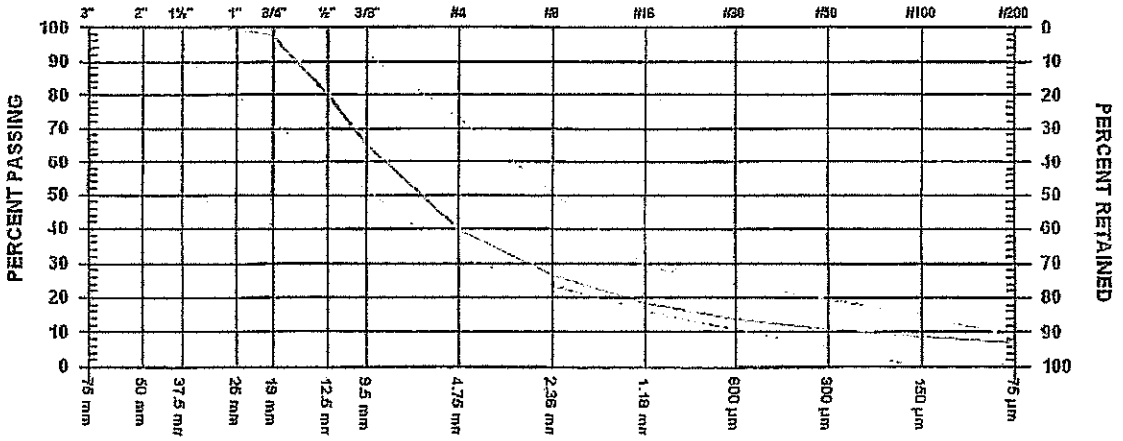
PROJECT Mount Polley

CONTRACTOR

SIEVE TEST NO. 27 DATE RECEIVED 2012.Jul.18 DATE TESTED 2012.Jul.20 DATE SAMPLED 2012.Jul.

SUPPLIER
SOURCE
SPECIFICATION Mt Polley - Zone F
MATERIAL TYPE Filter Sample

SAMPLED BY D.Ostritchenko
TESTED BY AMEC lab
TEST METHOD WASHED



GRAVEL SIZES			PERCENT PASSING	GRADATION LIMITS
3"	75	mm		
2"	50	mm		100 - 100
1 1/2"	37.5	mm	100.0	
1"	25	mm	99.7	
3/4"	19	mm	97.9	
1/2"	12.5	mm	80.6	60 - 100
3/8"	9.5	mm	65.5	

SAND SIZES AND FINES			PERCENT PASSING	GRADATION LIMITS
No. 4	4.75	mm	40.0	31 - 73
No. 8	2.36	mm	26.8	
No. 16	1.18	mm	18.9	16 - 29
No. 30	600	µm	14.2	
No. 50	300	µm	11.1	
No. 100	150	µm	8.9	0 - 15
No. 200	75	µm	7.1	0 - 9

MOISTURE CONTENT 4.0%

COMMENTS

 2012.Jul.25 AMEC Environment & Infrastructure PER. YMichaud

AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

SIEVE ANALYSIS REPORT
8 16 30 50 SERIES

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

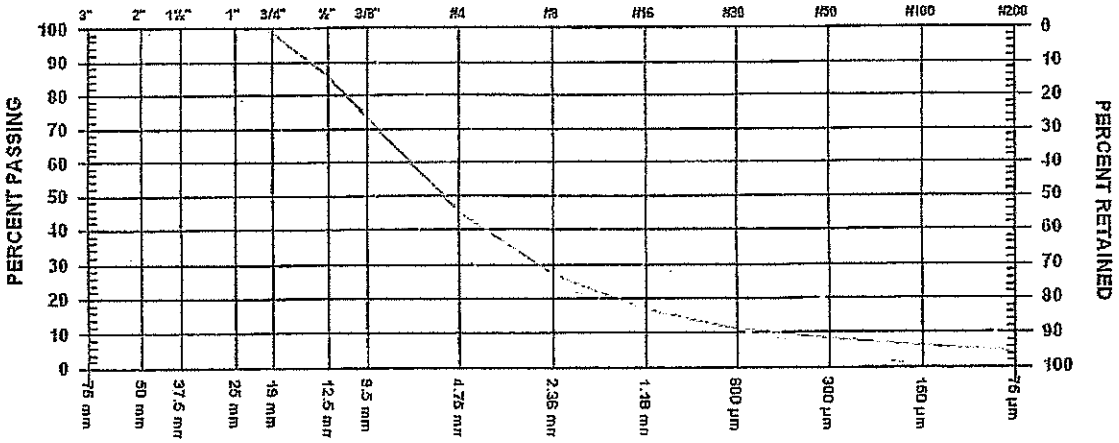
JECT Mount Polley

TRACTOR

'E TEST NO. 28 DATE RECEIVED 2012.Jul.29 DATE TESTED 2012.Jul.30 DATE SAMPLED 2012.Jul.29

PLIER Mt. Polley
RCE
CIFICATION Mt Polley - Zone F
ERIAL TYPE Filter Rock

SAMPLED BY MPMC
TESTED BY M. Lemcke
TEST METHOD WASHED



GRAVEL SIZES			PERCENT PASSING	GRADATION LIMITS
'	75	mm		
'	50	mm		100 - 100
1/2"	37.5	mm		
'	25	mm	100.0	
/4"	19	mm	99.1	
/2"	12.5	mm	86.1	60 - 100
/8"	9.5	mm	73.5	

SAND SIZES AND FINES			PERCENT PASSING	GRADATION LIMITS
No. 4	4.75	mm	45.6	31 - 73
No. 8	2.36	mm	27.4	
No. 16	1.18	mm	17.1	16 - 29
No. 30	600	µm	11.4	
No. 50	300	µm	8.5	
No. 100	150	µm	6.5	0 - 15
No. 200	75	µm	4.9	0 - 9

MOISTURE CONTENT 2.9%

MMENTS

 2012.Aug.10 AMEC Environment & Infrastructure PER.

AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

SIEVE ANALYSIS REPORT
10 20 40 60 SERIES

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

TO
Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

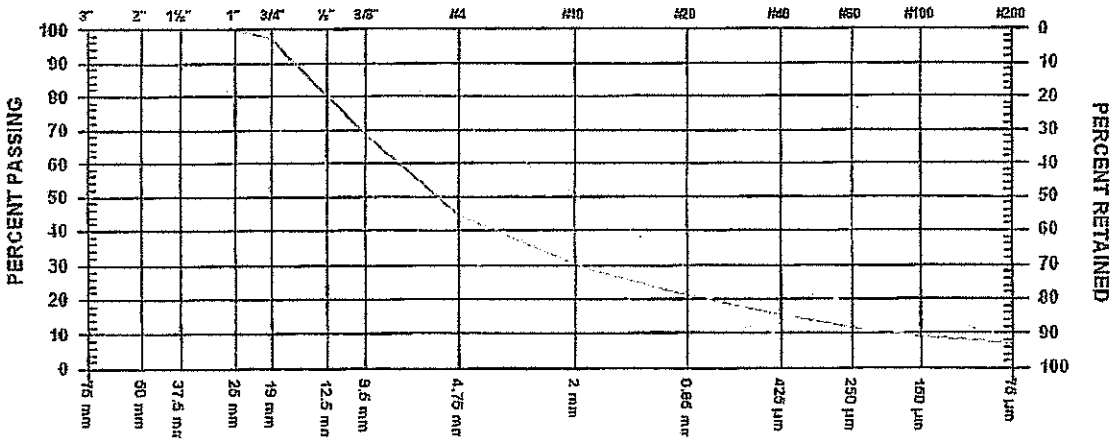
PROJECT Mount Polley

CONTRACTOR

SIEVE TEST NO. 29 DATE RECEIVED 2012.Sep.12 DATE TESTED 2012.Sep.20 DATE SAMPLED 2012.Sep.

SUPPLIER Perimeter Embankment
SOURCE Sta 45+00, Elv. 961.4m
SPECIFICATION Mt Polley - Zone F
MATERIAL TYPE Filter Zone F

SAMPLED BY MPMC staff
TESTED BY AMEC lab
TEST METHOD WASHED



GRAVEL SIZES		PERCENT PASSING	GRADATION LIMITS
3"	75 mm		
2"	50 mm		100 - 100
1 1/2"	37.5 mm		
1"	25 mm	100.0	
3/4"	19 mm	97.4	
1/2"	12.5 mm	80.3	60 - 100
3/8"	9.5 mm	68.9	

SAND SIZES AND FINES		PERCENT PASSING	GRADATION LIMITS
No. 4	4.75 mm	44.6	31 - 73
No. 10	2.00 mm	30.2	
No. 20	850 µm	21.2	16 - 29
No. 40	425 µm	15.7	
No. 60	250 µm	12.0	
No. 100	150 µm	9.4	0 - 15
No. 200	75 µm	7.3	0 - 9

MOISTURE CONTENT 4.8%

COMMENTS

 2012.Oct.06 AMEC Environment & Infrastructure PER. [signature]

AMEC Environment & Infrastructure
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SIEVE ANALYSIS REPORT
8 16 30 50 SERIES

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

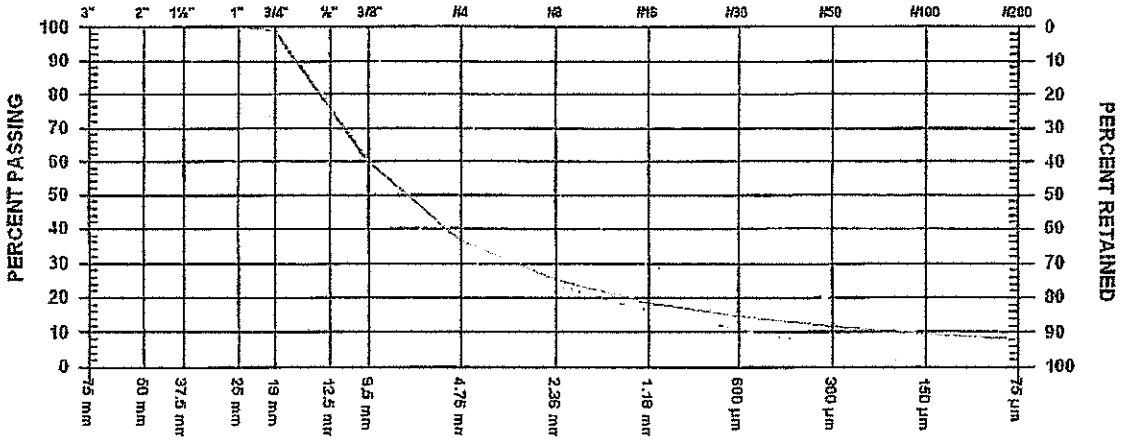
JECT Mount Polley

TRACTOR

'E TEST NO. 30 DATE RECEIVED 2012.Oct.01 DATE TESTED 2012.Oct.23 DATE SAMPLED 2012.Sep.26

PLIER
RCE South Embankment
CIFICATION Mt Polley - Zone F
ERIAL TYPE Sta 14+50, Elv. 963.38m

SAMPLED BY MPMC
TESTED BY D. DeSousa
TEST METHOD WASHED



GRAVEL SIZES			PERCENT PASSING	GRADATION LIMITS
'	75	mm		
'	50	mm		100 - 100
1/2"	37.5	mm		
'	25	mm	100.0	
/4"	19	mm	99.4	
/2"	12.5	mm	76.2	60 - 100
/8"	9.5	mm	60.1	

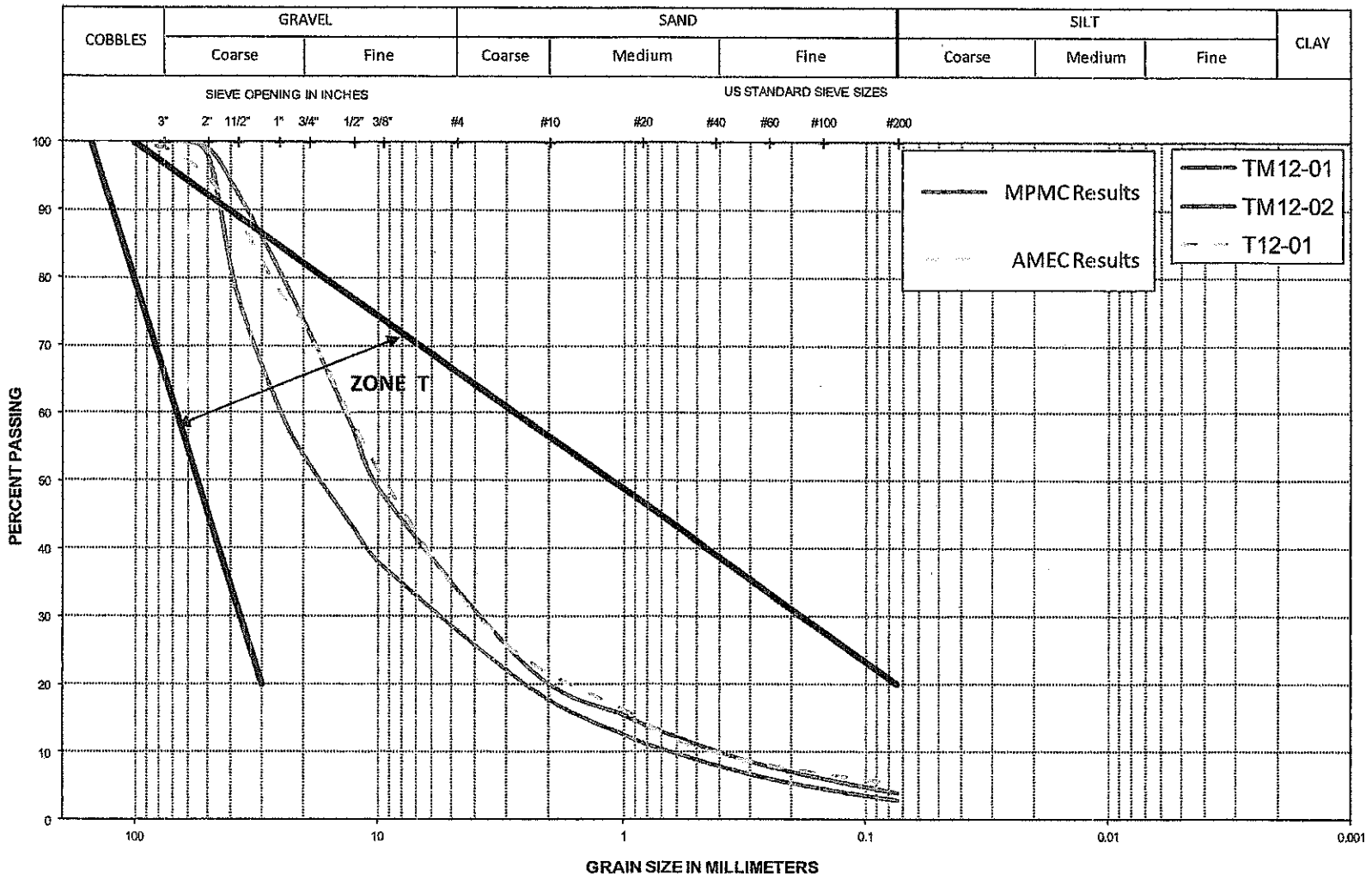
SAND SIZES AND FINES			PERCENT PASSING	GRADATION LIMITS
No. 4	4.75	mm	36.8	31 - 73
No. 8	2.36	mm	25.4	
No. 16	1.18	mm	18.9	16 - 29
No. 30	600	µm	14.7	
No. 50	300	µm	11.9	
No. 100	150	µm	9.8	0 - 15
No. 200	75	µm	7.9	0 - 9

MOISTURE CONTENT 3.7%

IMENTS

 2012.Oct.28 AMEC Environment & Infrastructure PER. GMichaud

2012 ZONE T (TRANSITION) GRADATIONS



AMEC Environment & Infrastructure
A division of AMEC Americas Limited
3456 Opie Crescent, Prince George, BC, V2N 2P9

SIEVE ANALYSIS REPORT
8 16 30 50 SERIES

PROJECT NO. VM0560
CLIENT Mount Polley Mining Corp.
C.C.

Mount Polley Mining Corp.
P.O. Box 12
Likely, BC
V0L 2N0

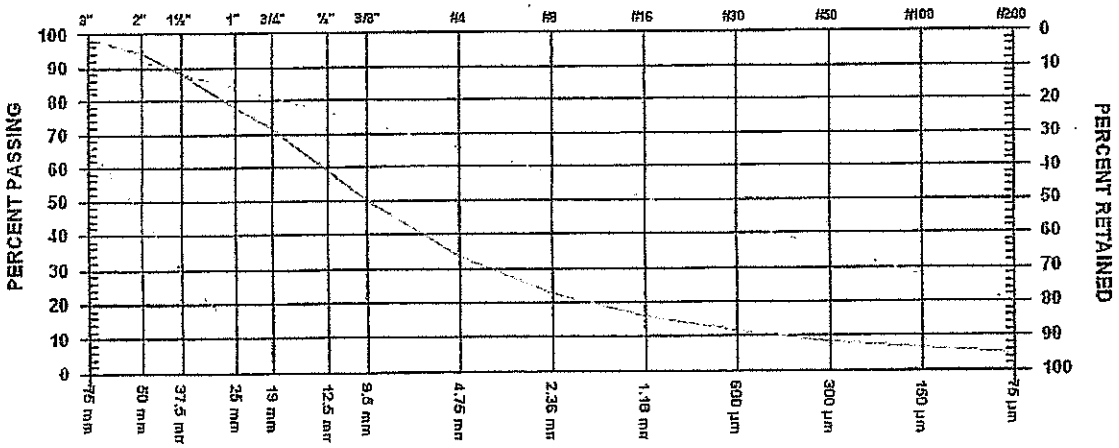
JECT Mount Polley

TRACTOR

E TEST NO. 26 DATE RECEIVED 2012.Jul.18 DATE TESTED 2012.Jul.20 DATE SAMPLED 2012.Jul.18

PLIER
RCE
CIFICATION Mt Polley - Zone T
ERIAL TYPE Transition

SAMPLED BY D.Ostritchnko
TESTED BY AMEC lab
TEST METHOD WASHED



GRAVEL SIZES			PERCENT PASSING	GRADATION LIMITS
"	75	mm	98.9	67 - 97
"	50	mm	94.7	46 - 92
1/2"	37.5	mm	88.7	30 - 88
"	25	mm	78.0	
/4"	19	mm	71.8	0 - 81
/2"	12.5	mm	59.0	
/8"	9.5	mm	50.4	

SAND SIZES AND FINES			PERCENT PASSING	GRADATION LIMITS
No. 4	4.75	mm	33.7	
No. 8	2.36	mm	23.2	
No. 16	1.18	mm	16.2	
No. 30	600	µm	11.7	
No. 50	300	µm	8.7	
No. 100	150	µm	6.8	
No. 200	75	µm	5.3	0 - 20

MOISTURE CONTENT 1.0%

MMENTS

 2012.Jul.25 AMEC Environment & Infrastructure PER. MMichaud

APPENDIX C

SAMPLE REPORTS

Mount Polley Mine

Tailing Storage Facility Embankment – Stage 8 (2012)

CONSTRUCTION DAILY REPORT

Imperial Metals

amec

DAILY REPORT NO.: TSF12-07-18

AMEC PROJECT NO.: VM00560A

HOURS WORKED: 6:00am to 6:00pm (12.0 hours) WEATHER: 29° C, Sunny

DESCRIPTION OF WORK PERFORMED TODAY

Construction Activities

Zone S – PE:

- Till placed between **Sta. 45+75 to 47+75.** El. 960.5m

Zone F – SE:

- Filter placed between **Sta. 12+75 to 16+00.**
- Filter graded between **Sta. 5+75 to 15+40.**

Zone F – ME:

- Filter placed between **Sta. 16+00 to 21+00.**

PE:

- Tie-in preparations continue.

Compaction Testing

-Till material **tested** and **approved** from **Sta. 28+00** to **Sta. 32+00.** **(Lift 2)**
-Till material **tested** and **approved** from **Sta. 39+00** to **Sta. 42+00.** **(Lift 2)**

Material Testing

- Moisture test performed
- Filter (in-place) sample collected

Instrumentation Monitoring

- N/A

REMARKS (Delays, interruptions, extra work activities, unusual occurrences, etc. relevant to today's work)

- AMEC Representative on site (Dmitri Ostritchenko)
- Peterson on site

CRITICAL INFORMATION

- N/A

Field Inspector. **Mitchell Regenstreif** _____ Signature _____ Date

AMEC Rep. **Dmitri Ostritchenko** _____ Signature _____ Date

MPMC Rep. Blythe Golobic _____ _____

DAILY PHOTOGRAPHS

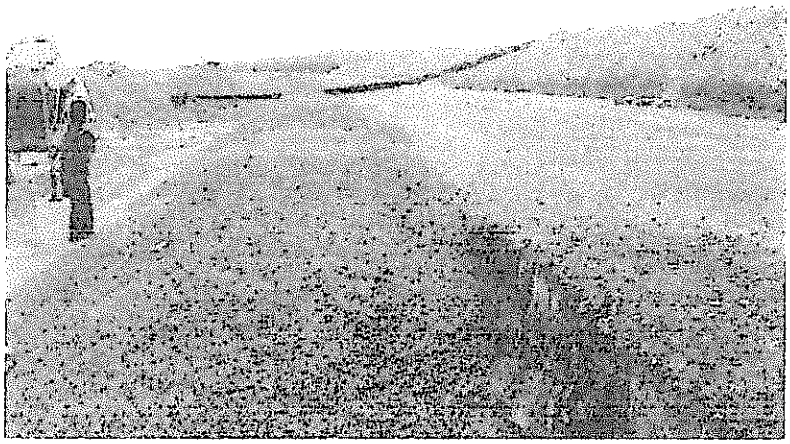


Figure 1: Filter placed near to the ME pipe.

Figure 2: Completion of the SE filter layer.

Figure 3: Tie-in preparations by corner-5.

Mount Polley Mine

Tailing Storage Facility Embankment – Stage 8 (2012)

CONSTRUCTION DAILY REPORT

Imperial Metals

amec

DAILY REPORT NO.: TSF12-08-01

AMEC PROJECT NO.: VM00560A

HOURS WORKED: 6:00am to 6:00pm (12.0 hours) **WEATHER:** 16° C, Consistant light rain

DESCRIPTION OF WORK PERFORMED TODAY

Construction Activities

Sand Cells – SE:

- Construction begun from **Sta. 5+85** to **Sta. 7+50.**

Zone S – SE:

- Placement from **Sta. 15+28** to **Sta. 15+50. El. 960.69m**

Zone S – ME:

- Placement from **Sta. 15+50** to **Sta. 16+28. El. 960.50m**
- Placement from **Sta. 23+70** to **Sta. 27+50.**

Zone F – SE:

- Placement from **Tie-in** to **Sta. 5+85.**

Zone T – PE:

- Placement from **Sta. 27+40** to **Sta. 38+37.**

Compaction Testing

-Till material **tested** and **approved** from **Sta. 15+39** to **Sta. 19+84. (Lift 3)**

Material Testing

- Moisture test was performed.

Instrumentation Monitoring

-N/A

REMARKS (Delays, interruptions, extra work activities, unusual occurrences, etc. relevant to today's work)

- AMEC Representative not on site
- Peterson on site
-Filter was placed by 4-corner where the construction ceases to follow the design. Additional efforts will be needed to fix the area (cut/fill as needed) before till placement can begin.

CRITICAL INFORMATION

Field Inspector. **Mitchell Regenstreif** _____ *Signature* _____ *Date*

AMEC Rep. **Dmitri Ostritchenko** _____ _____

	Signature	Date
MPMC Rep. Blythe Golobic		

DAILY PHOTOGRAPHS

Figure 1: Shallow slope of till resulted in a slight over-lap of the filter layer

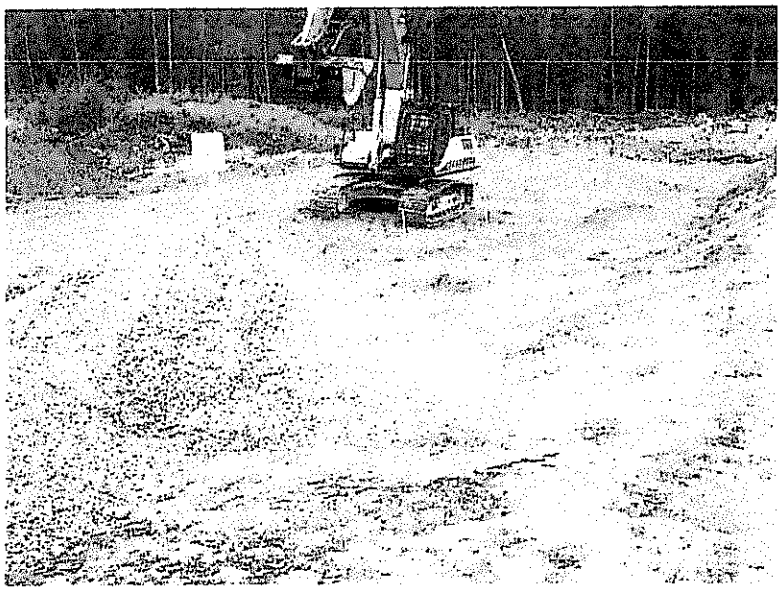
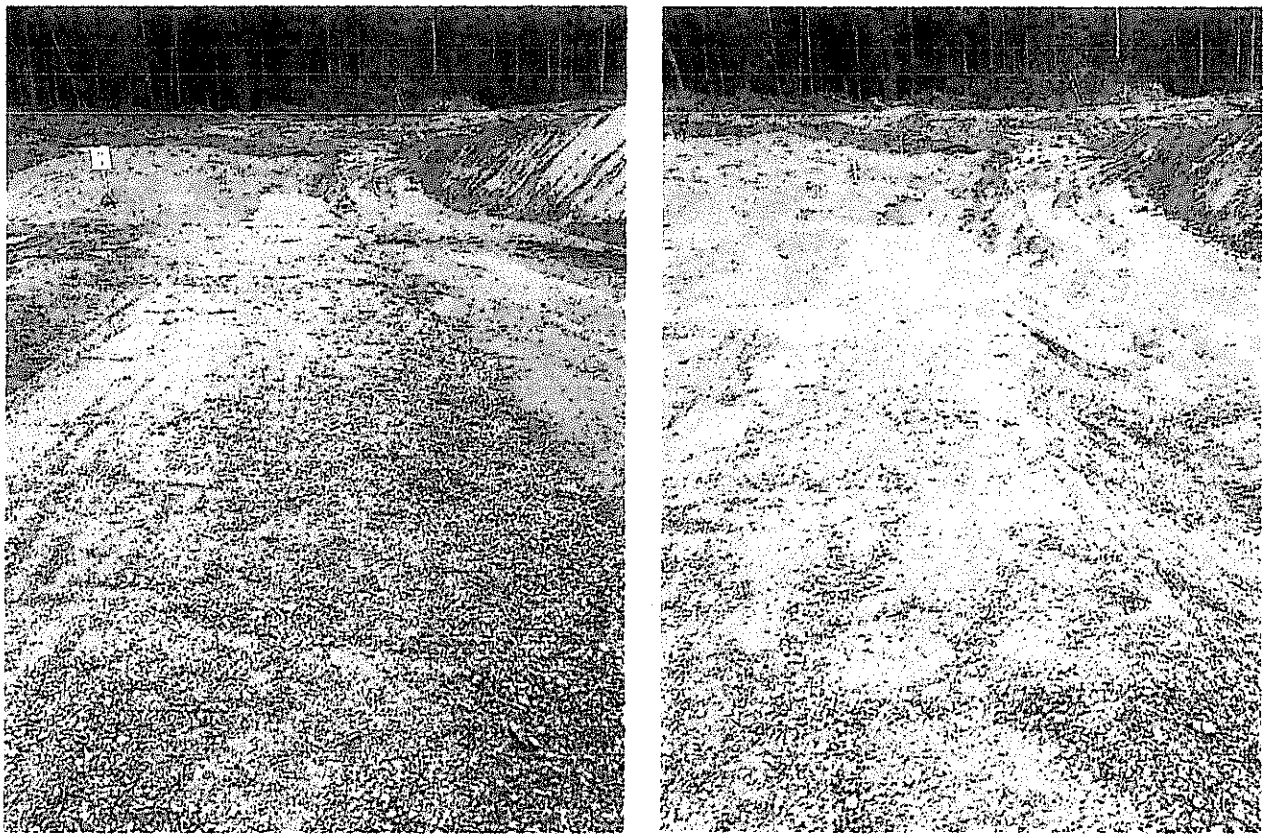


Figure 2: Placement of filter by 4-corner within the outlined bounds



Figure(s) 3: The blue marker indicates where the T/F contact is supposed to be at the given elevation. As we approach 4-corner, material must be added - whereas material must be removed as we distance ourselves from 4-corner.